

Section 25

Bipolar Junction Transistor – Design

25.2 Base Doping Design

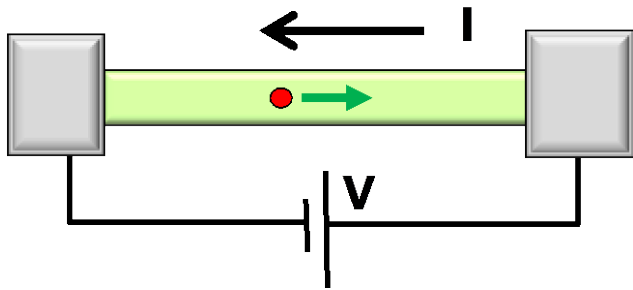
Gerhard Klimeck
gekco@purdue.edu



School of Electrical and
Computer Engineering

Section 25

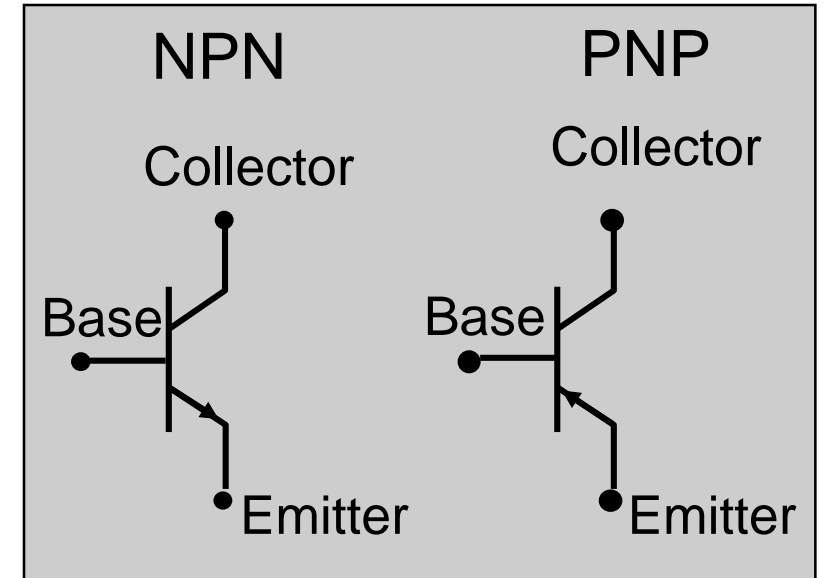
Bipolar Junction Transistor - Design



$$I = G \times V$$

$$= q \times n \times v \times A$$

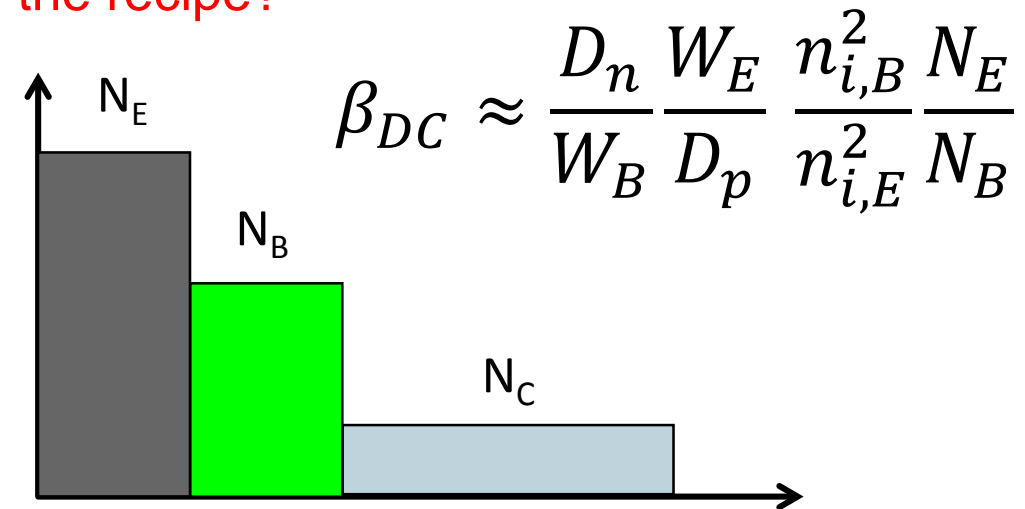
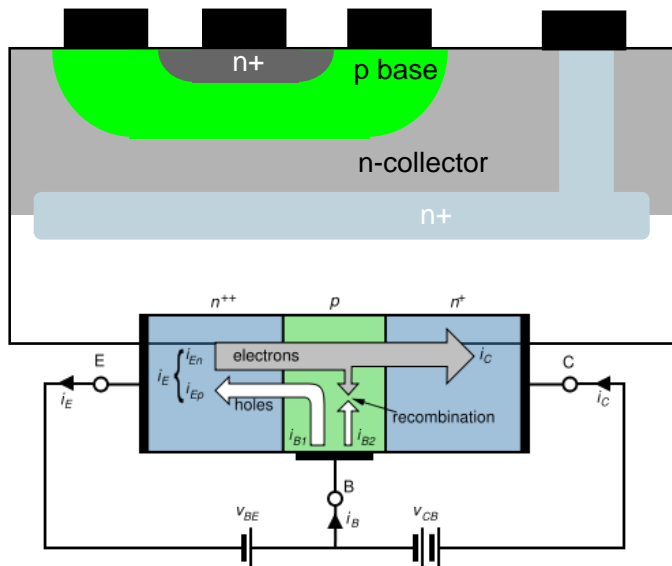
↑ charge density
 ↑ velocity
 area



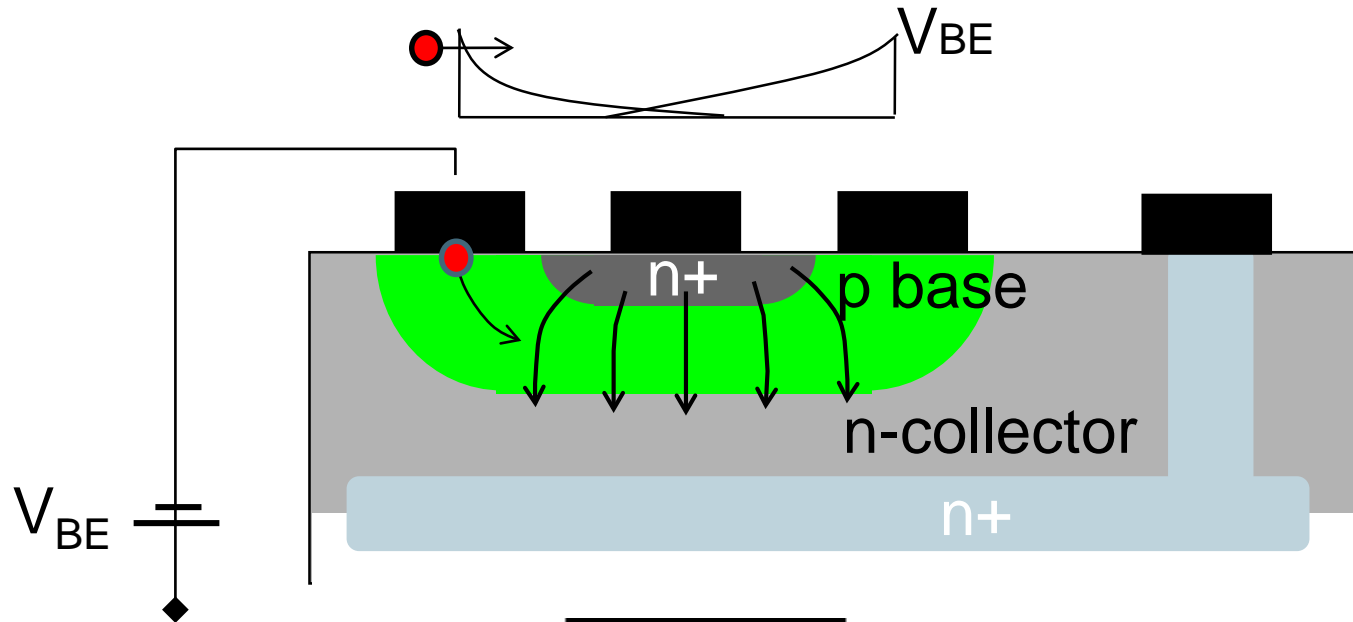
What's wrong with the recipe?

- > • 25.1 Current gain in BJTs
- > • 25.2 Base Doping Design
 - » Current Crowding – Non-Uniform Turn-On
 - » Punch-through
 - » Base Width Modulation

- > • 25.3
- > • 25.4
- > • 25.5
- > • 25.6



Problem of Low Base Doping: Current Crowding - Non-Uniform Turn-On

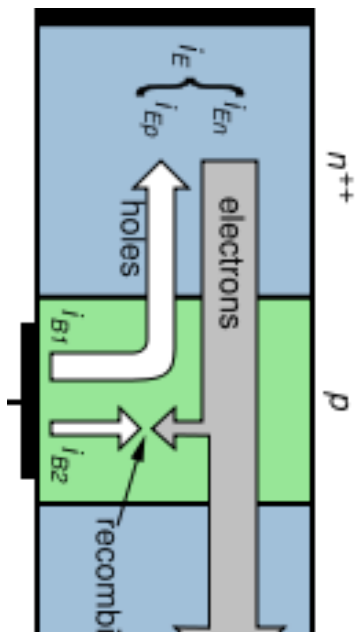


Double diffused junction configuration:

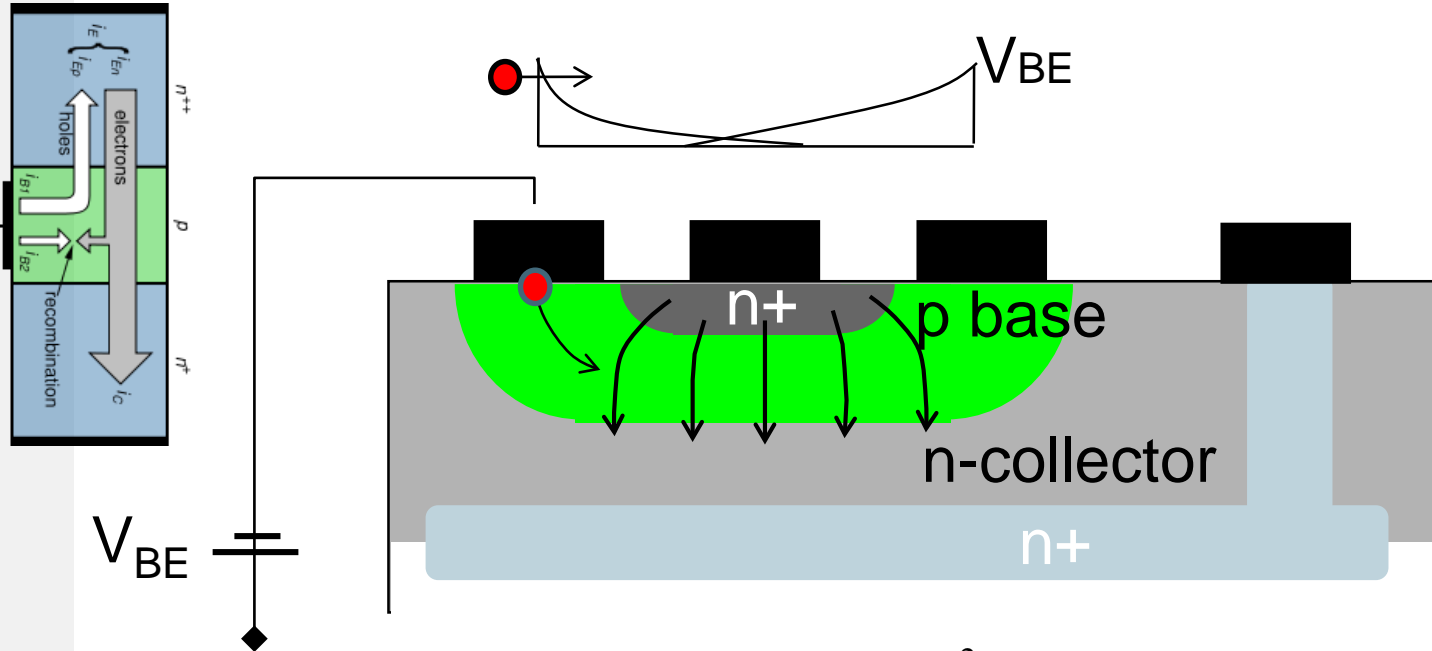
Emitter doping must compensate / overcome the base doping

$$\beta_{DC} \approx \frac{D_n}{W_B} \frac{W_E}{D_p} \frac{n_{i,B}^2}{n_{i,E}^2} \frac{N_E}{N_B}$$

Low doping in base
=> resistance along the current path
=> potential drop



Problem of Low Base Doping: Current Crowding - Non-Uniform Turn-On



$$\beta = \frac{I_C}{I_B} = \frac{\int J_C(x) dx}{\int J_B(x) dx} = \frac{\int \frac{qD_n}{W_B} \frac{n_{i,B}^2}{N_B} (e^{qV'_{BE}(x)\beta} - 1) dx}{\int \frac{qD_p}{W_E} \frac{n_{i,E}^2}{N_E} (e^{qV'_{BE}(x)\beta} - 1) dx}$$

Double diffused junction configuration:

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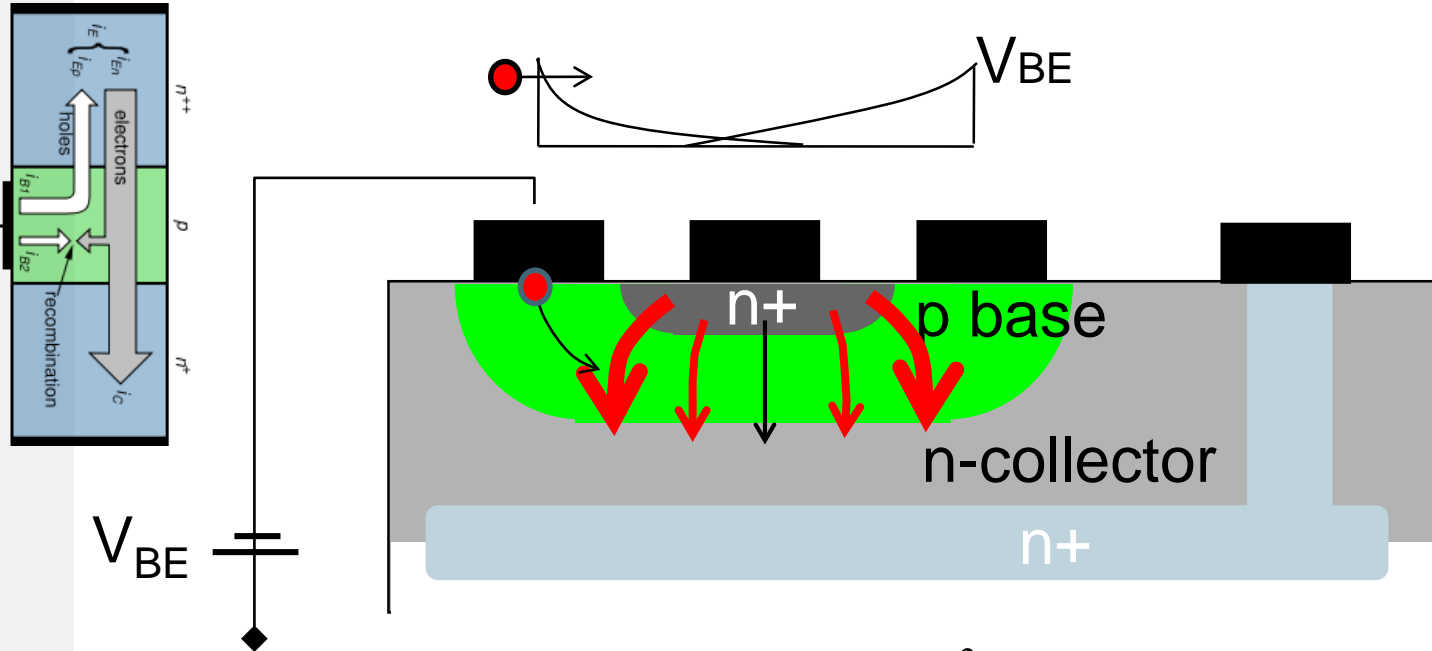
$$\beta_{DC} \approx \frac{D_n}{W_B} \frac{W_E}{D_p} \frac{n_{i,B}^2}{n_{i,E}^2} \frac{N_E}{N_B}$$

Low doping in base
=> resistance along the current path
=> potential drop

=> Determines the injection
=> Spatially dependent
=> More current in the corners

The larger current density near the emitter may cause localized heating and high injection effects

Problem of Low Base Doping: Current Crowding - Non-Uniform Turn-On



$$\beta = \frac{I_C}{I_B} = \frac{\int J_C(x) dx}{\int J_B(x) dx} = \frac{\int \frac{qD_n}{W_B} \frac{n_{i,B}^2}{N_B} (e^{qV'_{BE}(x)\beta} - 1) dx}{\int \frac{qD_p}{W_E} \frac{n_{i,E}^2}{N_E} (e^{qV'_{BE}(x)\beta} - 1) dx}$$

Non-zero base resistance results in a lateral potential difference under the emitter region

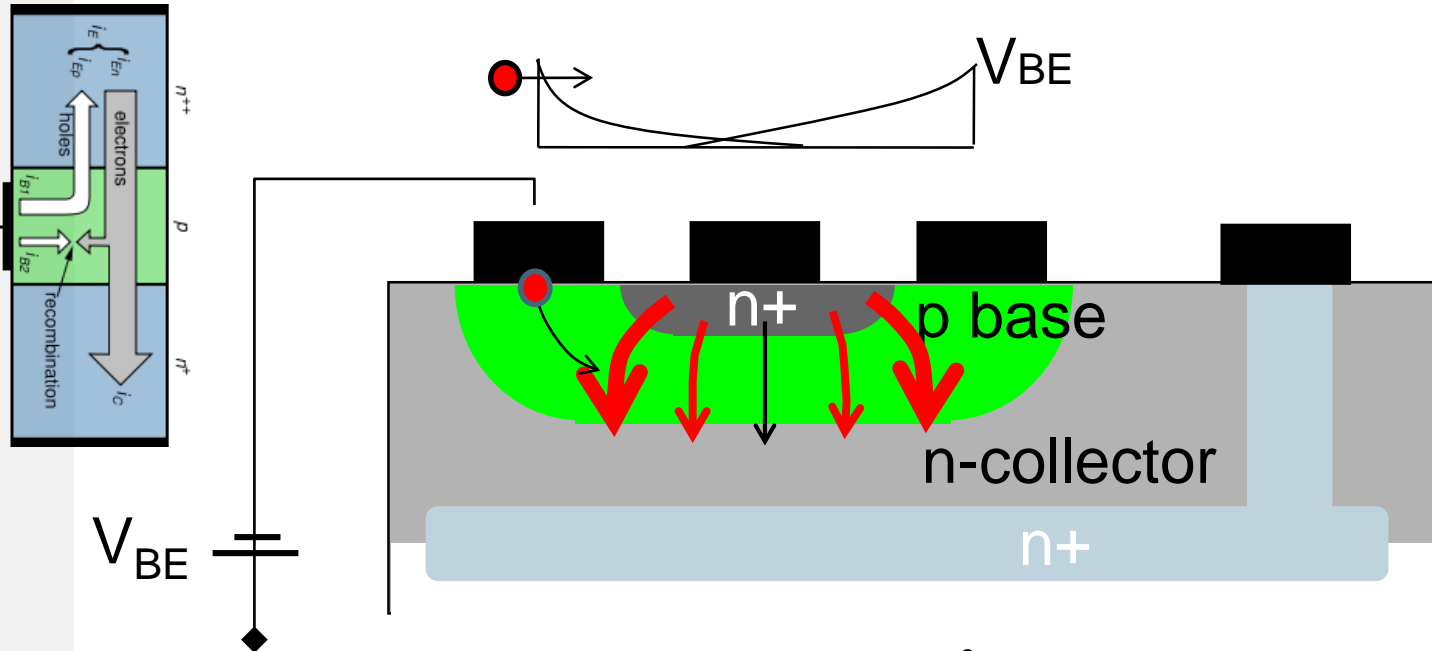
For an n-p-n transistor as shown, the potential decreases from edge of the emitter towards the center (the emitter is highly doped and can be considered an equipotential region)

Double diffused junction configuration:
Emitter doping must compensate / overcome the base doping

$$\beta_{DC} \approx \frac{D_n}{W_B} \frac{W_E}{D_p} \frac{n_{i,B}^2}{n_{i,E}^2} \frac{N_E}{N_B}$$

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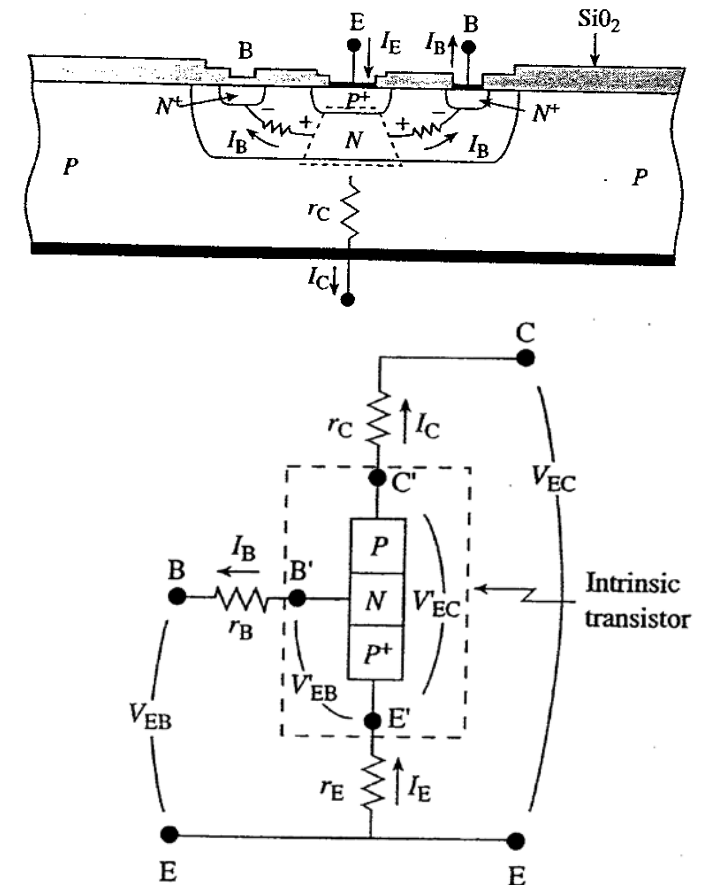
Problem of Low Base Doping: Current Crowding - Non-Uniform Turn-On



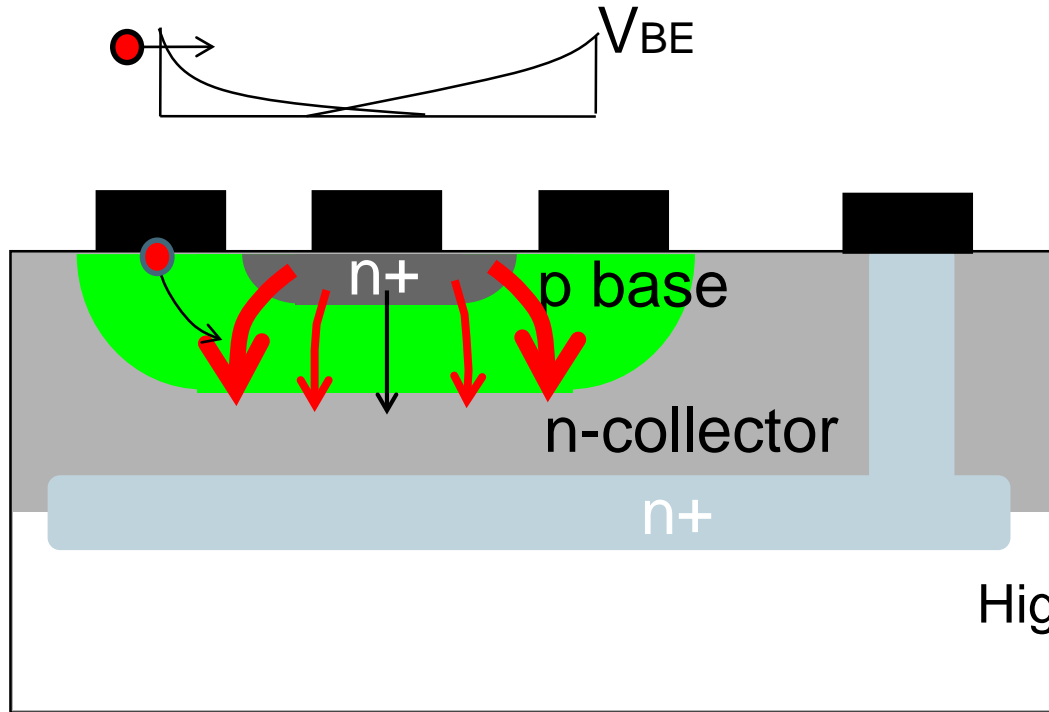
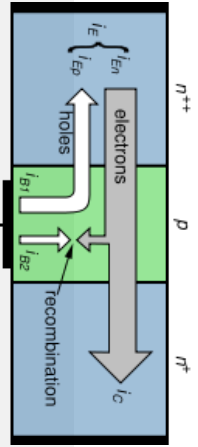
$$\beta = \frac{I_C}{I_B} = \frac{\int J_C(x) dx}{\int J_B(x) dx} = \frac{\int \frac{qD_n}{W_B} \frac{n_{i,B}^2}{N_B} (e^{qV'_{BE}(x)\beta} - 1) dx}{\int \frac{qD_p}{W_E} \frac{n_{i,E}^2}{N_E} (e^{qV'_{BE}(x)\beta} - 1) dx}$$

If the base doping is kept to small values, it will have a high resistance:
Lesser ability to conduct means higher resistance

Sketches from text book

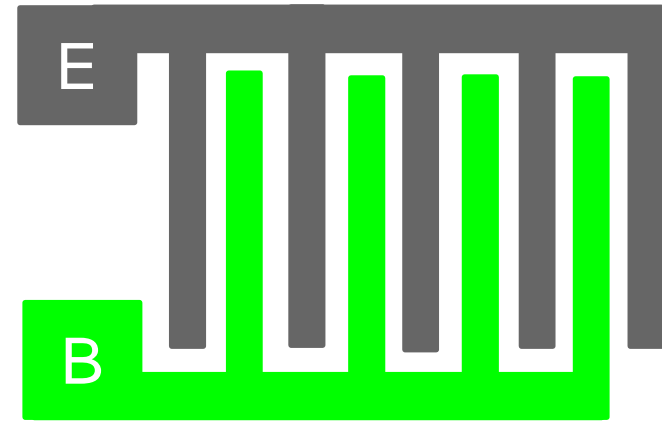


Low Base Doping: Non-uniform Turn-on



Non-uniform current inefficient
High current at the edge can cause burn-out

$$\beta = \frac{I_C}{I_B} = \frac{\int J_C(x) dx}{\int J_B(x) dx} = \frac{\int \frac{qD_n}{W_B} \frac{n_{i,B}^2}{N_B} (e^{qV'_{BE}(x)\beta} - 1) dx}{\int \frac{qD_p}{W_E} \frac{n_{i,E}^2}{N_E} (e^{qV'_{BE}(x)\beta} - 1) dx}$$



Interdigitated designs for almost all high power transistors (E-B distance minimized)

Low Base Doping: Current Crowding

Key facts:

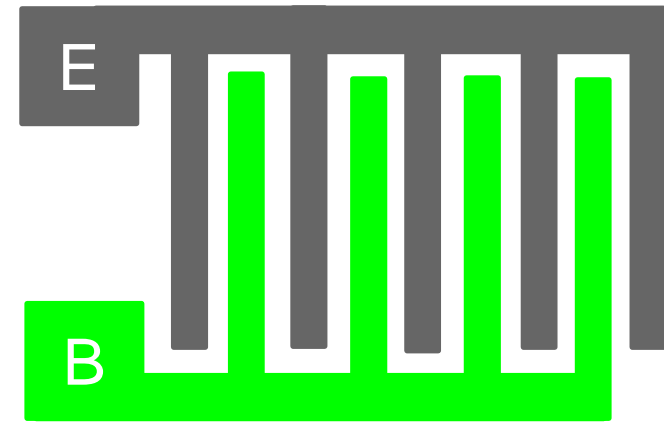
1. Current crowding is due to 2D nature of BJTs
2. It is a function of the doping concentration
3. As base doping concentration increases, resistivity decreases
 - Consequence: Current gain goes smaller
→ Emitter current injection efficiency decreases

$$\beta_{DC} \approx \frac{D_n}{W_B} \frac{W_E}{D_p} \frac{n_{i,B}^2}{n_{i,E}^2} \frac{N_E}{N_B}$$

The larger current density near the emitter may cause localized heating and high injection effects

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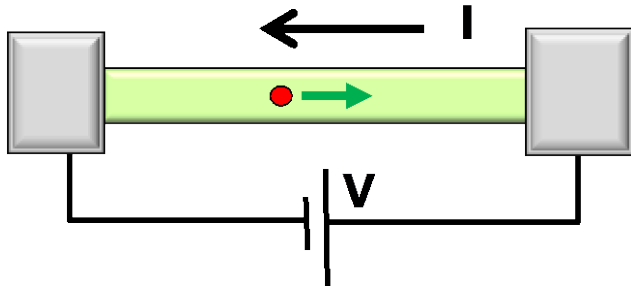
Possible Solution: Emitter widths are fabricated with an inter-digitated design
→ Many narrow emitters connected in parallel to achieve the required emitter area



Interdigitated designs for almost all high power transistors (E-B distance minimized)

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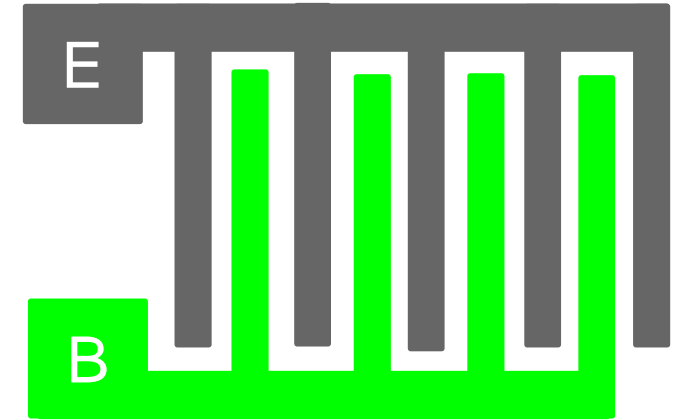
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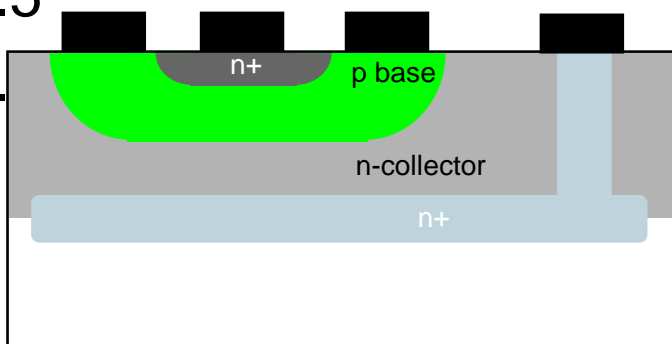
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↑ charge density
 ↑ velocity
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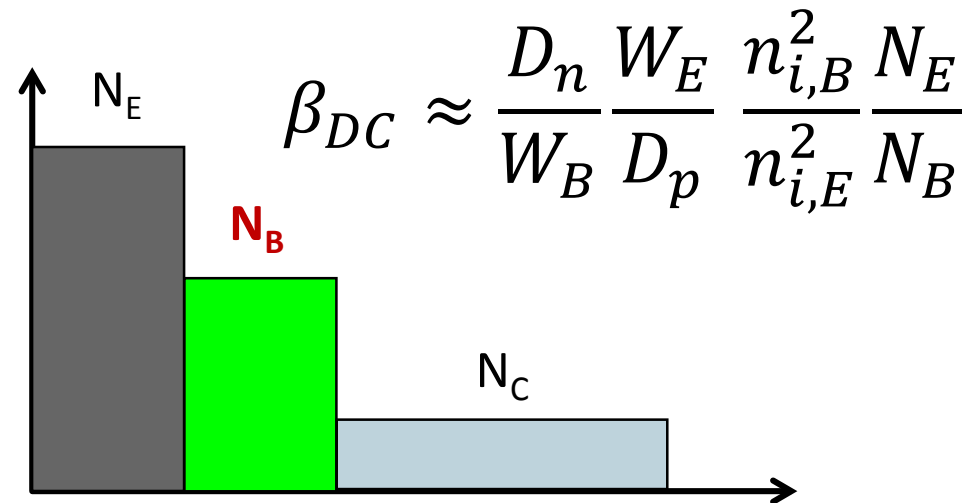


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- 25.2 Considerations for base doping
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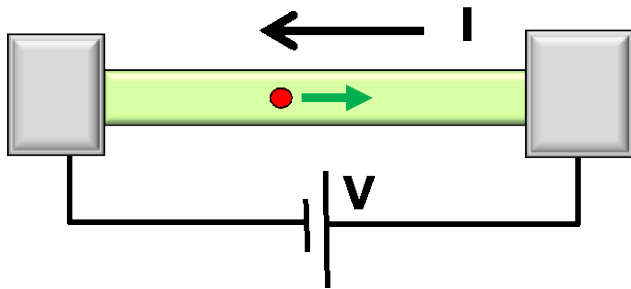


What's wrong with the recipe?



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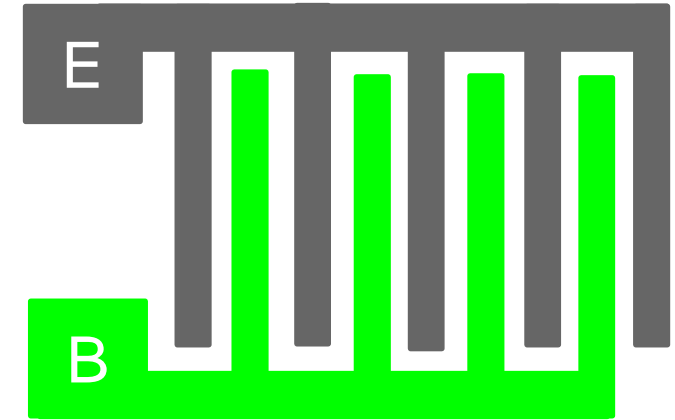
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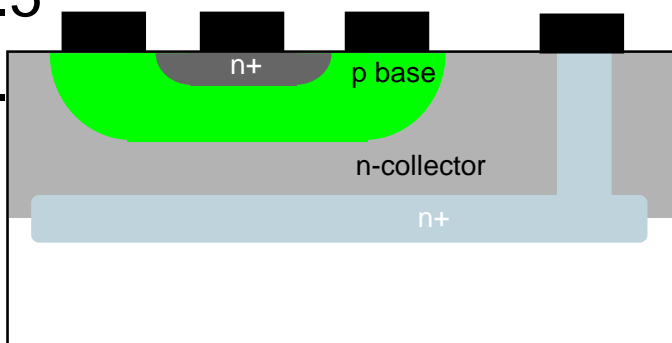
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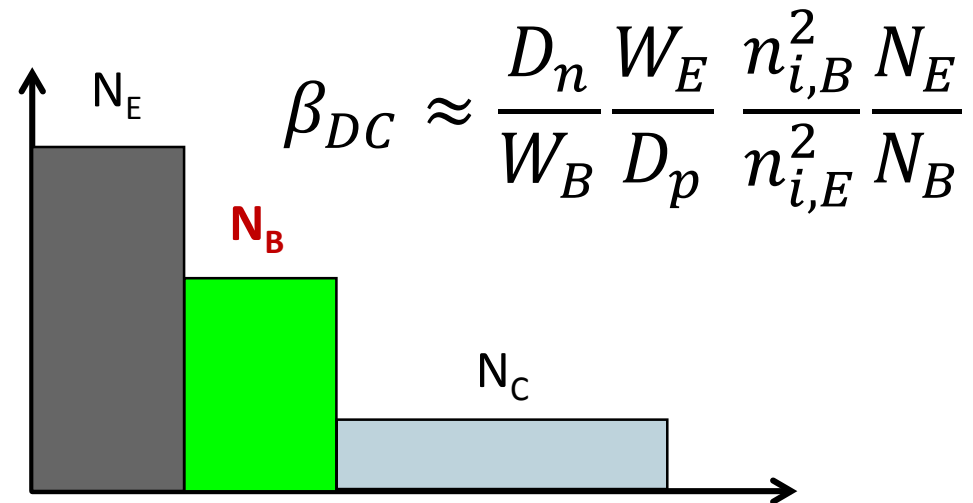


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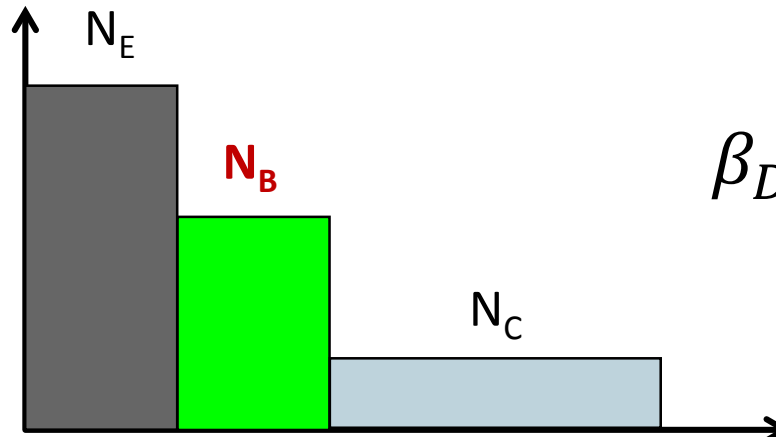
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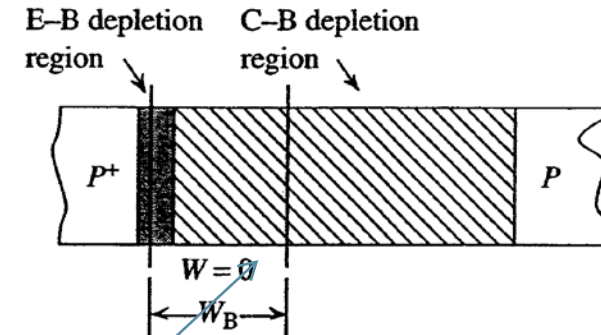
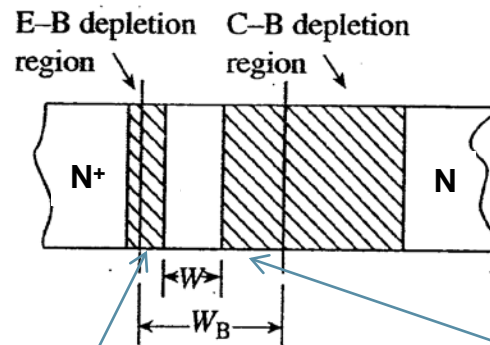
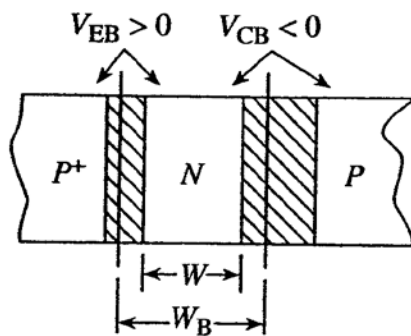
What's wrong with the recipe?



Problem of Low Base Doping: Punch-through



$$\beta_{DC} \approx \frac{D_n}{W_B} \frac{W_E}{D_p} \frac{n_{i,B}^2}{n_{i,E}^2} \frac{N_E}{N_B}$$



$$x_{p,BE} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_E}{N_B (N_E + N_B)} (V_{bi} - V_{BE})}$$

V_{BE} is positive (forward bias)

$$x_{p,BC} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_C}{N_B (N_C + N_B)} (V_{bi} - V_{BC})}$$

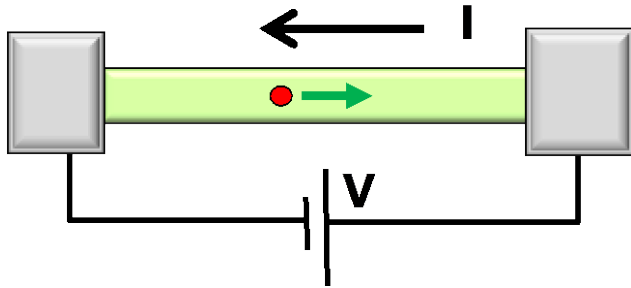
V_{BC} is negative (reverse bias)

$\Rightarrow x_{p,BC}$ grows

Low base doping is not a good idea!

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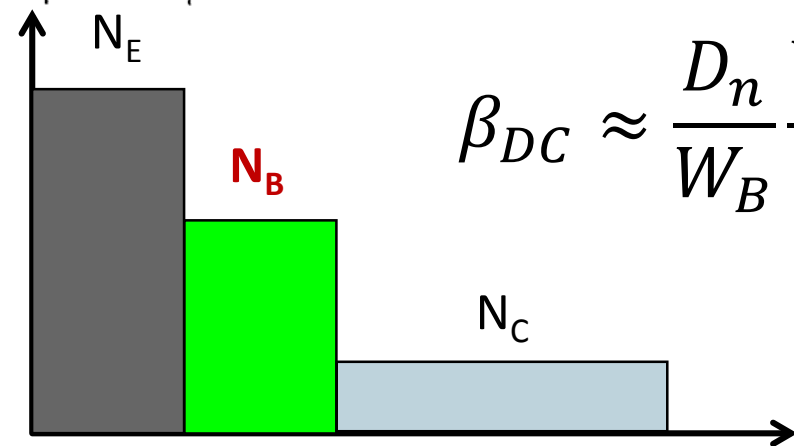
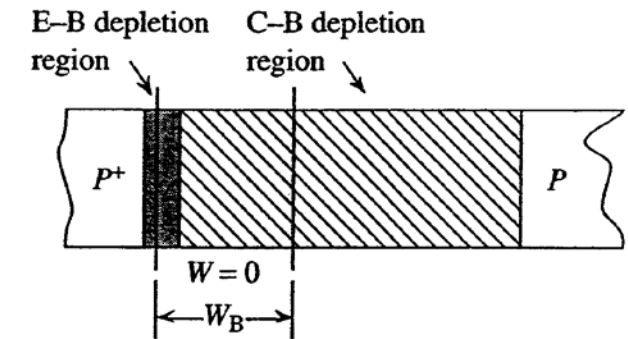
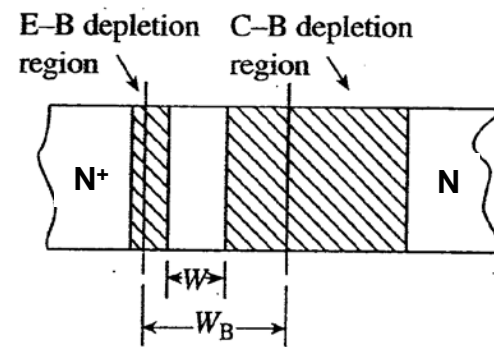
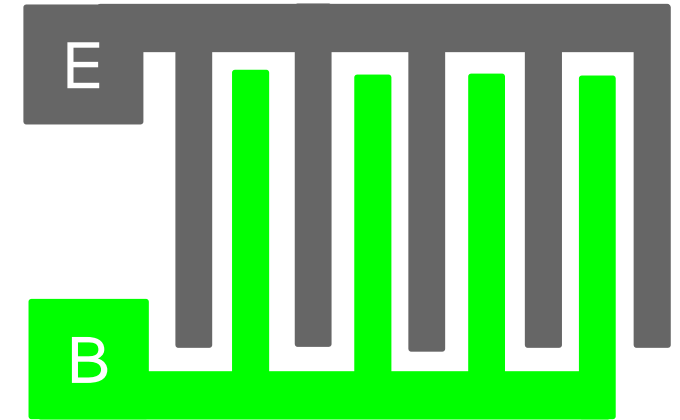
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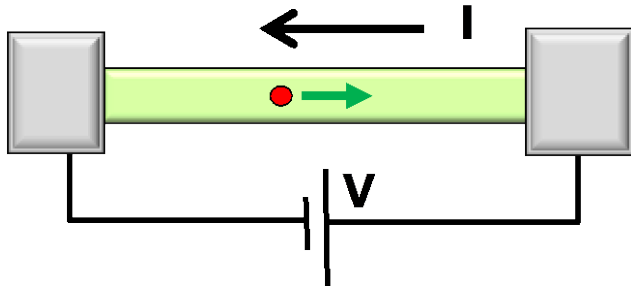
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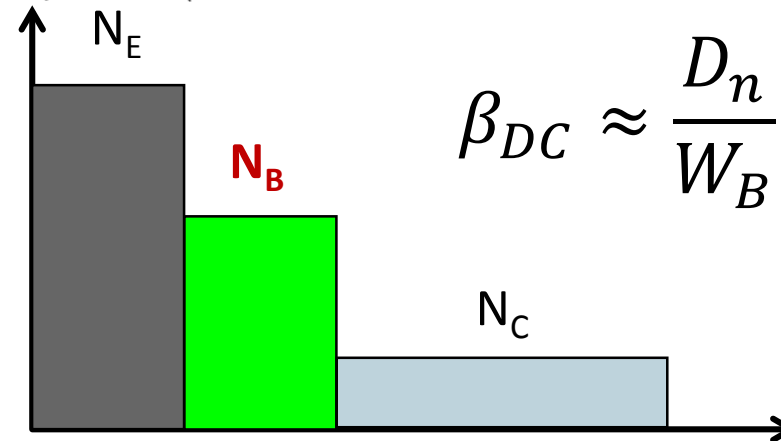
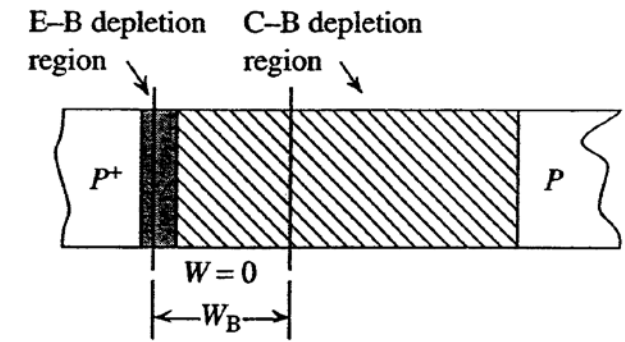
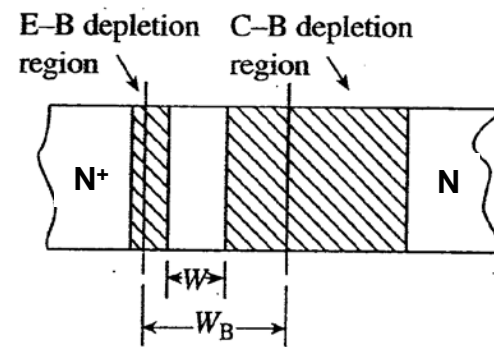
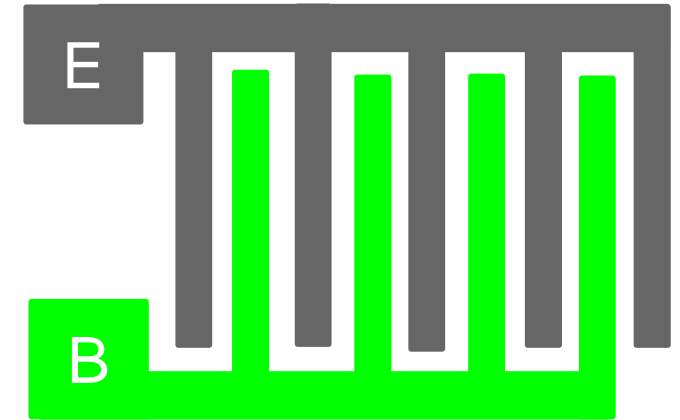
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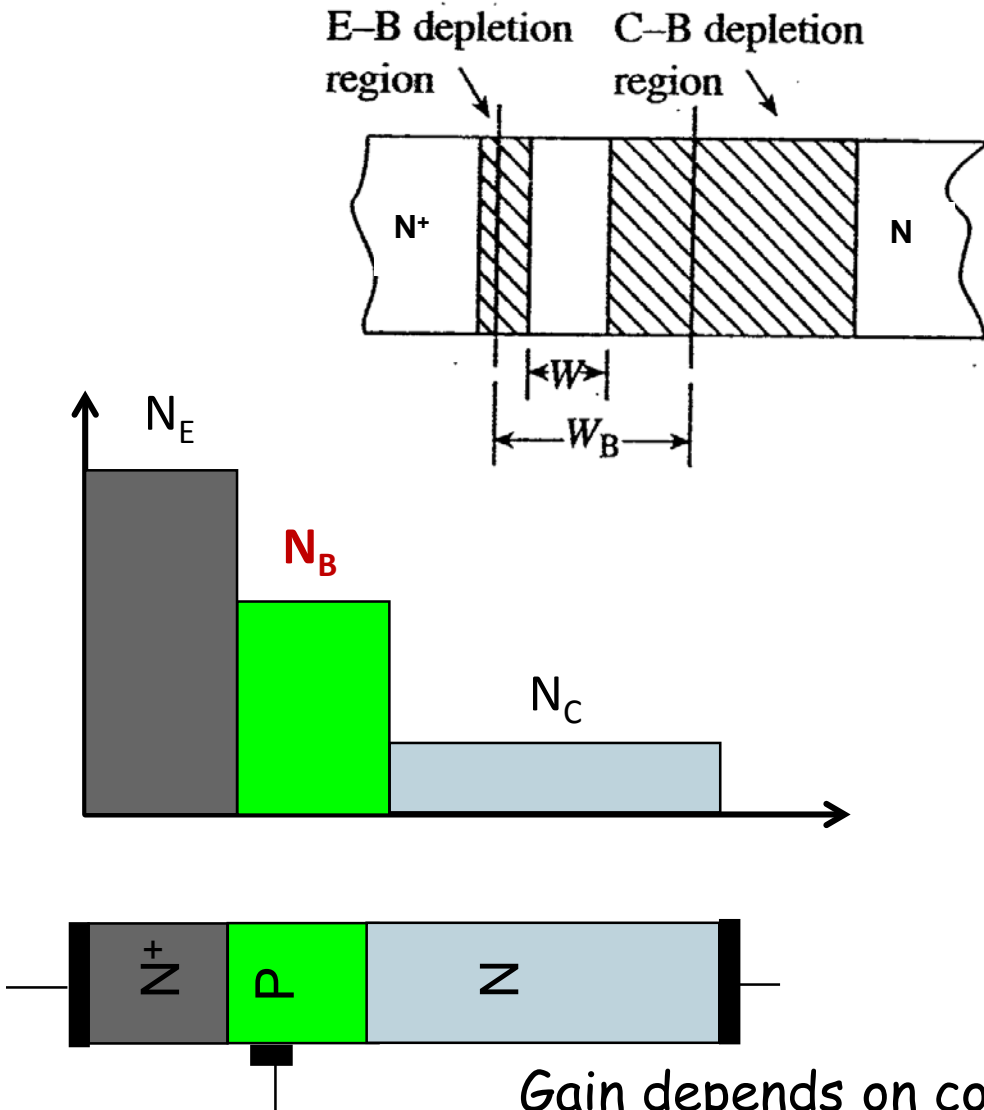
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$$x_{p,BE} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_E}{N_B (N_E + N_B)} (V_{bi} - V_{BE})}$$

$$x_{p,BC} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_C}{N_B (N_C + N_B)} (V_{bi} - V_{BC})}$$

Problem of low Base-doping: Base Width Modulation



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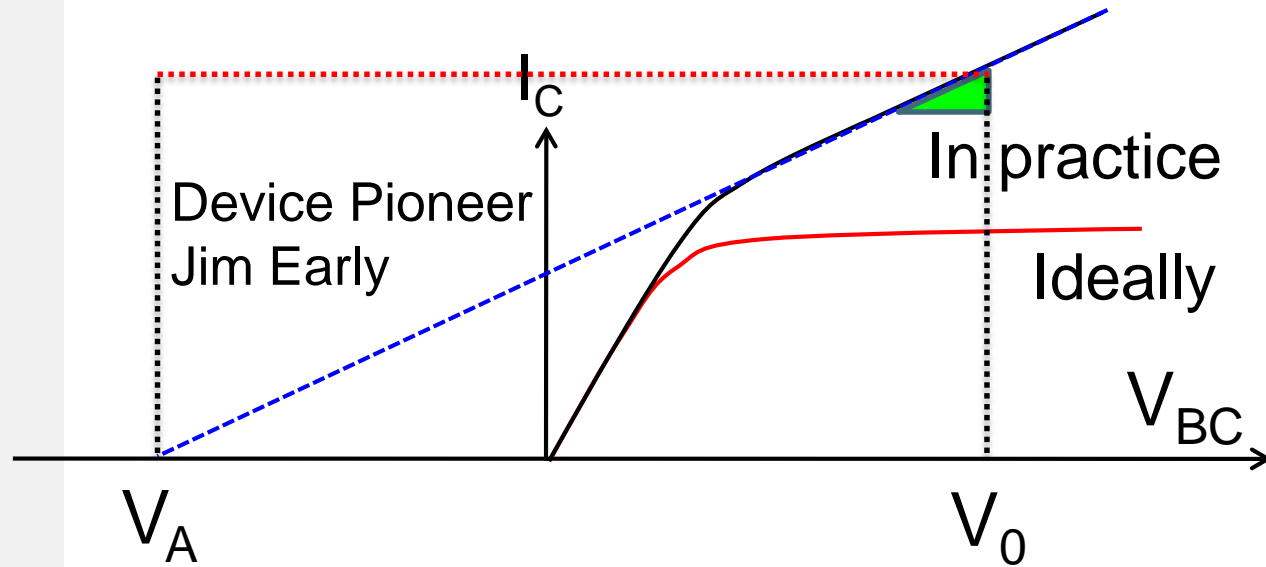
$$\beta_{DC} \approx \frac{D_n}{W_B} \frac{W_E}{D_p} \frac{n_{i,B}^2 N_E}{n_{i,E}^2 N_B}$$

Electrical base region is smaller than the metallurgical region!

$$\beta_{DC} \approx \frac{D_n}{W_B - x_{p,B} - x_{p,C}} \frac{W_E}{D_p} \frac{N_E}{N_B}$$

Gain depends on collector voltage (bad) ...
Depletion region width modulation

Problem of low Base-doping: Base Width Modulation

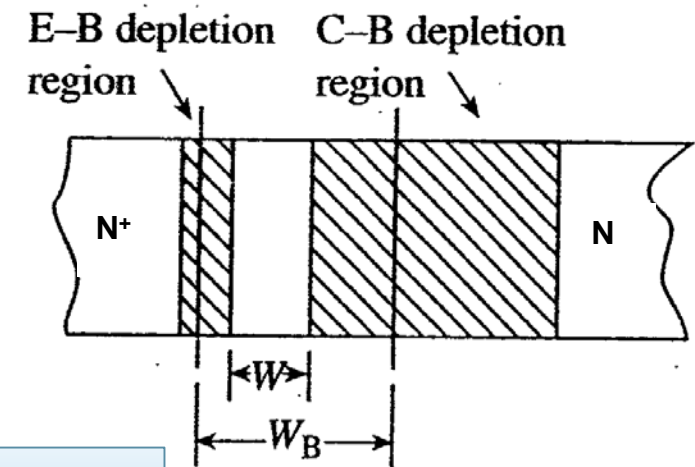


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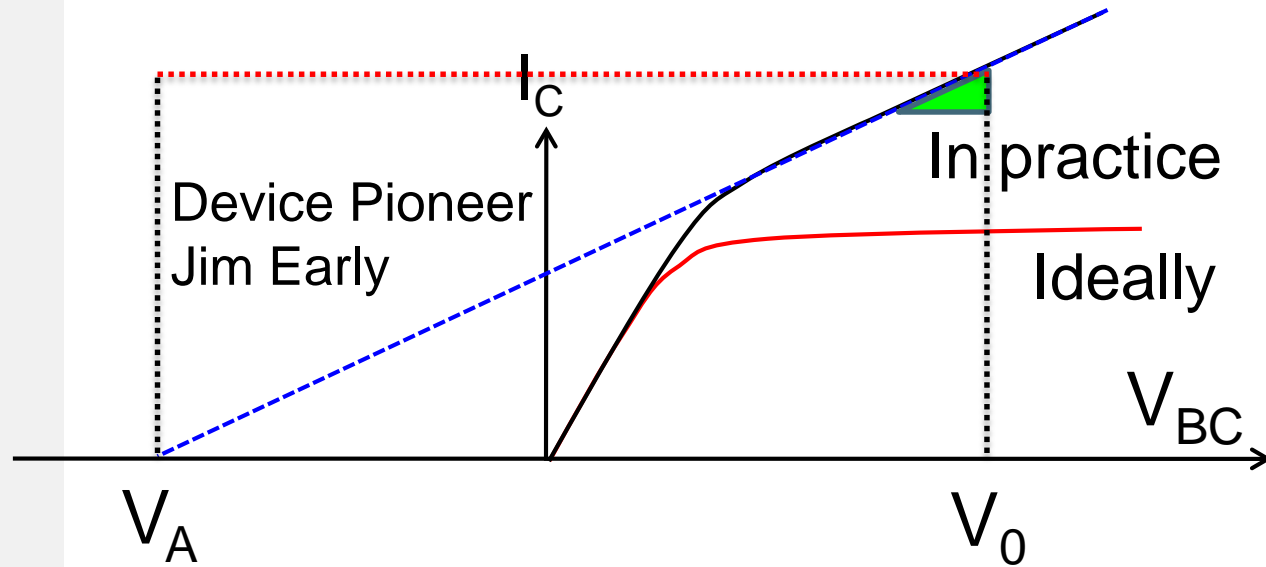
- Fix V_{BE}
- Increase $V_{CE} = V_{BE} + V_{BC}$

=> increase depletion at BC junction
=> increase total current I_C



- Draw a tangential to the transistor $I-V$ at the point of interest.
- The Early voltage: $(V_0 - V_A)$ in figure above

Problem of low Base-doping: Base Width Modulation



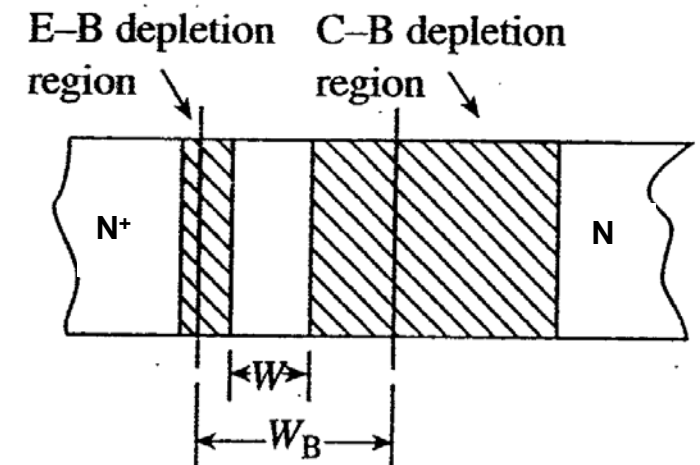
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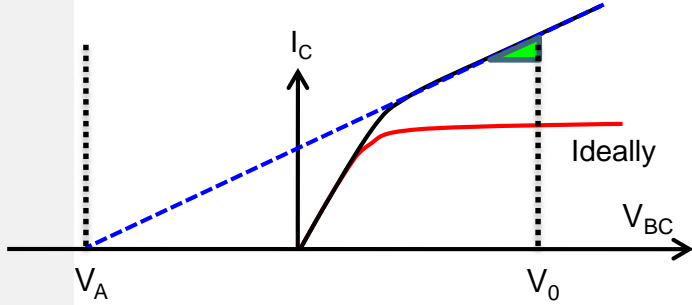
$$\frac{dI_C}{dV_{BC}} = \frac{I_C}{V_{BC} + V_A} \approx \frac{I_C}{V_A}$$

$$\beta_{DC} \approx \frac{D_n}{W_B - x_{p,B} - x_{p,C}} \frac{W_E}{D_p} \frac{n_{i,B}^2}{n_{i,E}^2} \frac{N_E}{N_B}$$

$$I_{n,C} = -\frac{qD_n}{W_B'} \frac{n_{i,B}^2}{N_B} (e^{(qV_{BE}/kT)} - 1) + \frac{qD_n}{W_B'} \frac{n_{i,B}^2}{N_B} (e^{(qV_{BC}/kT)} - 1)$$



Punch-through and Early Voltage



$$\frac{dI_C}{dV_{BC}} = \frac{I_C}{V_{BC} + V_A} \approx \frac{I_C}{V_A}$$

$$\begin{aligned} \frac{dI_C}{dV_{BC}} &= \frac{dI_C}{d(qN_B W_B)} \frac{d(qN_B W_B)}{dV_{BC}} \\ &= \frac{1}{qN_B} \left(\frac{dI_C}{dW_B} \right) \left[\frac{dQ_B}{dV_{BC}} \right] \\ &= -\frac{1}{qN_B} \left(\frac{I_C}{W_B} \right) C_{CB} \end{aligned}$$

$$\begin{aligned} -\frac{C_{CB}}{qN_B} \frac{I_C}{W_B} &\approx \frac{I_C}{V_A} \\ \Rightarrow V_A &= -\frac{qN_B W_B}{C_{CB}} \rightarrow \infty \end{aligned}$$

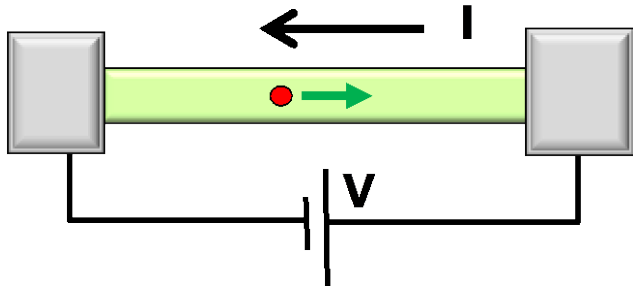
Need higher N_B and W_B or ...

$$C_{CB} = \frac{K_s \epsilon_0}{x_{n,C} + x_{p,B}}$$

$$\begin{aligned} I_C &= \frac{qD_n}{W_B} \frac{n_{i,B}^2}{N_B} (e^{qV_{BE}\beta} - 1) + \frac{qD_n}{W_B} \frac{n_{i,B}^2}{N_B} (e^{qV_{BC}\beta} - 1) \\ &= \frac{\xi}{W_B} \end{aligned}$$

$$\frac{dI_C}{dW_B} = \frac{d}{dW_B} \left(\frac{\xi}{W_B} \right) = -\frac{\xi}{W_B^2} = -\frac{I_C}{W_B}$$

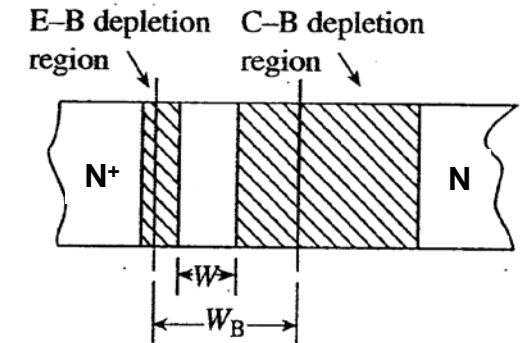
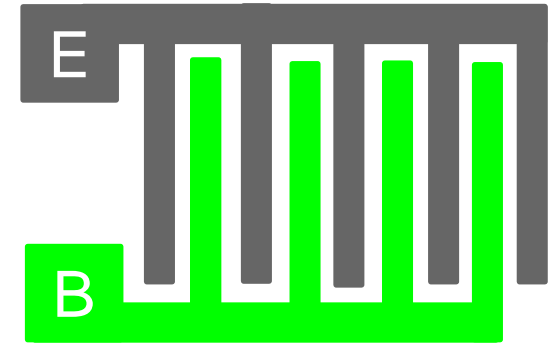
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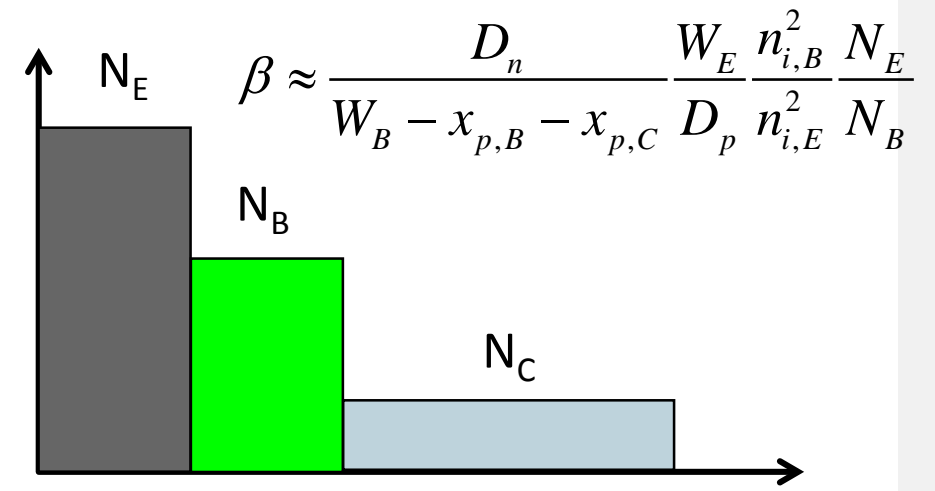
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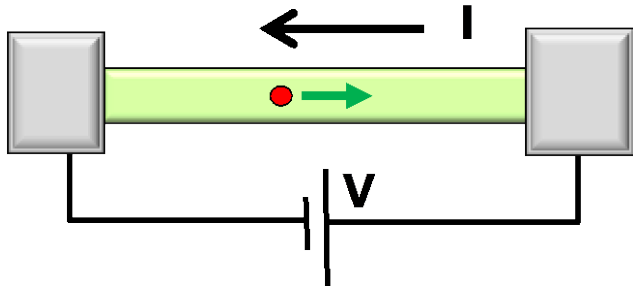
$$x_{p, BC} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_C}{N_B (N_C + N_B)} (V_{bi} - V_{BC})}$$

$$V_A = -\frac{q N_B W_B}{C_{CB}} \quad C_{CB} = \frac{K_s \epsilon_0}{x_{n,C} + x_{p,B}}$$



Section 25

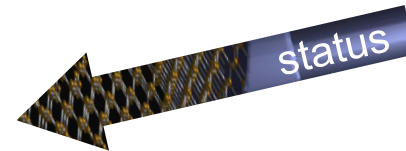
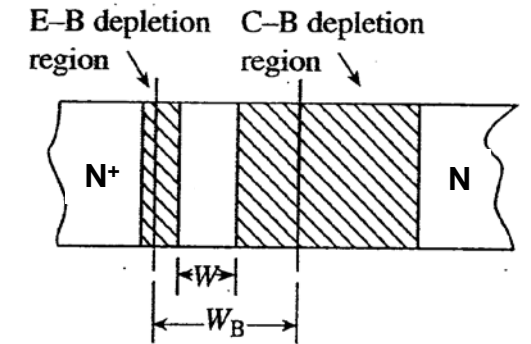
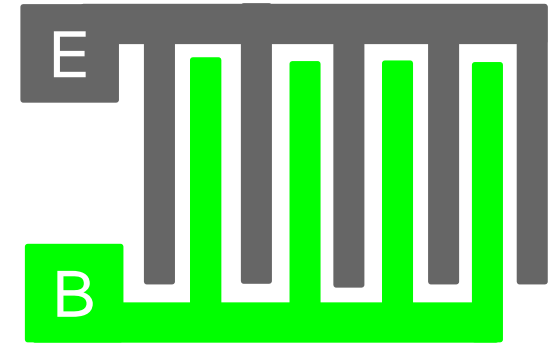
Bipolar Junction Transistor - Design



$$I = G \times V$$

$$= q \times n \times v \times A$$

↑ charge density
 ↑ velocity
 area



- > • 25.1 Current gain in BJTs
- > • 25.2 Base Doping Design
 - » Current Crowding – Non-Uniform Turn-On
 - » Punch-through
 - » Base Width Modulation
- > • 25.3 Collector Doping Design (Kirk Effect, Base Pushout)

> • 25.4

> • 25.5

> • 25.6

$$x_{p, BE} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_E}{N_B (N_E + N_B)} (V_{bi} - V_{BE})}$$

$$x_{p, BC} = \sqrt{\frac{2k_s \epsilon_0}{q} \frac{N_C}{N_B (N_C + N_B)} (V_{bi} - V_{BC})}$$

$$V_A = -\frac{q N_B W_B}{C_{CB}} \quad C_{CB} = \frac{K_s \epsilon_0}{x_{n,C} + x_{p,B}}$$

