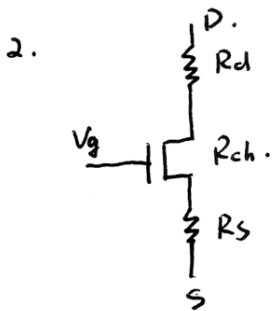


ECE 305 HW 11.

1. a. when $V_{gs} = V_{ds} = V_{dd} = 1.8V$, $I_{on} = I_{ds} \doteq 110 \mu A$
 when $V_{gs} = 0$, $V_{ds} = V_{dd} = 1.8V$, $I_{off} = I_{ds} \doteq 0 A$

b. As subthreshold current is exponential, $V_{th(sat)} \doteq 0.8V$, $I_{th(sat)} = 8 \times 10^{-6} A$ (linear)

c. $Q_{inv} = C_{ox} (V_{gs} - V_{th}) = 3 \mu F/cm^2 \times (1.8 - 0.8V) = 3 \mu C/cm^2$ (negative)
 or more precisely $Q_{inv} = C_{ox} (V_{gs} - V_{th} - I_d \cdot R_s) = 3 \mu F/cm^2 (1.8 - 0.8 - 110 \mu A \cdot 1k\Omega)$
 $\doteq 2.67 \mu C/cm^2$ (negative)



the effective $V'_{gs} = V_{gs} - I_d \cdot R_s$.

the effective $V'_{ds} = V_{ds} - I_d (R_s + R_d)$.

so just replace V_{gs} (or V_{ds}) with V'_{gs} (or V'_{ds}) to correct the series resistance.

a. $I_{on} = W C_{ox} V (V_{gs} - V_{th})$ ideal case.

$I_{on} = W C_{ox} V (V'_{gs} - V_{th})$ real case

so $I_{on} = W C_{ox} V (V_{gs} - V_{th} - I_{on} \cdot R_s)$

$$V = \frac{I_{on}}{W C_{ox} (V_{gs} - V_{th} - I_{on} \cdot R_s)} = \frac{110 \mu A}{1 \mu m \cdot 3 \mu F/cm^2 \cdot (1.8V - 0.8V - 110 \mu A \cdot 1k\Omega)}$$

$$= 4.1 \times 10^7 \text{ cm/s}$$

b. In the linear region, $I_{ds} \doteq 20 \mu A$ when $V_{gs} = 1.8V$, $V_{ds} = 0.1V$.

$$R_{total} = \frac{V_{ds}}{I_{ds}} = \frac{0.1V}{20 \mu A} = 5k\Omega.$$

$$R_{ch} = R_{total} - R_s - R_d = 5k\Omega - 1k\Omega - 1k\Omega = 3k\Omega.$$

ideally $I_d(\text{linear}) = \mu C_{ox} \frac{W}{L} (V_g - V_{th}) \cdot V_d$,

so $R_{ch} = \frac{V_d}{I_d} = \frac{1}{\mu C_{ox} \frac{W}{L} (V_g - V_{th})} = 3k\Omega.$

$$\Rightarrow \mu = \frac{1}{R_{ch} C_{ox} \frac{W}{L} (V_g - V_{th})} = \frac{1}{3k\Omega \times 3 \mu F/cm^2 \times \frac{1 \mu m}{14 \mu m} \times (1.8V - 0.8V)}$$

$$\doteq 1.56 \text{ cm}^2/V \cdot s.$$

c. The drain current is drift current:

$$I_d(y_1) = w \mu Q_n(y_1) E_{y_1}$$

$$Q_n = -C_{ox} [V_g - V_{th} - V_{y_1}]$$

$$\text{So } I = w \mu Q_n E_{y_1} = \frac{w \mu C_{ox}}{L} [(V_g - V_t) V_d - \frac{1}{2} V_d^2]$$

$$\Rightarrow E_{y_1} = -\frac{1}{L} \frac{[(V_g - V_t) V_d - \frac{1}{2} V_d^2]}{[V_g - V_t - V_{y_1}]}$$

For small V_d , we can ignore $(-\frac{1}{2} V_d^2)$, and $Q_n \approx -C_{ox} (V_g - V_t)$

$$\text{So } E_{y_1} \approx -\frac{V_d}{L} \text{ for } V_d \ll V_g - V_t.$$