

Spring 2019 Purdue University

ECE 255: L33

High Frequency Response I

(Sedra and Smith, 7th Ed., Sec. 10.2)

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Lundstrom: 2019

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Announcements

HW10 Due 5:00 PM Friday, April 19 in EE-209 dropbox

LTSpice Project III Due 5:00 PM Wed, April 17

LTSpice Help Session to be announced

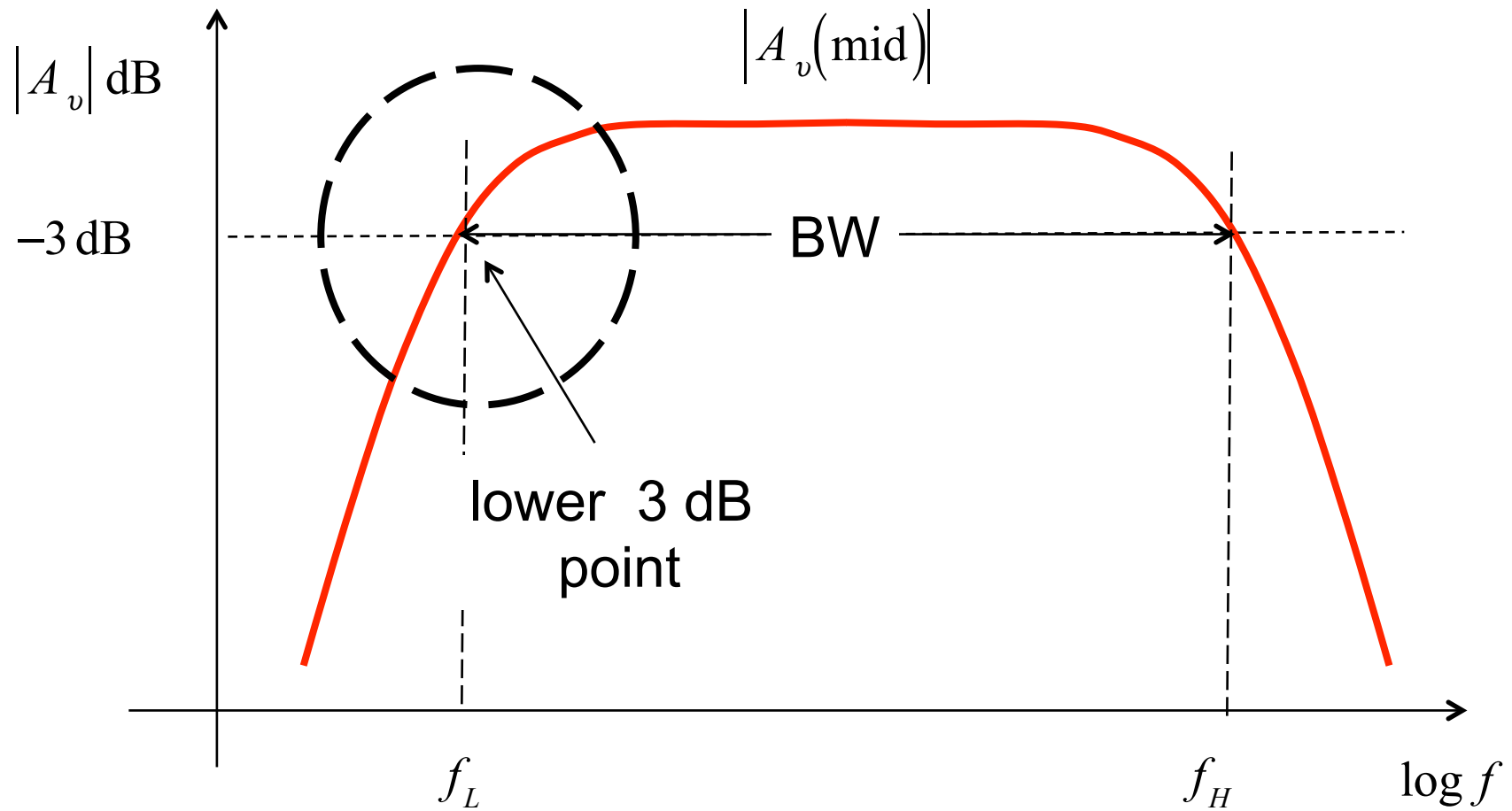
Practice Final Exam posted

No Office Hours today (Lundstrom)

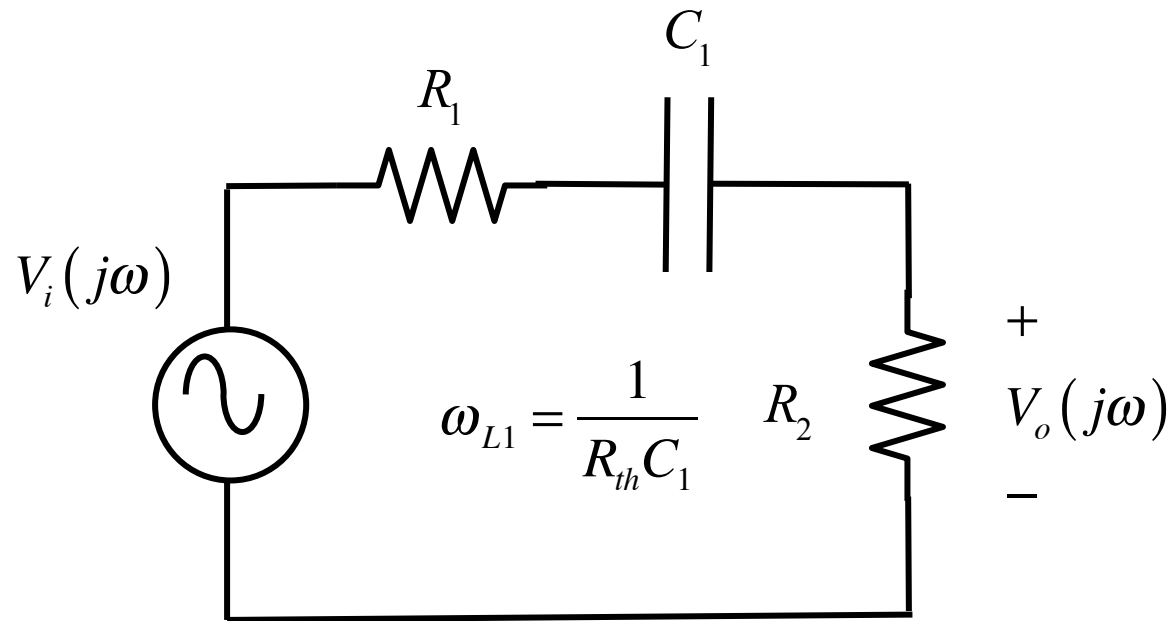
Outline

- 1) **LF review**
- 2) Low pass filter / STC circuits
- 3) High freq model for MOSFETs
- 4) High freq models for BJTs

Bode plot



Short-circuit time constant method



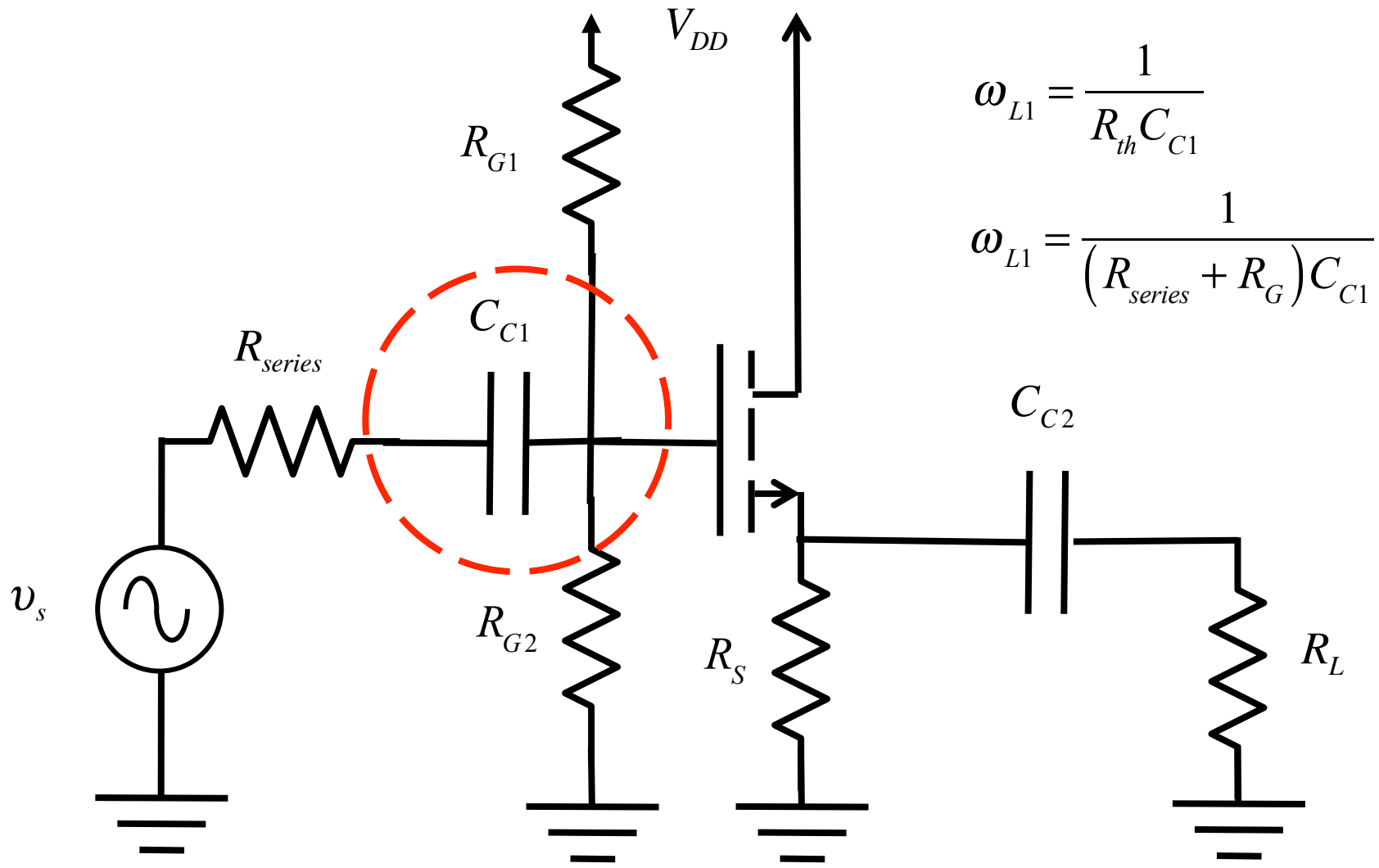
The corner frequency (the pole) is one over a time constant – just find the RC time constant.

While we compute this corner frequency, we assume that the other C's are shorted – this produces a STC circuit.

$$\omega_L \approx \omega_{L_{\max}}$$

$$\omega_L < \omega_{L1} + \omega_{L2} + \omega_{L3} + \dots$$

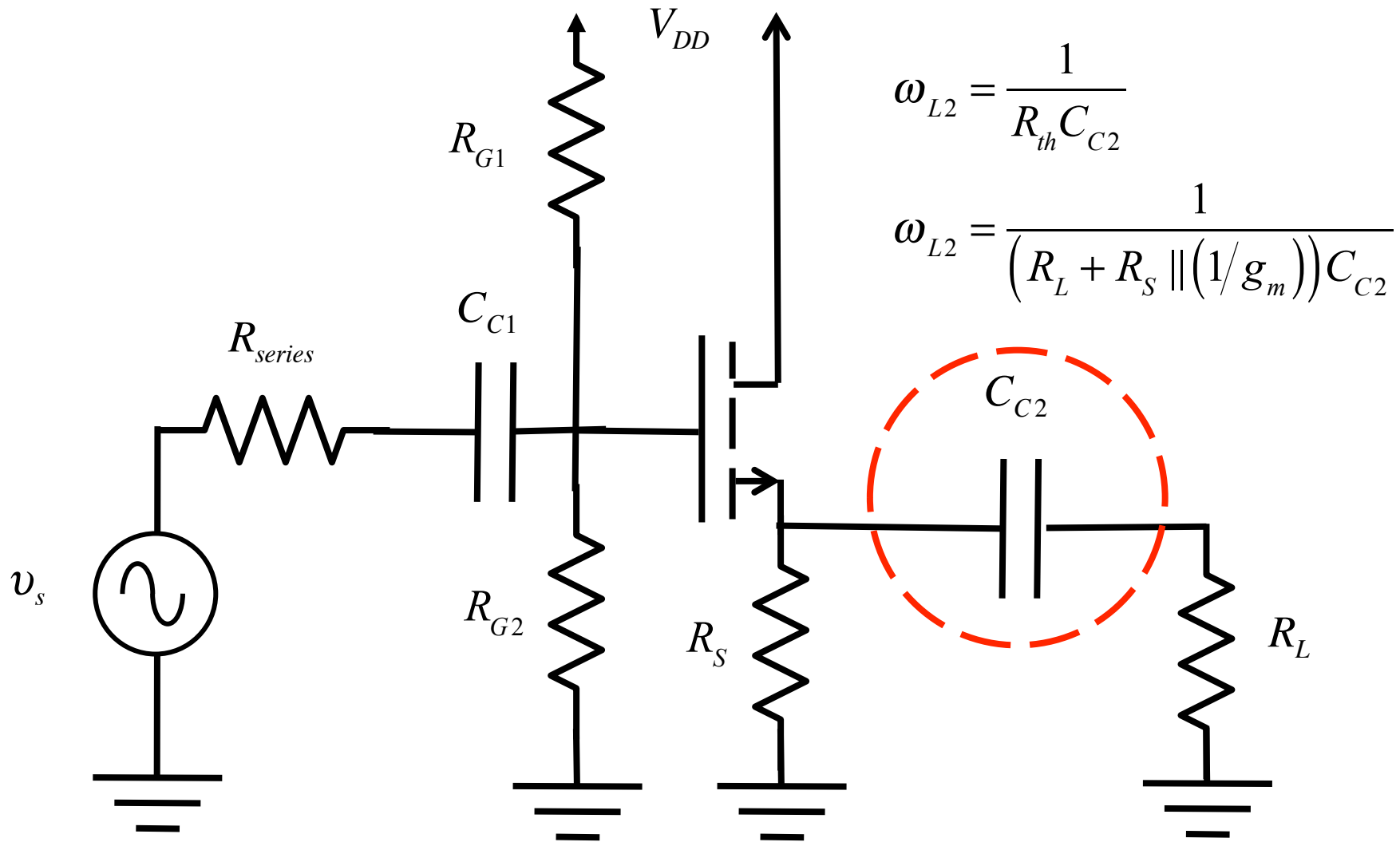
Example: Common Drain Amplifier



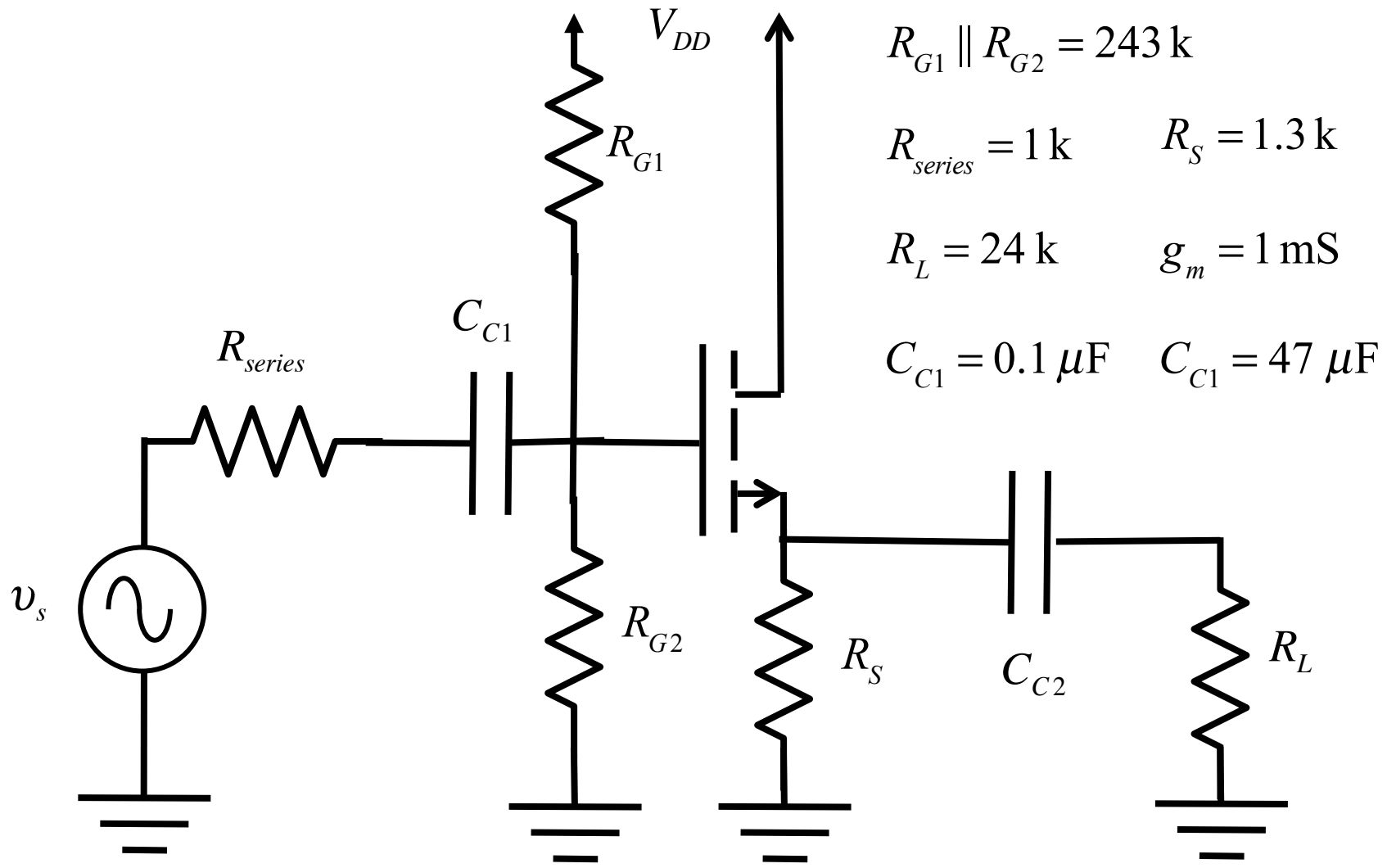
$$\omega_{L1} = \frac{1}{R_{th} C_{C1}}$$

$$\omega_{L1} = \frac{1}{(R_{series} + R_G) C_{C1}}$$

Example: Common Drain Amplifier



Compute the LF corner freq.



Compute the LF corner freq.

$$\omega_{L1} = \frac{1}{(1 + 243) \times 10^3 \times 0.1 \times 10^{-6}} = 41$$

$$\omega_{L2} = \frac{1}{(24 + 1.3 \parallel 1) \times 10^3 \times 47 \times 10^{-6}} = 0.87$$

$$\omega_L \approx \omega_{L1} = 41 = 2\pi f_L$$

$$f_L = 6.5 \text{ Hz}$$

$$R_{G1} \parallel R_{G2} = 243 \text{ k}$$

$$R_{series} = 1 \text{ k} \quad R_S = 1.3 \text{ k}$$

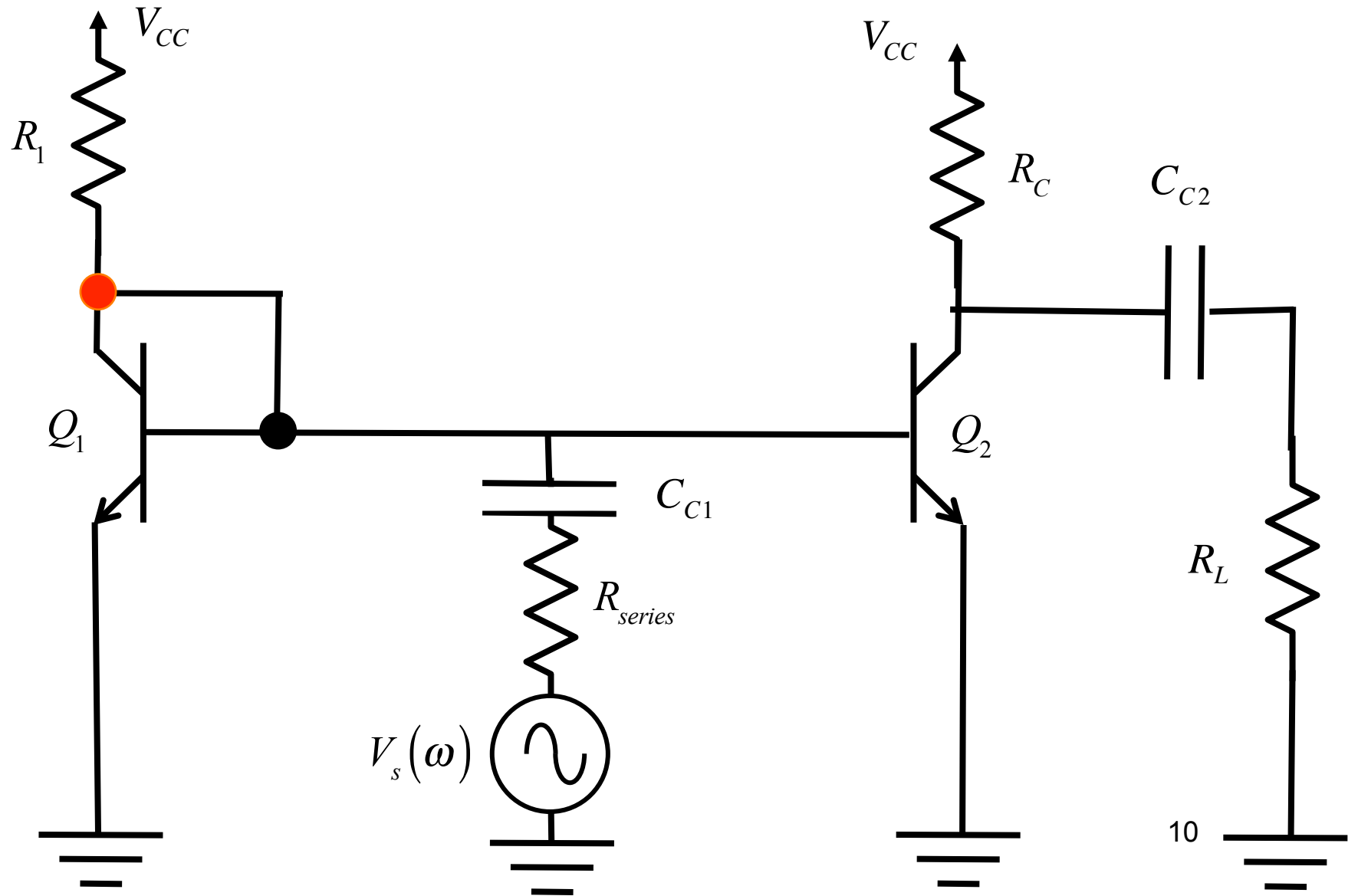
$$R_L = 24 \text{ k} \quad g_m = 1 \text{ mS}$$

$$C_{C1} = 0.1 \mu\text{F} \quad C_{C2} = 47 \mu\text{F}$$

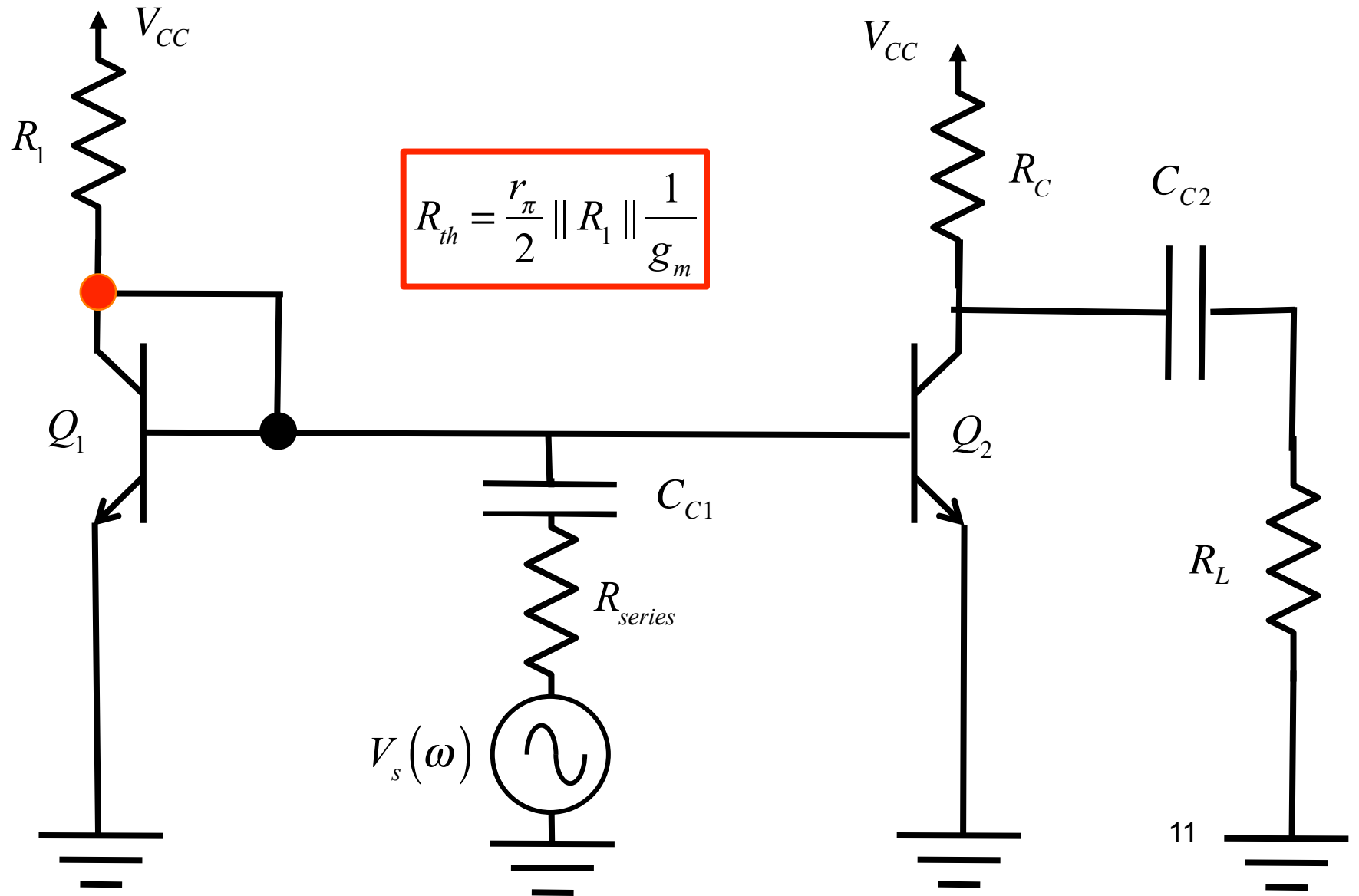
$$\omega_{L1} = \frac{1}{(R_{series} + R_G) C_{C1}}$$

$$\omega_{L2} = \frac{1}{(R_L + R_S \parallel (1/g_m)) C_{C2}}$$

Find the Thevenin eq. resistance for C_1



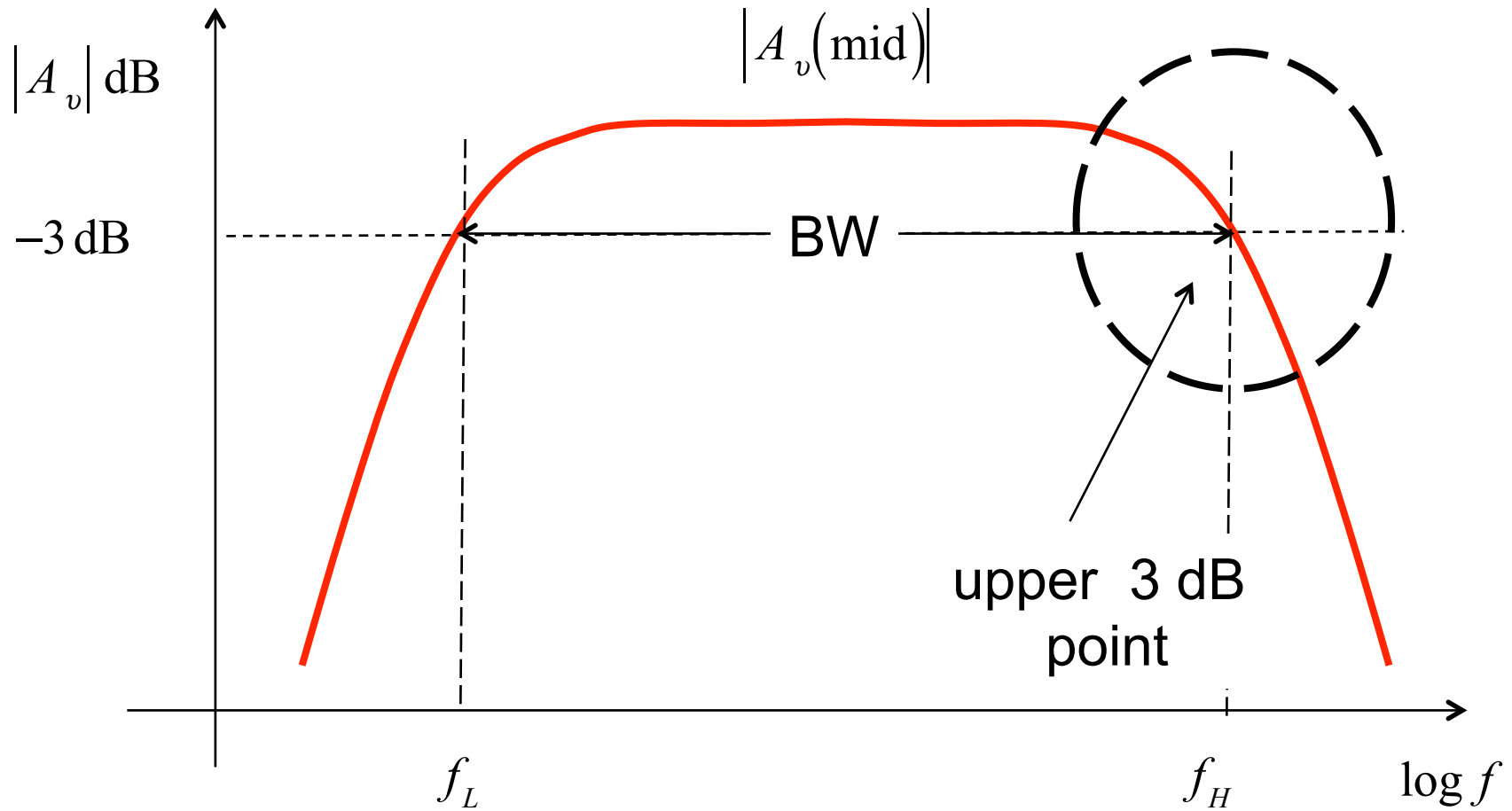
Thevenin eq. resistance for C_1



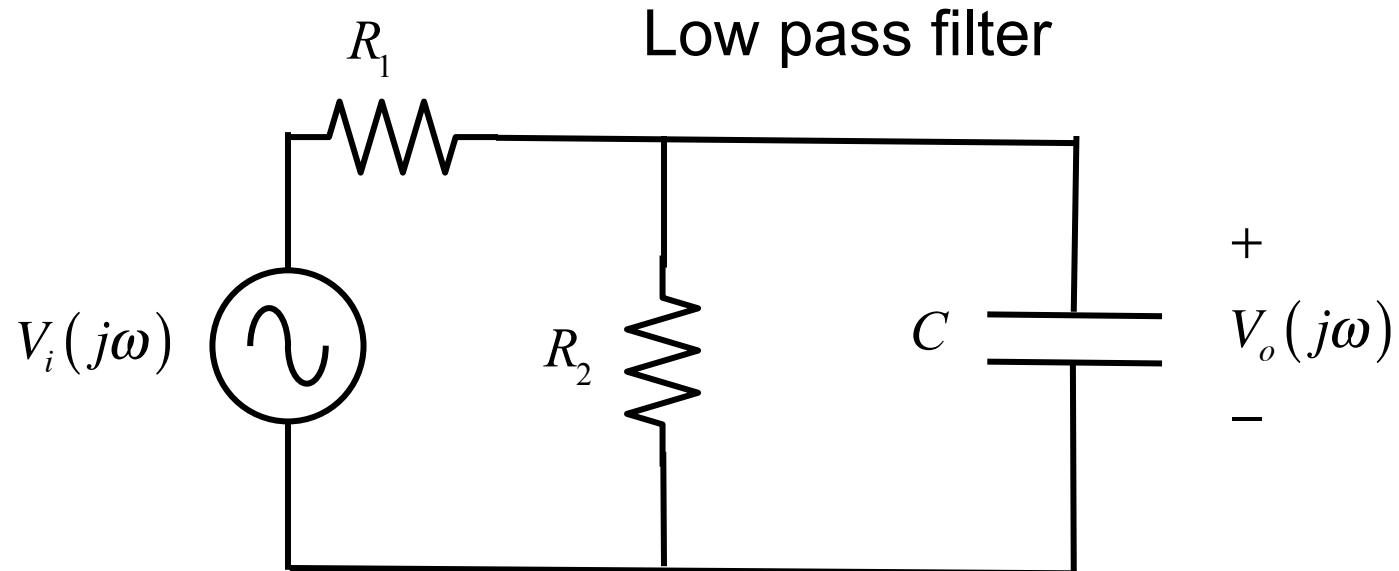
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Bode plot



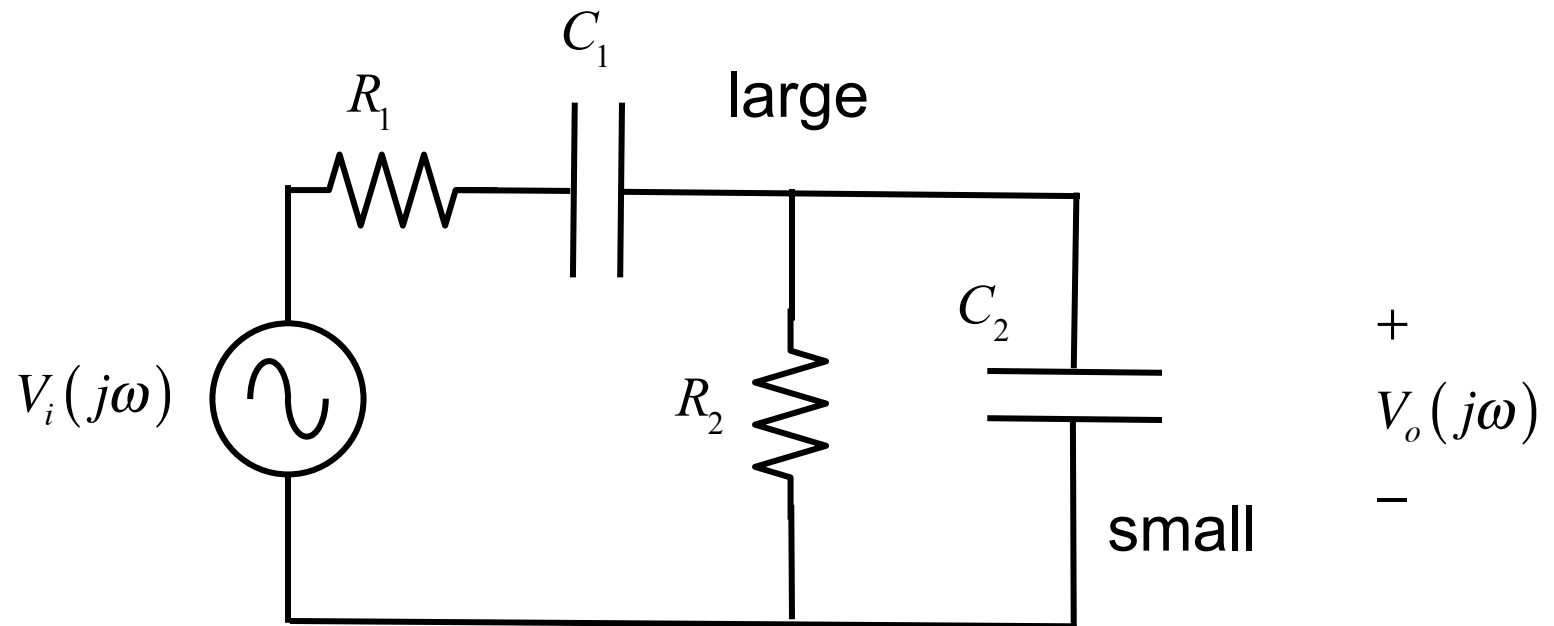
STC



$$T(j\omega) = \frac{Y_1}{Y_1 + Y_2} = \frac{1/R_1}{1/R_1 + (1/R_2 + j\omega C)}$$

$$T(j\omega) = \frac{T_{mid}}{1 + j\omega/\omega_H} \quad \omega_H = \frac{1}{(R_1 \parallel R_2)C} = \frac{1}{R_{th}C}$$

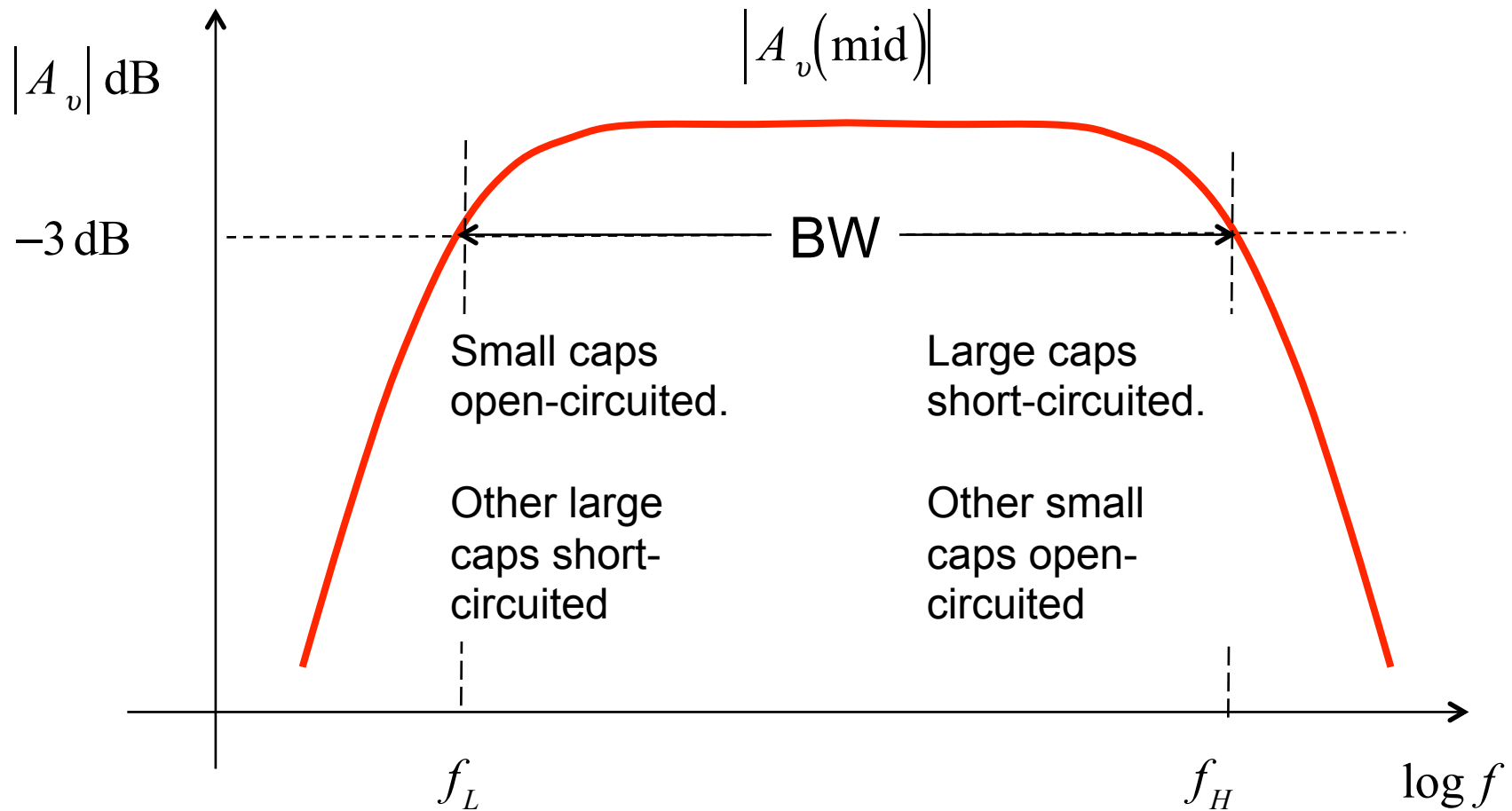
How would we analyze **this** circuit?



1) $\omega_L = \frac{1}{(R_1 + R_2)C_1}$ C_2 open

2) $\omega_H = \frac{1}{(R_1 \parallel R_2)C_2}$ C_1 short

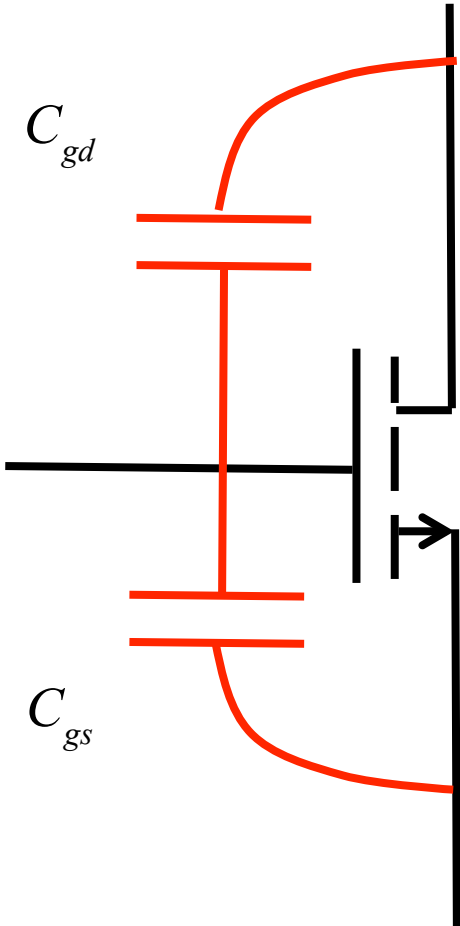
Bode plot



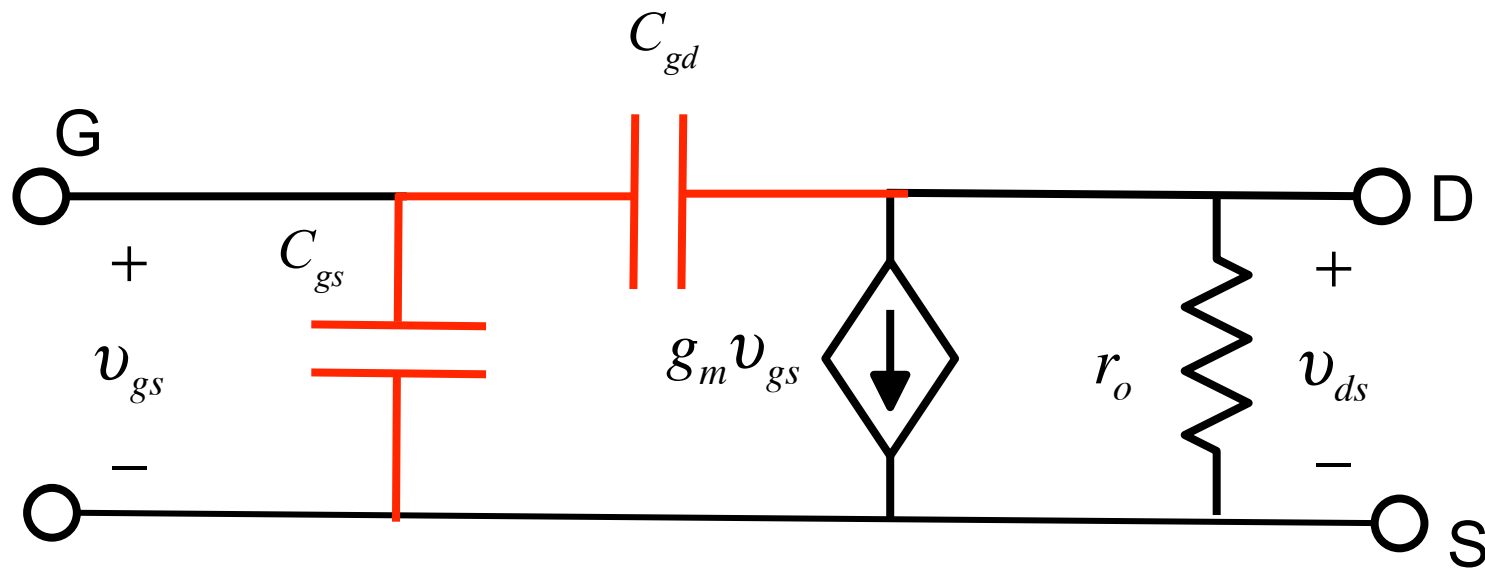
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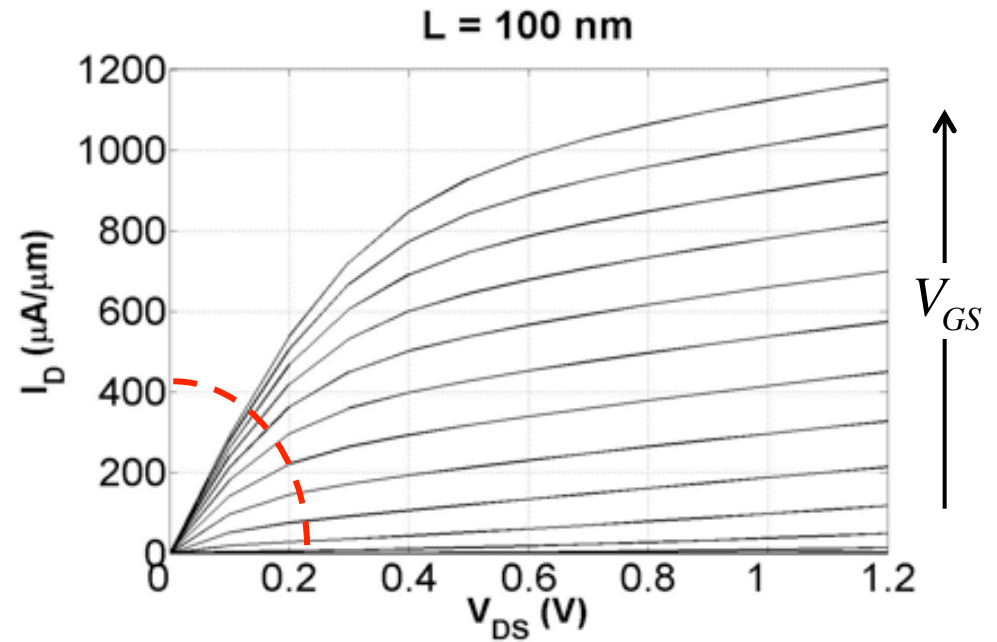
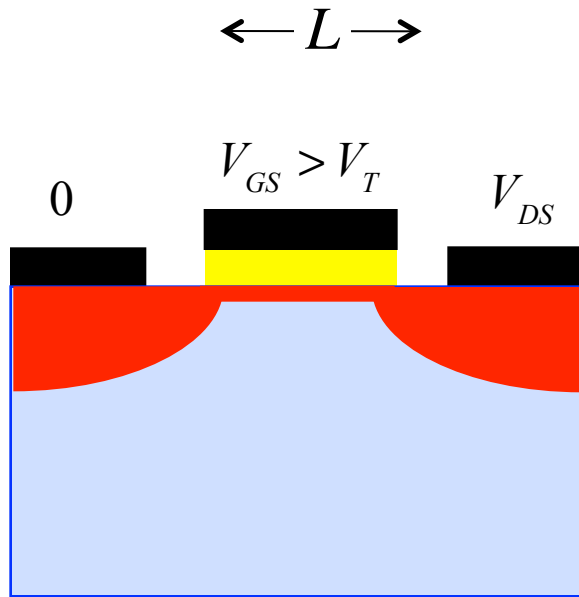
The answer



The hf hybrid pi model

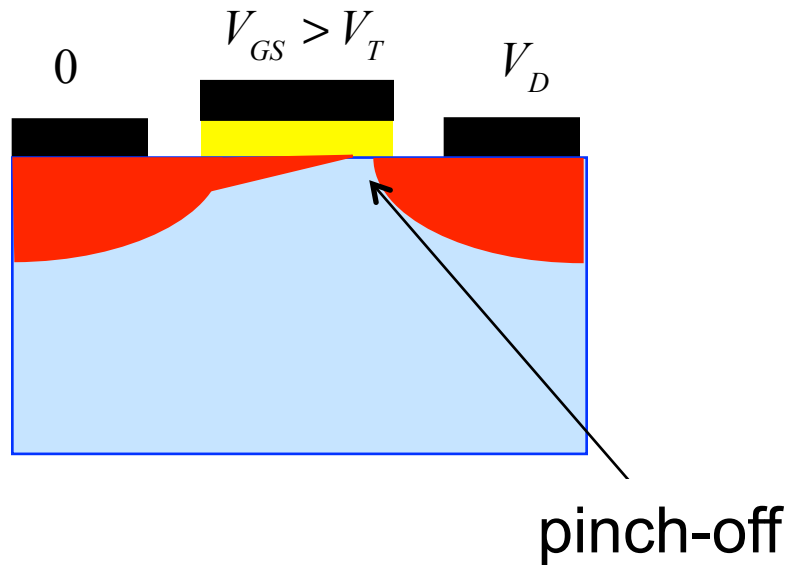


MOSFET under low V_{DS}



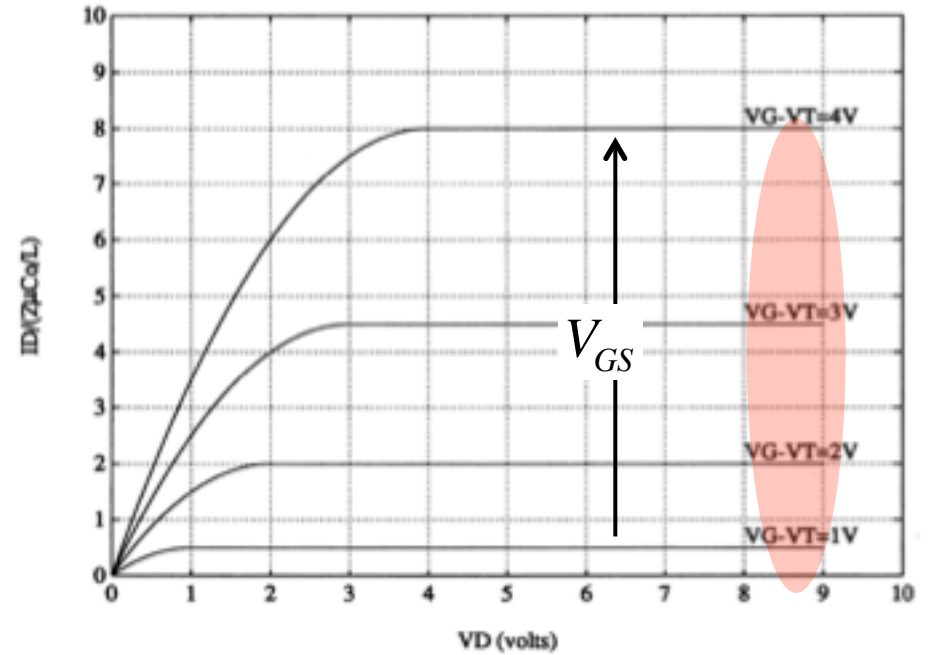
$$C \equiv \frac{K_r \epsilon_0}{t} \quad C_{gs} = \frac{WL}{2} \frac{K_{ox} \epsilon_0}{t_{ox}} = C_{gd}$$

MOSFET under high V_{DS}



$$C_{gs} = \frac{2WLK_{ox}\epsilon_0}{3t_{ox}}$$

$$C_{gd} \approx 0$$

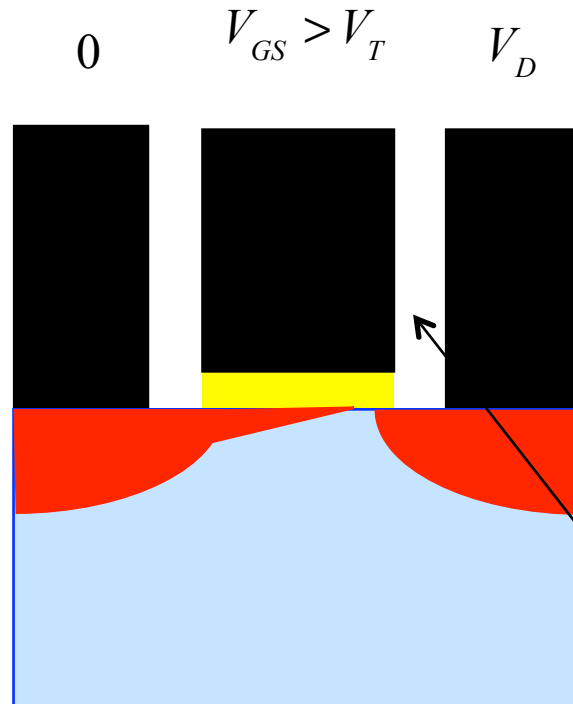


Gate-drain overlap/fringing field capacitance

$$C_{gs} = \frac{2WLK_{ox}\epsilon_0}{3t_{ox}}$$

$$C_{gd} > 0$$

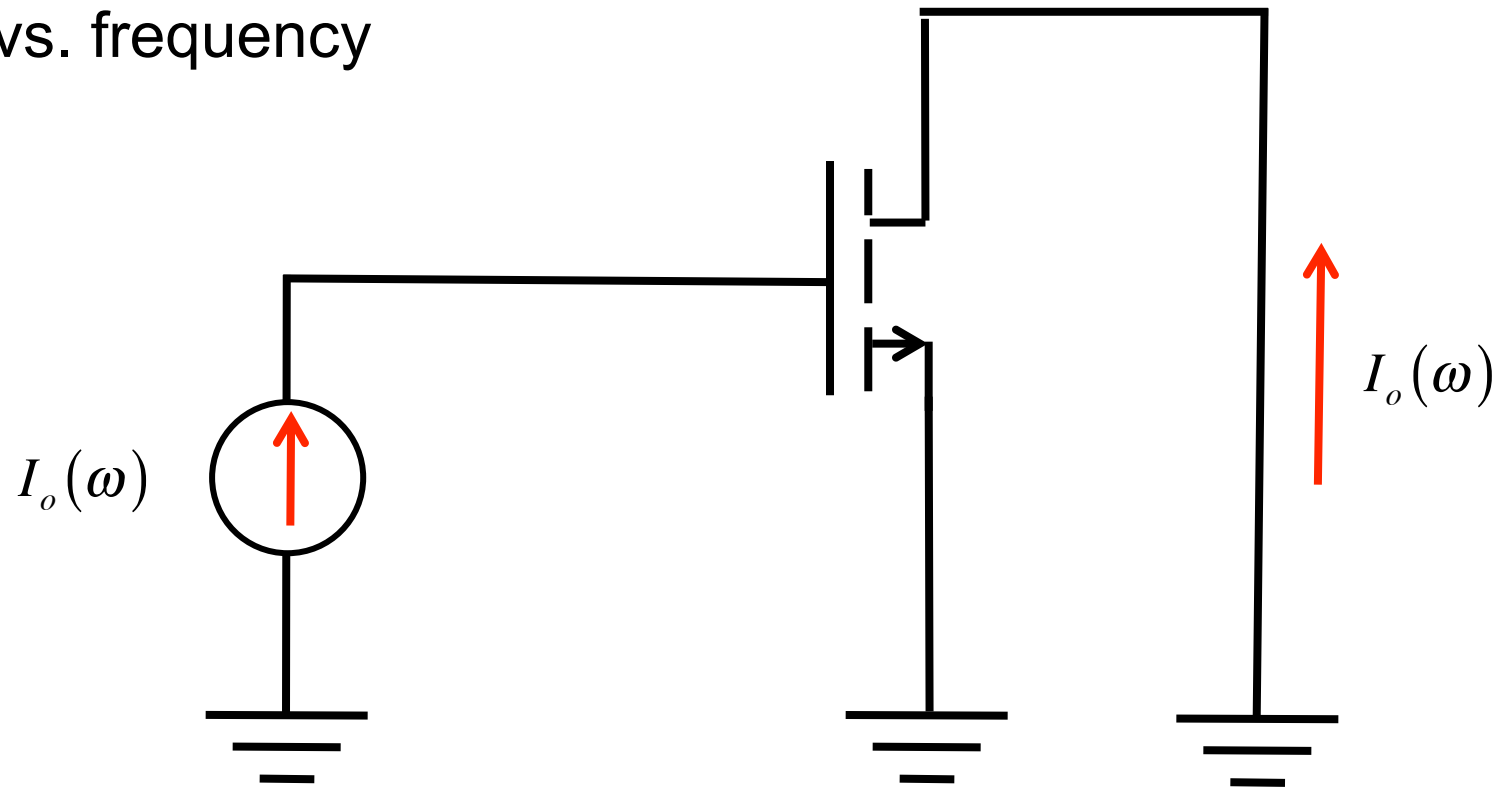
Miller capacitance!



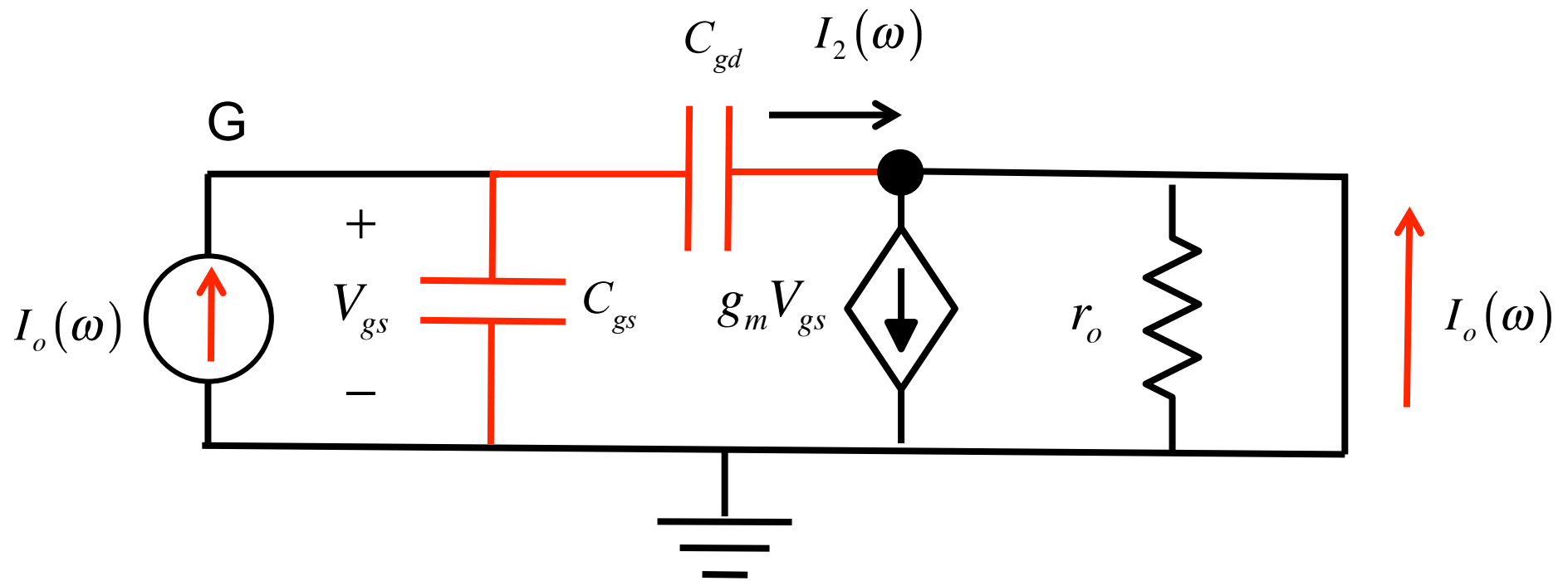
Two plates separated by distance.

Characterizing a MOSFET

Short circuit current gain vs. frequency



The hf hybrid pi model



$$I_2 + I_o = g_m V_{gs}$$

$$I_o = (g_m - j\omega C_{gd}) V_{gs}$$

$$\frac{I_o}{I_i} = \frac{g_m}{j\omega(C_{gs} + C_{gd})} \left(1 - j\omega C_{gd}/g_m\right)$$

$$I_o = g_m V_{gs} - I_2$$

$$V_{gs} = I_i \frac{1}{j\omega(C_{gs} + C_{gd})}$$

$$\frac{I_o}{I_i} \approx \frac{g_m}{j\omega(C_{gs} + C_{gd})}$$

$$I_2 = V_{gs} j\omega C_{gd}$$

Characterizing a MOSFET

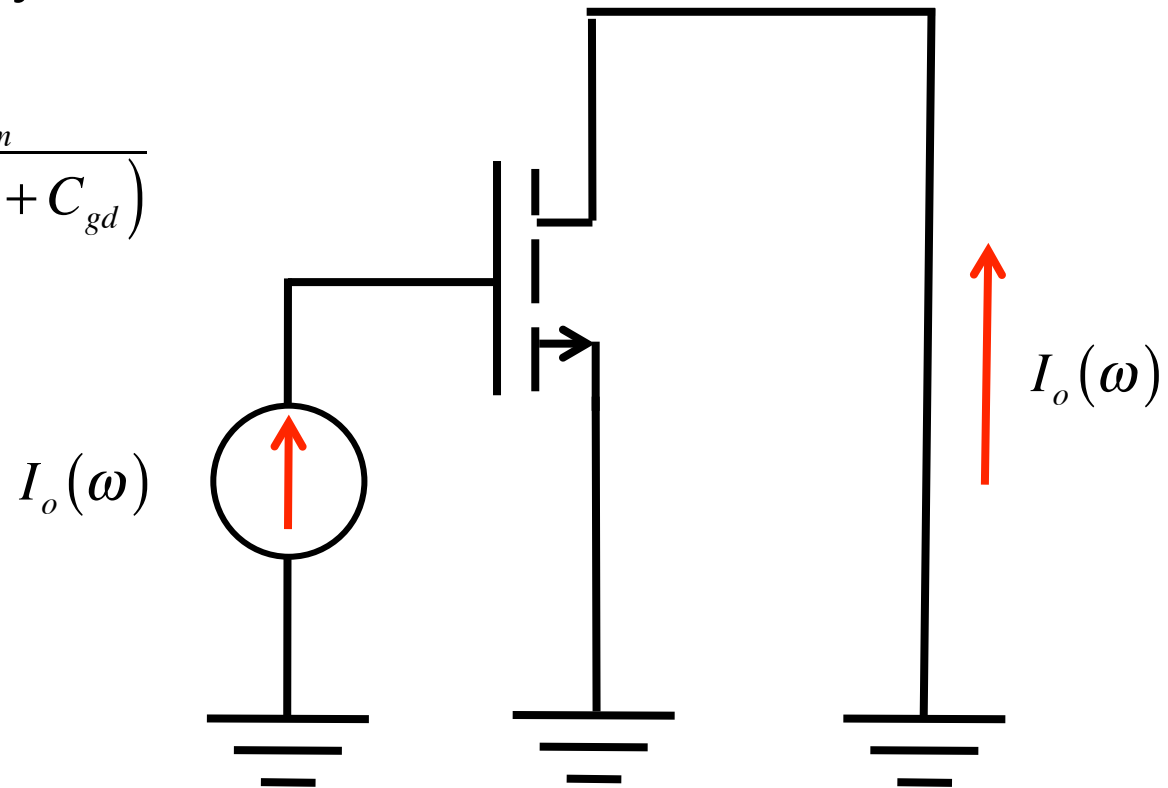
Short circuit current
gain vs. frequency

$$\beta(\omega) = \frac{I_o}{I_i} \approx \frac{g_m}{j\omega(C_{gs} + C_{gd})}$$

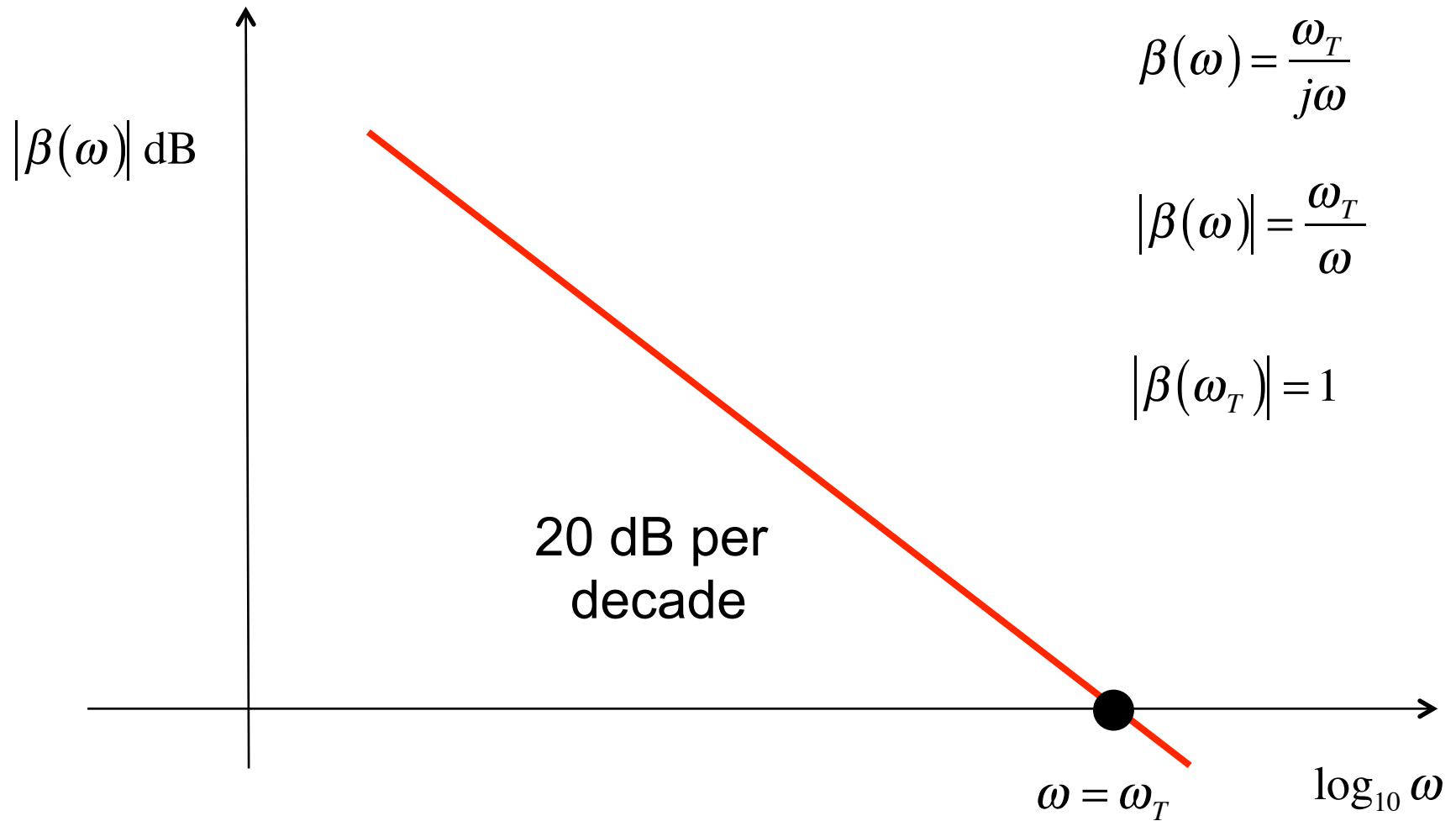
$$\beta(\omega) = \frac{\omega_T}{j\omega}$$

$$\omega_T = \frac{g_m}{(C_{gs} + C_{gd})}$$

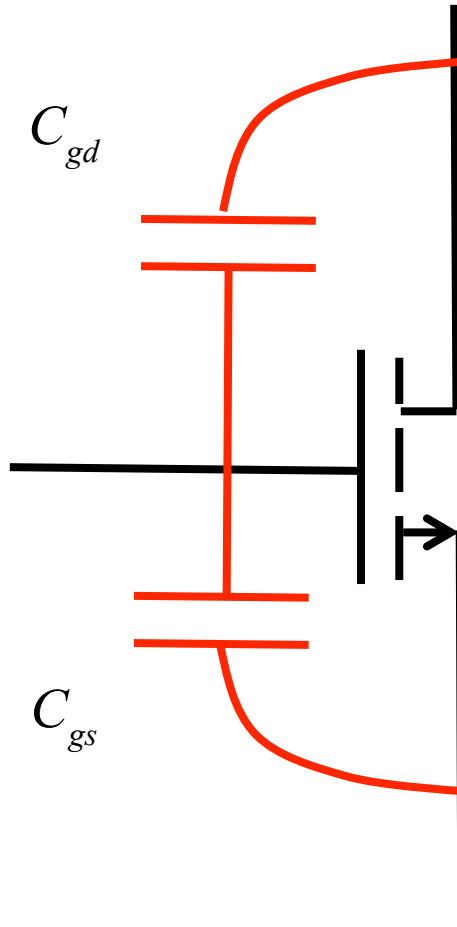
$$\omega_T = \frac{g_m}{C_{tot}}$$



Gain-Bandwidth product



Gain-Bandwidth product



$$\omega_T = \frac{g_m}{(C_{gs} + C_{gd})} = 2\pi f_T$$

f_T is an important figure of merit for a transistor.

$$f_T(\text{max}) = \frac{1}{2\pi t_t}$$

$$t_t = \frac{L}{\langle v \rangle}$$