

## Section 27

# Heterojunction Bipolar Transistor

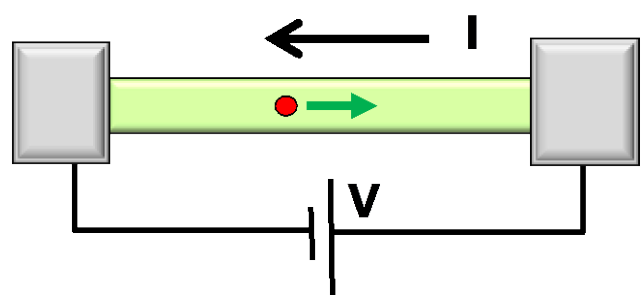
### 27.7 Double heterojunction HBTs

Gerhard Klimeck  
[gekco@purdue.edu](mailto:gekco@purdue.edu)



School of Electrical and  
Computer Engineering

# Section 27 Heterojunction Bipolar Transistor



$$I = G \times V$$

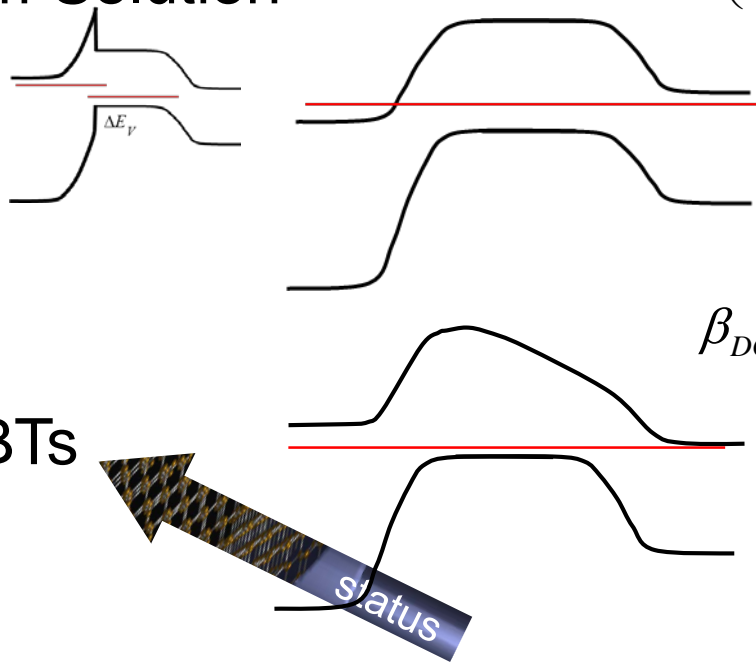
$$= q \times n \times v \times A$$

↑ charge density    ↑ velocity    area

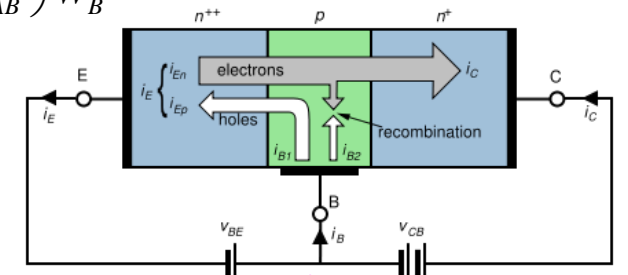
$$\beta_{poly,ballistic} \rightarrow \frac{n_{i,B}^2}{n_{i,E}^2} \times \frac{N_E}{N_B} \times \frac{v_{th}}{v_s}$$

$$\frac{n_{i,B}^2}{n_{i,E}^2} = \frac{N_{C,B} N_{V,B} e^{-E_{g,B}\beta}}{N_{C,E} N_{V,E} e^{-E_{g,E}\beta}} \approx e^{(E_{g,E} - E_{g,B})\beta}$$

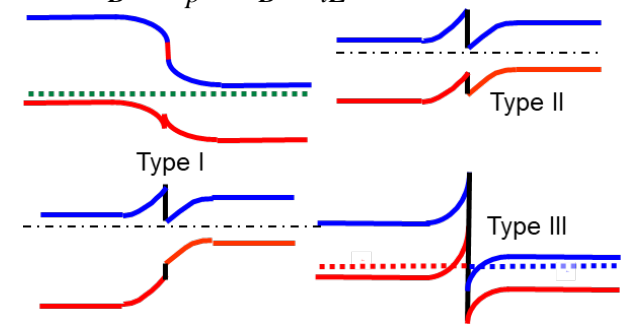
- 1 • 27.1 Applications, Concept, Innovation, Nobel Prize
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$$J_n = q \left( \frac{n_{iB}^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{qV_{BE}/k_B T}$$



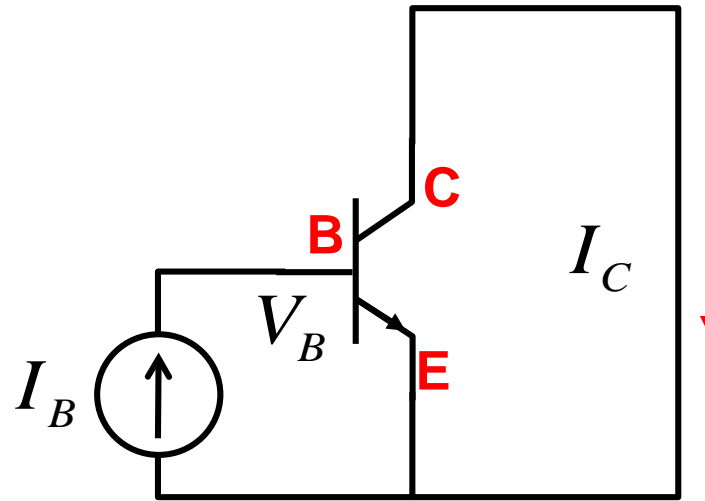
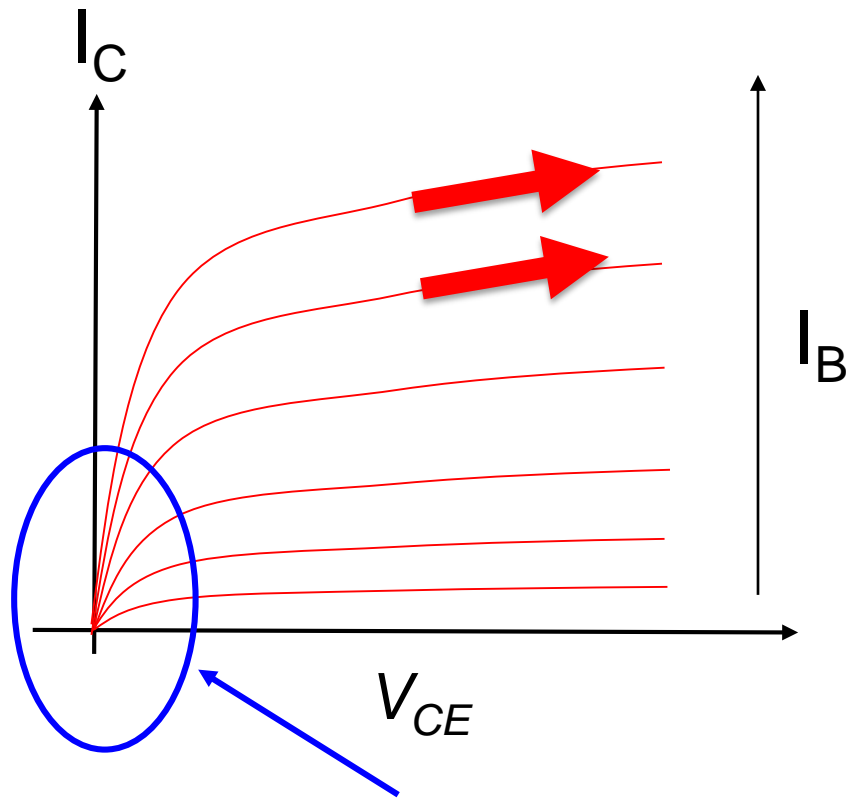
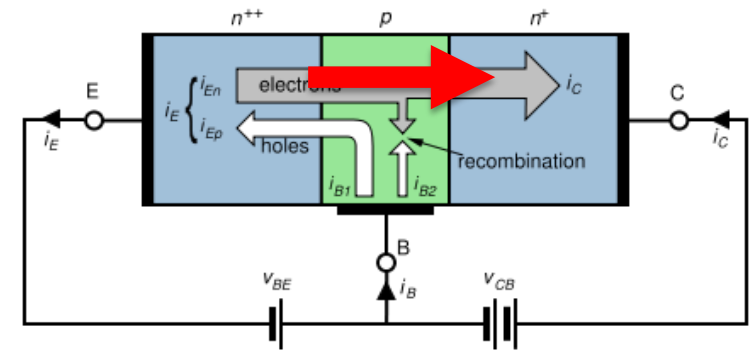
$$\beta_{DC} = \frac{N_E D_n W_E n_{iB}^2}{N_B D_p W_B n_{iE}^2}$$



Mark Lundstrom, "Heterostructure Fundamentals," Purdue University, 1995.  
 Herbert Kroemer, "Heterostructure bipolar transistors and integrated circuits," Proc. *IEEE*, **70**, pp. 13-25, 1982.

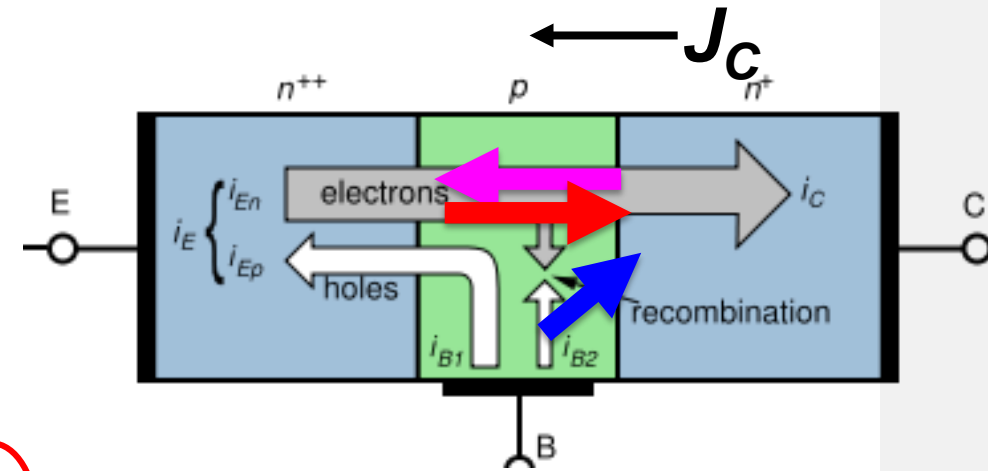
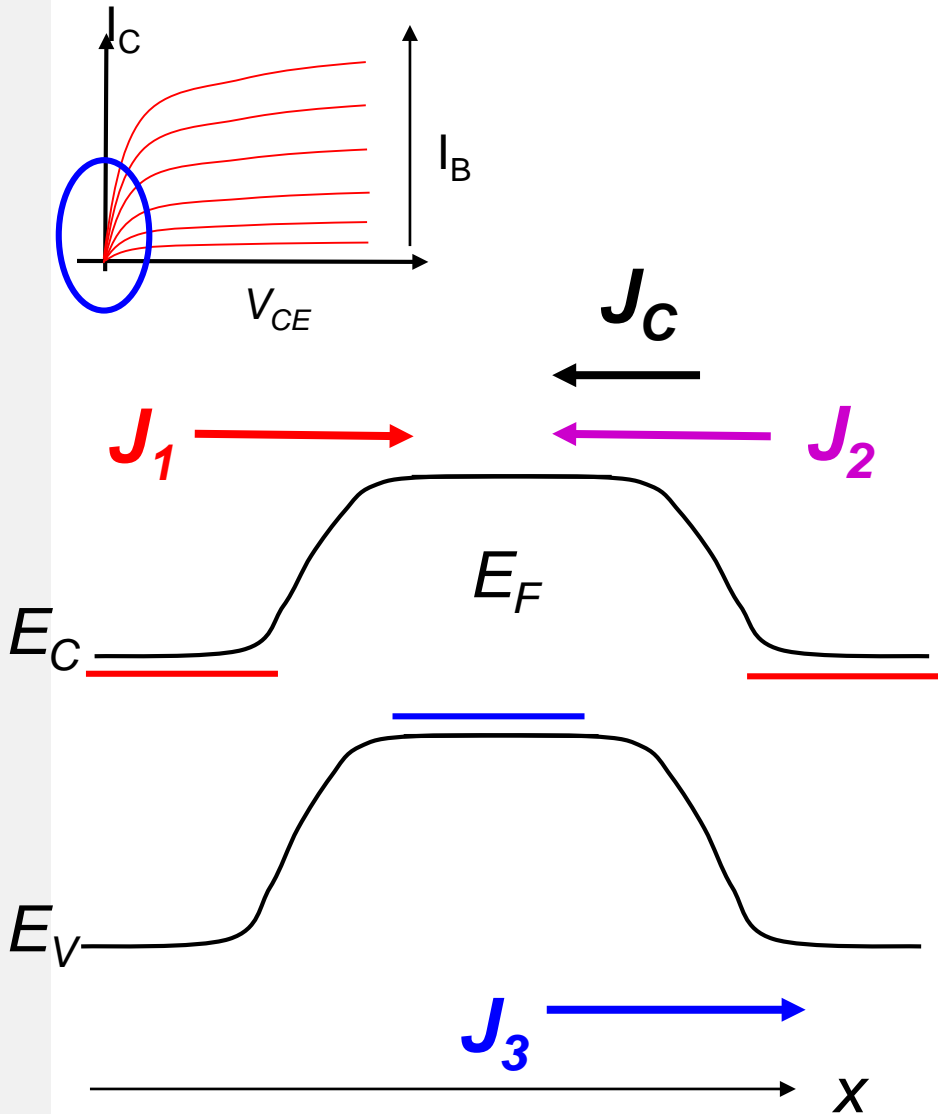
# Offset Voltage - What happens when $V_{CE}=0$

So far we always considered a reverse bias on BC junction



does  $I_C = 0$  at  $V_{CE} = 0$ ?

# Offset Voltage



$$J_1 = q \left( \frac{n_{iB}^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{q(V_E - V_E)/k_B T} \text{ electrons}$$

$$J_2 = q \left( \frac{n_{iB}^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{q(V_E - V_C)/k_B T} \text{ electrons}$$

$$J_3 = q \left( \frac{n_{iC}^2}{N_{DC}} \right) \frac{D_p}{W_C} e^{q(V_E - V_C)/k_B T} \text{ holes}$$

$$J_C = J_1 - J_2 - J_3$$

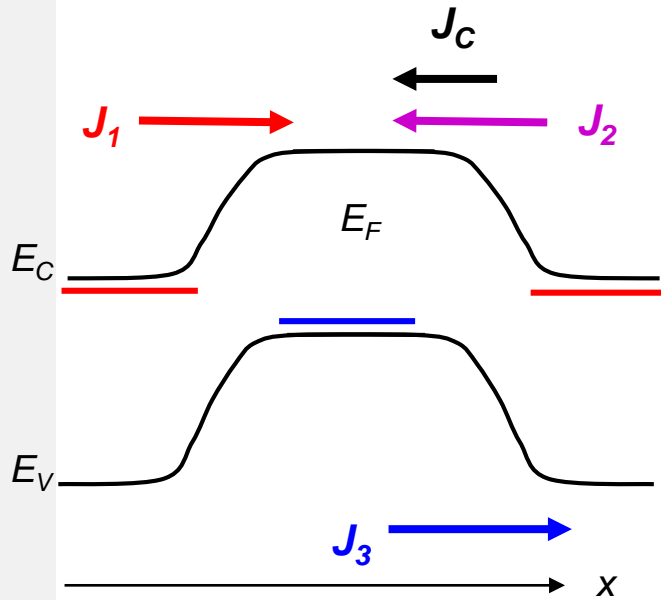
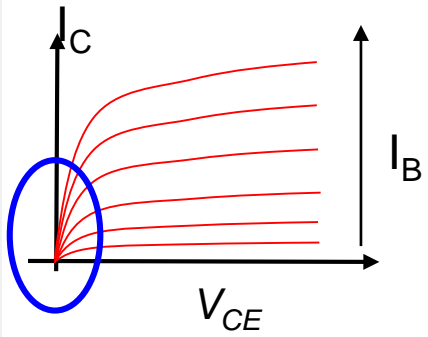
$J_1$  and  $J_2$  are balanced for identical voltages

$J_3$  causes an additional component

$J_3$  and  $J_2$  need to balance  $J_1$  at  $V_E = 0$

set  $J_C = 0$ , assume  $V_E = 0$ , solve for  $V_C = V_{OS}$

# Offset Voltage



$$J_1 = q \left( \frac{n_{iB}^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{q(V_B - V_E)/k_B T} \quad \text{electrons}$$

$$J_2 = q \left( \frac{n_{iB}^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{q(V_B - V_C)/k_B T} \quad \text{electrons}$$

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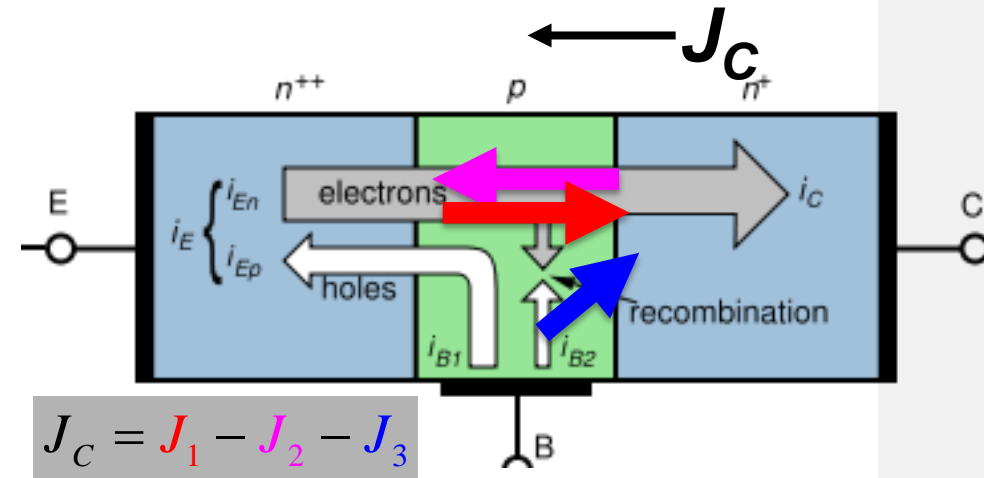
set  $J_C = 0$ , assume  $V_E = 0$ , solve for  $V_C = V_{OS}$

$J_3$  and  $J_2$  need to balance  $J_1$  at  $V_E = 0$

$$\gamma_R = \frac{J_2}{J_3} = \frac{\left( n_{iB}^2 / N_{AB} \right) \left( D_n / W_B \right)}{\left( n_{iC}^2 / N_{DC} \right) \left( D_p / W_C \right)}$$

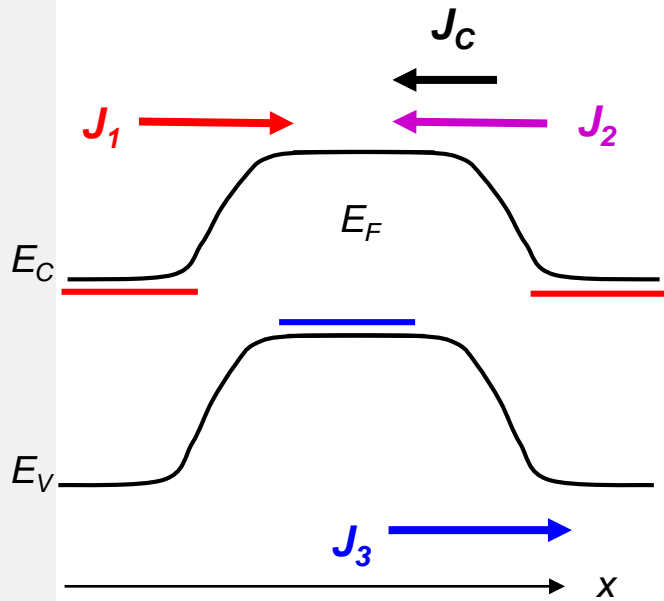
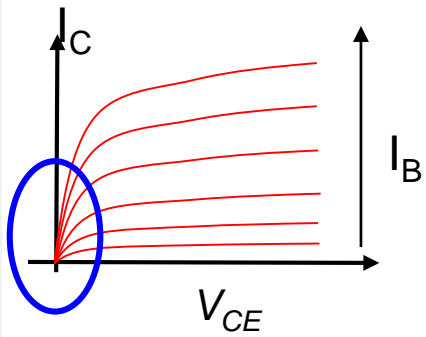
(Reverse Emitter injection efficiency)

$$V_{OS} = \frac{k_B T}{q} \ln \left( 1 + 1/\gamma_R \right)$$



$$J_C = J_1 - J_2 - J_3$$

# Offset Voltage



$$J_1 = q \left( \frac{n_{iB}^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{q(V_B - V_E)/k_B T} \quad \text{electrons}$$

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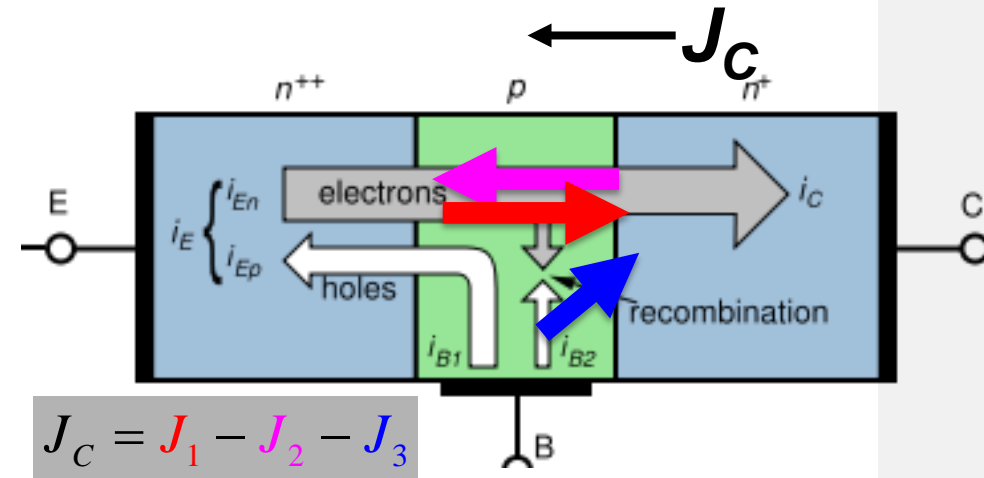
set  $J_C = 0$ , assume  $V_E = 0$ , solve for  $V_C = V_{OS}$

$J_3$  and  $J_2$  need to balance  $J_1$  at  $V_E = 0$

$$\gamma_R = \frac{J_2}{J_3} = \frac{\left( n_{iB}^2 / N_{AB} \right) \left( D_n / W_B \right)}{\left( n_{iC}^2 / N_{DC} \right) \left( D_p / W_C \right)}$$

(Reverse Emitter injection efficiency)

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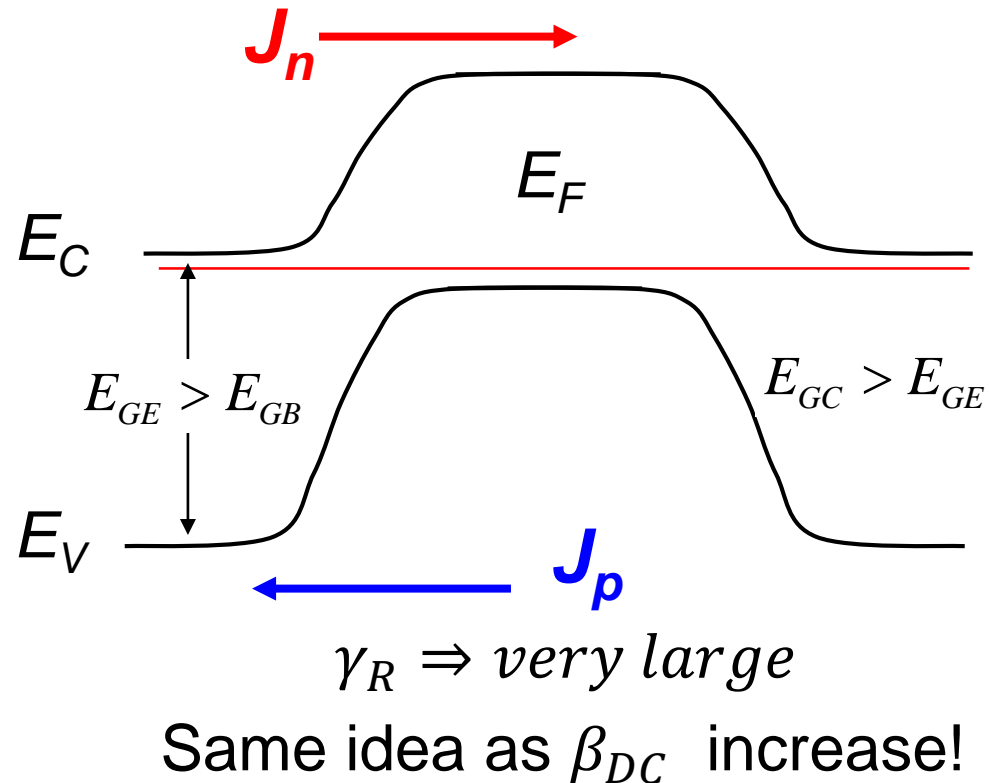
ideally  $J_3$  as small as possible

$\gamma_R \Rightarrow$  very large

$V_{OS} \Rightarrow$  very small

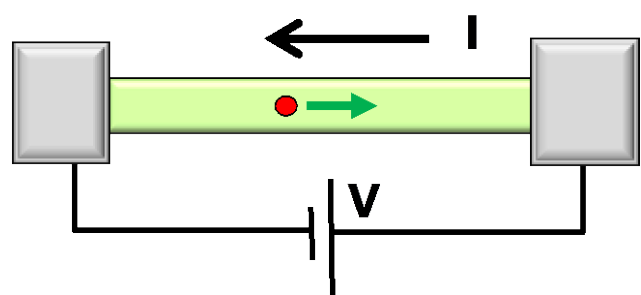
$\Rightarrow$  Increase gap in Collector  
Same idea as  $\beta_{DC}$  increase!

# Double HBJT - large collector bandgap



- Reduce  $V_{OS} = \frac{k_B T}{q} \ln(1 + 1/\gamma_R)$
- High voltage operations for high power devices
- Higher collector bandgap:
  - Reduced avalanche ( $3/2 E_G$ )
  - Increased Kirk current (keep control of collector junction)
- Symmetric operation can simplify circuits

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$$= q \times n \times v \times A$$

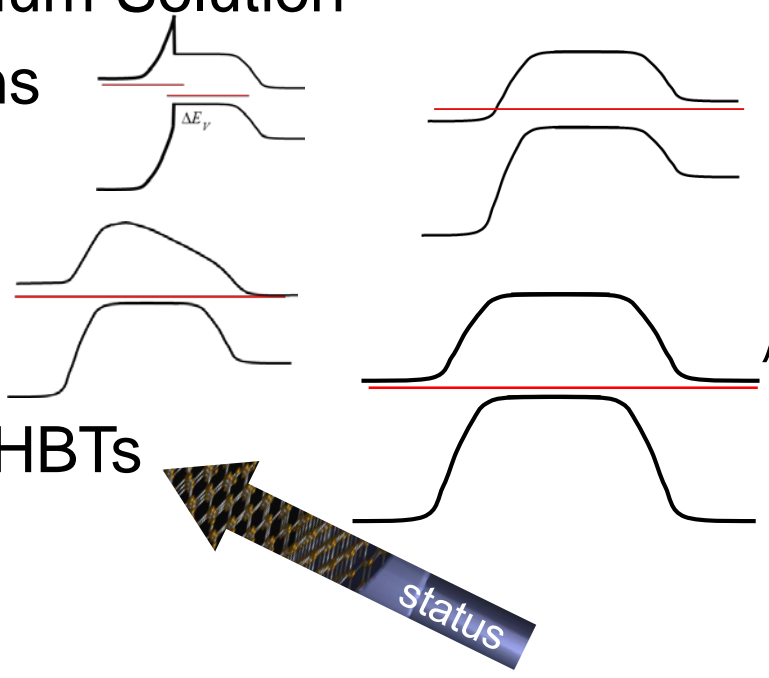
↑ charge density   
 ↑ velocity   
 area

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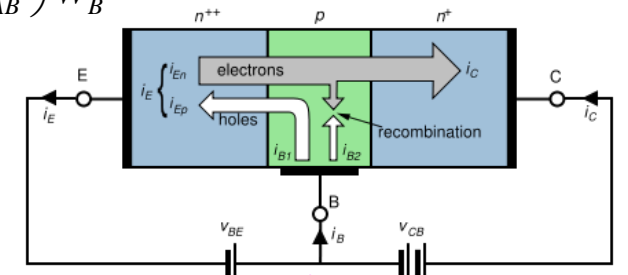
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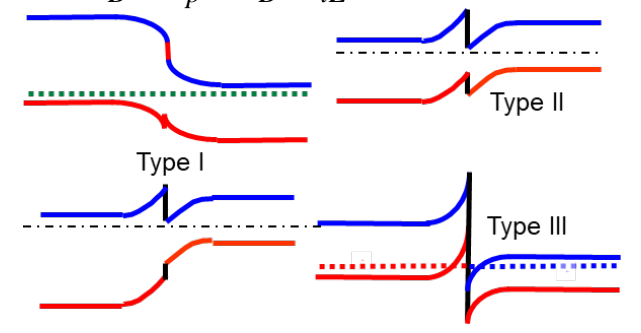
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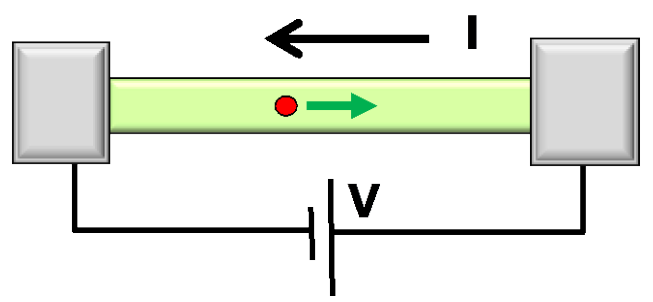
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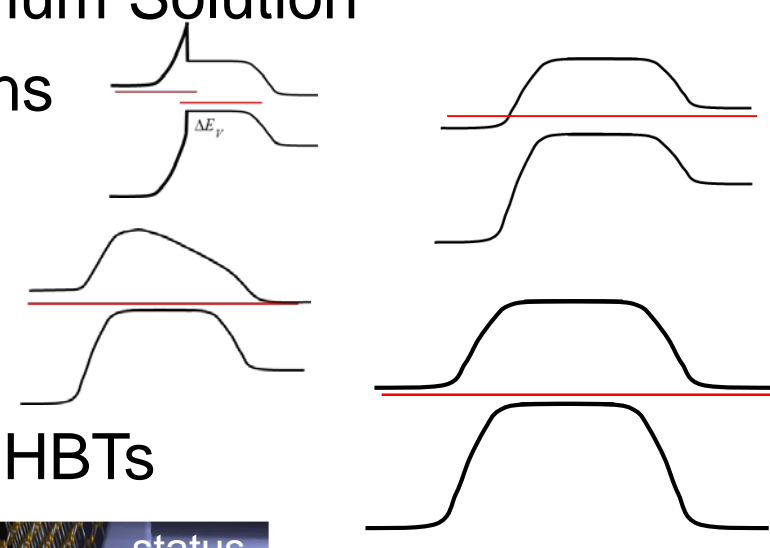
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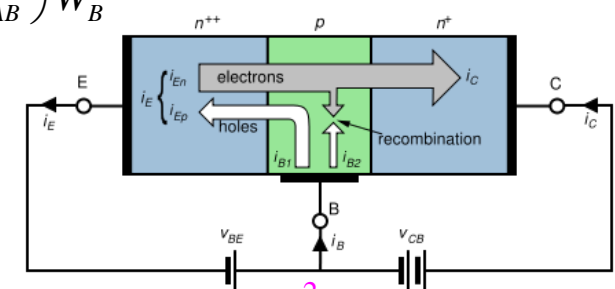
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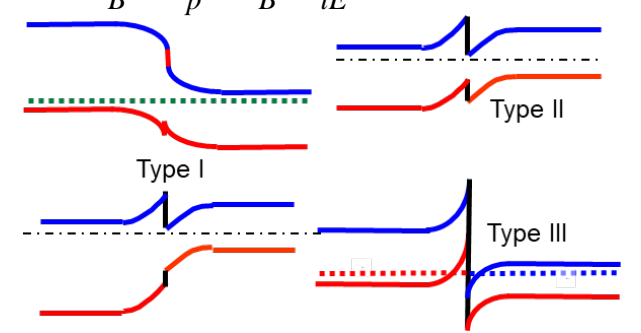
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