

## ECE-305: Spring 2015

# BJTs: Ebers-Moll Model

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Pierret, Semiconductor Device Fundamentals (SDF)  
pp. 403-407

4/27/15



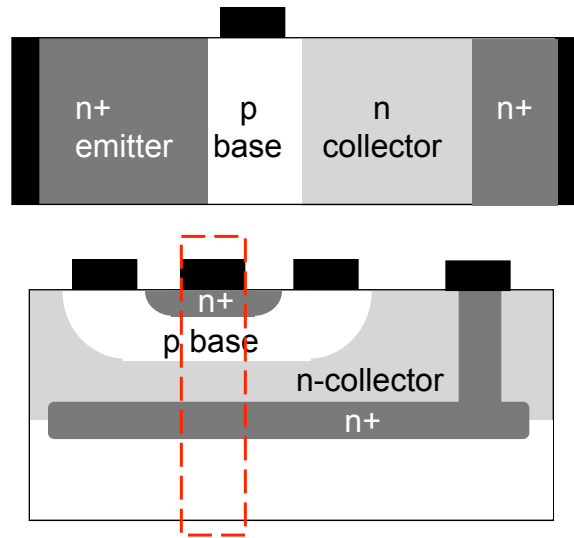
## last lecture

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- 1) Emitter injection efficiency
- 2) Base transport factor
- 3) Early effect
- 4) Speed (base transit time)
- 5) Effects of saturation
- 6) Gummel plots
- 7) Transconductance
- 8) HBTs
- 9) Emitter crowding**

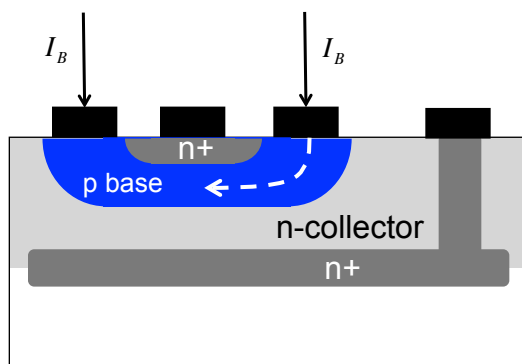
## 2D effects

*double  
diffused  
BJT*



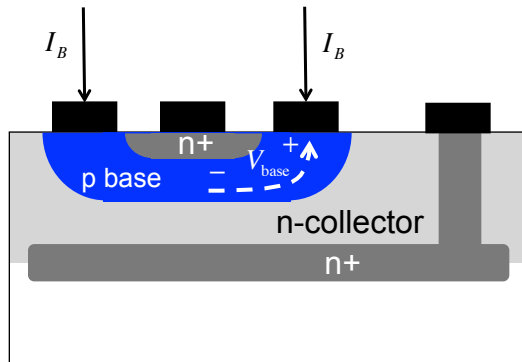
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## emitter current crowding



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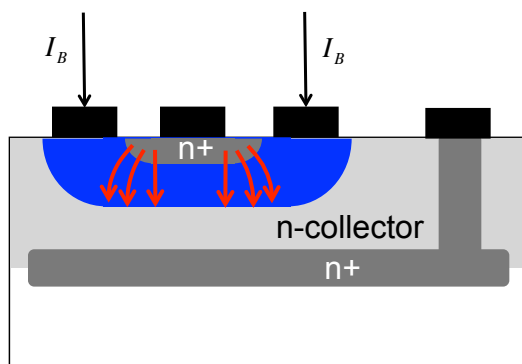
## emitter current crowding



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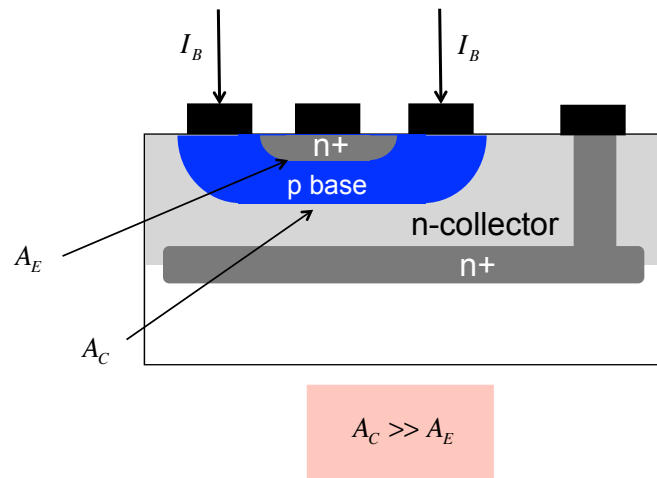
## emitter current crowding



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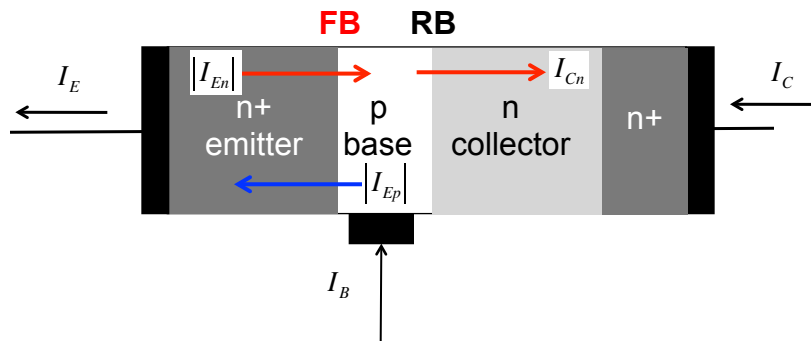
## emitter and collector areas



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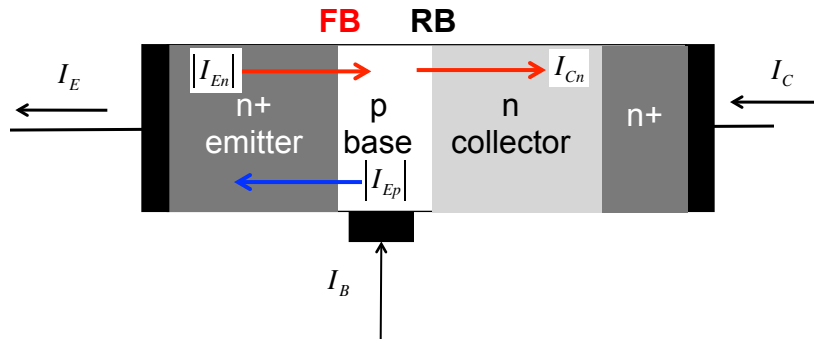
## Q1) Which is the base transport factor?



- a)  $|I_{En}| / (|I_{En}| + |I_{Ep}|)$       b)  $|I_{Cn}| / (|I_{En}| + |I_{Ep}|)$
- c)  $|I_{Cn}| / |I_{En}|$                       d)  $|I_{Ep}|$
- e)  $|I_{Cn}| / |I_{Ep}|$

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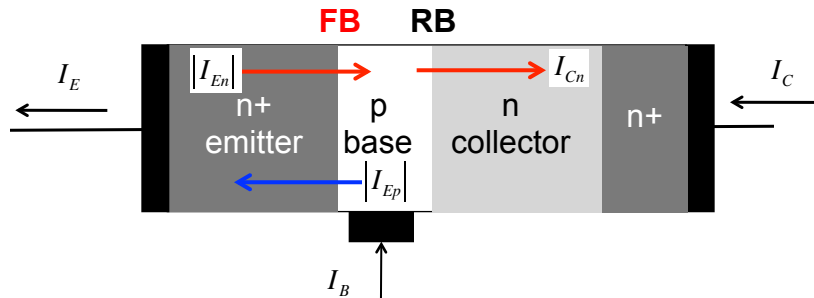
Q2) Which is beta\_dc?



- a)  $|I_{En}| / (|I_{En}| + |I_{Ep}|)$
- b)  $|I_{Cn}| / (|I_{En}| + |I_{Ep}|)$
- c)  $|I_{Cn}| / |I_{En}|$
- d)  $|I_{Ep}|$
- e)  $|I_{Cn}| / |I_{Ep}|$

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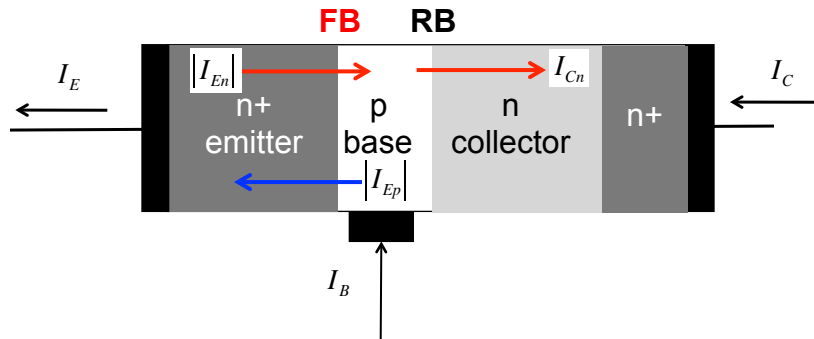
Q3) Which is alpha\_dc?



- a)  $|I_{En}| / (|I_{En}| + |I_{Ep}|)$
- b)  $|I_{Cn}| / (|I_{En}| + |I_{Ep}|)$
- c)  $|I_{Cn}| / |I_{En}|$
- d)  $|I_{Ep}|$
- e)  $|I_{Cn}| / |I_{Ep}|$

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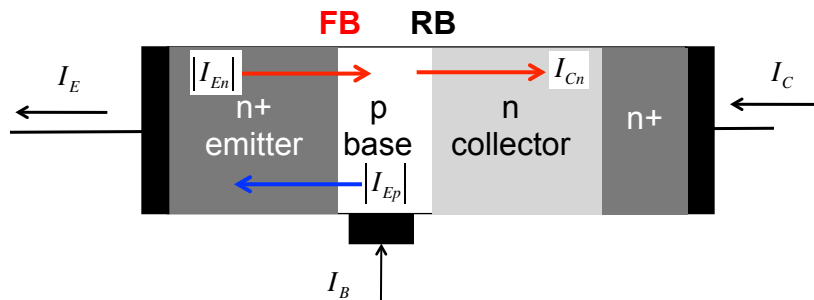
Q4) Which is the base current?



- a)  $|I_{En}| / (|I_{En}| + |I_{Ep}|)$       b)  $|I_{Cn}| / (|I_{En}| + |I_{Ep}|)$   
 c)  $|I_{Cn}| / |I_{En}|$                       d)  $|I_{Ep}|$   
 e)  $|I_{Cn}| / |I_{Ep}|$

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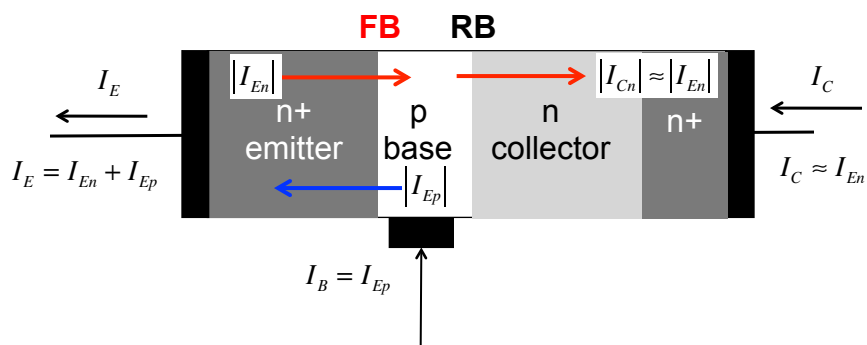
Q5) Which is the emitter injection efficiency?



- a)  $|I_{En}| / (|I_{En}| + |I_{Ep}|)$       b)  $|I_{Cn}| / (|I_{En}| + |I_{Ep}|)$   
 c)  $|I_{Cn}| / |I_{En}|$                       d)  $|I_{Ep}|$   
 e)  $|I_{Cn}| / |I_{Ep}|$

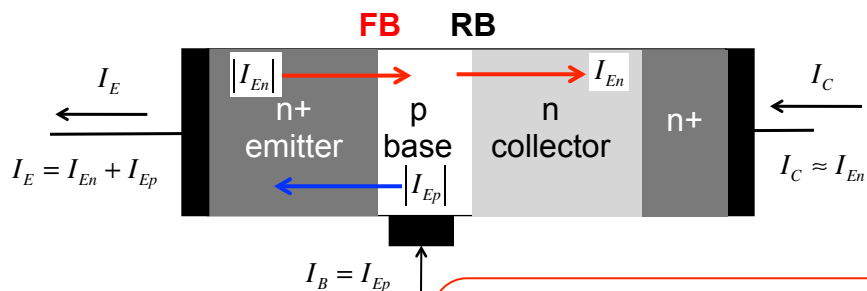
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## forward active region



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## emitter current: forward active region



$$|I_{En}| = qA_E \left( \frac{n_i^2}{N_{AB}} \right) \frac{D_n}{W_B} e^{qV_{BE}/k_B T}$$

$$|I_{Ep}| = qA_E \left( \frac{n_i^2}{N_{DE}} \right) \frac{D_p}{W_E} e^{qV_{BE}/k_B T}$$

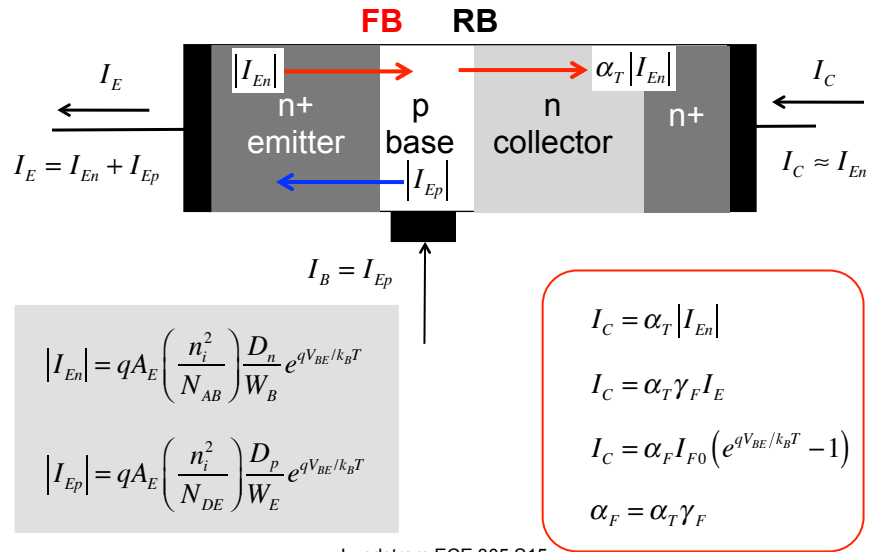
$$I_E = |I_{En}| + |I_{Ep}|$$

$$I_E = I_{F0} \left( e^{qV_{BE}/k_B T} - 1 \right)$$

$$I_{F0} = qA_E \left( \frac{n_i^2}{N_{AB}} \right) \frac{D_n}{W_B} + qA_E \left( \frac{n_i^2}{N_{DE}} \right) \frac{D_p}{W_E}$$

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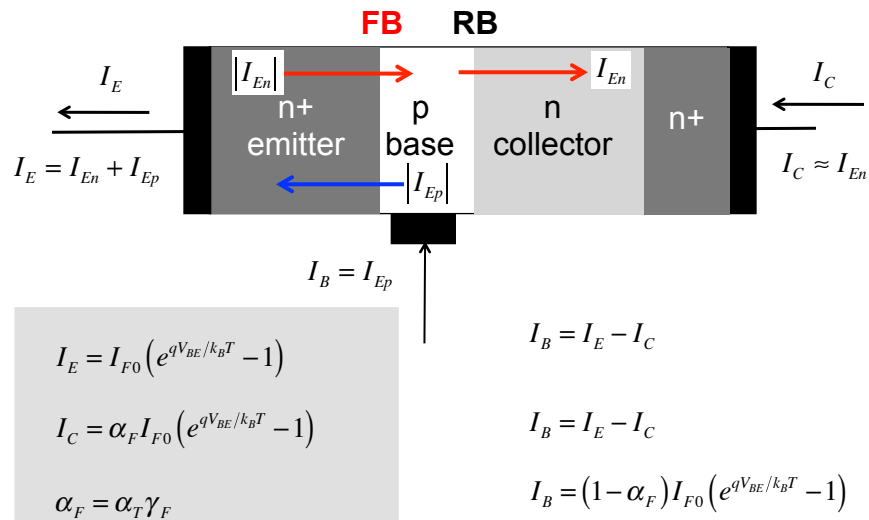
## collector current: forward active region



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## base current: forward active region

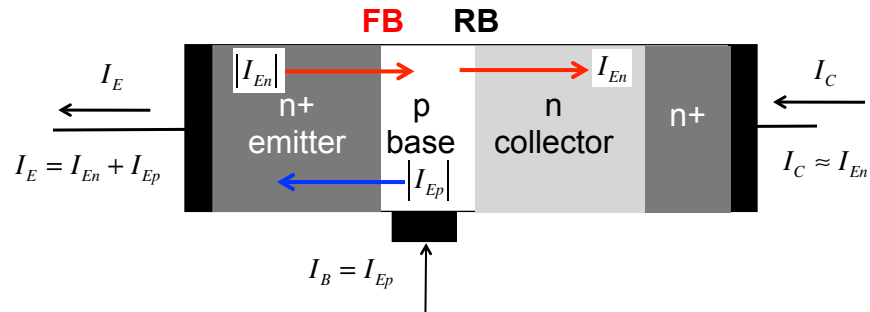


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## summary: forward active region



$$I_E = I_{F0} \left( e^{qV_{BE}/k_B T} - 1 \right)$$

$$\alpha_F = \alpha_T \gamma_F$$

$$I_C = \alpha_F I_{F0} \left( e^{qV_{BE}/k_B T} - 1 \right)$$

$$I_{F0} = qA_E \left( \frac{n_i^2}{N_{AB}} \right) \frac{D_n}{W_B} + qA_E \left( \frac{n_i^2}{N_{DE}} \right) \frac{D_p}{W_E}$$

$$I_B = (1 - \alpha_F) I_{F0} \left( e^{qV_{BE}/k_B T} - 1 \right)$$

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## Ebers-Moll model

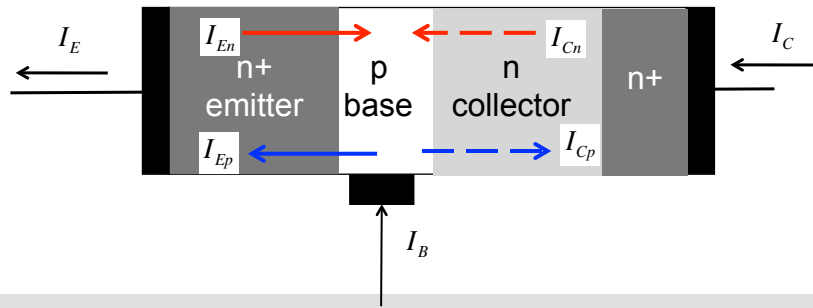
Question:

How do we describe the BJT in **any** region of operation?

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## emitter-base junction (the **forward** diode)



$$I_{En} = -qA \frac{D_n}{W_B} \frac{n_i^2}{N_{AB}} (e^{qV_{BE}/k_B T} - 1)$$

$$I_E(V_{BE}) = -I_{En}(V_{BE}) - I_{Ep}(V_{BE})$$

$$I_{Ep} = -qA \frac{D_p}{W_E} \frac{n_i^2}{N_{DE}} (e^{qV_{BE}/k_B T} - 1)$$

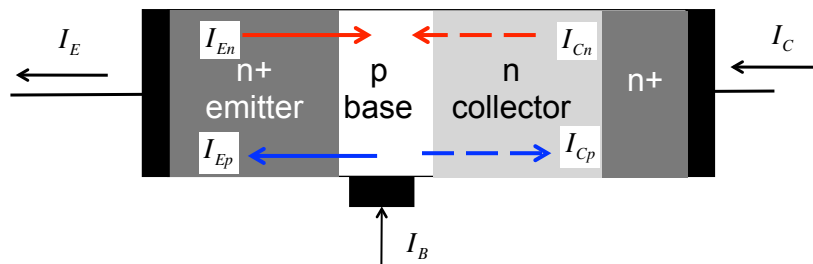
$$I_E(V_{BE}) = I_{F0} (e^{qV_{BE}/k_B T} - 1)$$

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## Base-collector junction (the **reverse** diode)



$$I_{Cn}(V_{BC}) = qA \frac{D_n}{W_B} \frac{n_i^2}{N_{AB}} (e^{qV_{BC}/k_B T} - 1)$$

$$I_C(V_{BC}) = -[I_{Cn}(V_{BC}) + I_{Cp}(V_{BC})]$$

$$I_{Cp}(V_{BC}) = qA \frac{D_p}{W_C} \frac{n_i^2}{N_{DC}} (e^{qV_{BC}/k_B T} - 1)$$

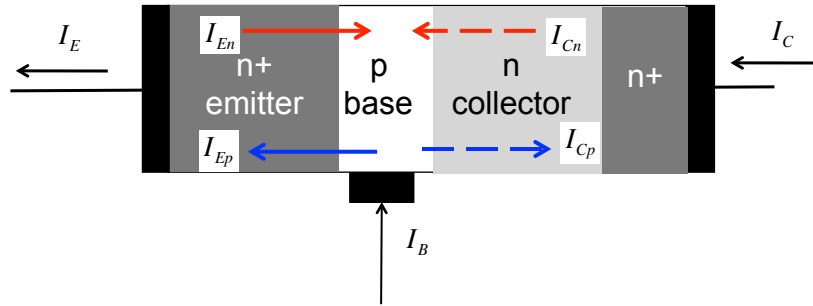
$$I_C(V_{BC}) = -I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

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## Both junctions....



$$I_C(V_{BC}) = -I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E(V_{BE}) = I_{F0} (e^{qV_{BE}/k_B T} - 1)$$

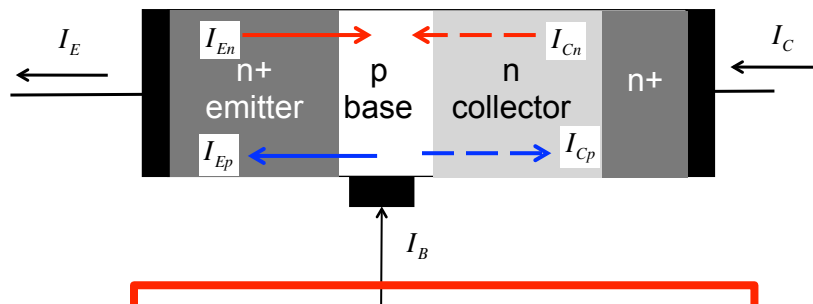
**But....**  
The two junctions are coupled!

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## Ebers-Moll model



$$I_C(V_{BE}, V_{BC}) = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E(V_{BE}, V_{BC}) = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

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## Ebers-Moll model

$$I_C(V_{BE}, V_{BC}) = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E(V_{BE}, V_{BC}) = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_B(V_{BE}, V_{BC}) = I_E(V_{BE}, V_{BC}) - I_C(V_{BE}, V_{BC})$$

See Pierret SDF, Chapter 11, sec. 11.1.4

## Ebers-Moll model

$$I_C(V_{BE}, V_{BC}) = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E(V_{BE}, V_{BC}) = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$\alpha_F = \alpha_T \gamma_F \quad I_{F0} = qA_E \left( \frac{n_i^2}{N_{AB}} \right) \frac{D_n}{W_B} + qA_E \left( \frac{n_i^2}{N_{DE}} \right) \frac{D_p}{W_E}$$

$$\alpha_R = \alpha_T \gamma_R \quad I_{R0} = qA_E \left( \frac{n_i^2}{N_{AB}} \right) \frac{D_n}{W_B} + qA_E \left( \frac{n_i^2}{N_{DC}} \right) \frac{D_p}{W_C}$$

$$\alpha_F I_{F0} = \alpha_R I_{R0}$$

## Ebers-Moll model

$$I_C(V_{BE}, V_{BC}) = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E(V_{BE}, V_{BC}) = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_B(V_{BE}, V_{BC}) = I_E(V_{BE}, V_{BC}) - I_C(V_{BE}, V_{BC})$$

$$\alpha_F I_{F0} = \alpha_R I_{R0}$$

See Pierret SDF, Chapter 11, sec. 11.1.4

## Check active region

$$I_C(V_{BE}, V_{BC}) = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1) \rightarrow \alpha_F I_{F0} e^{qV_{BE}/k_B T} + I_{R0}$$

$$I_E(V_{BE}, V_{BC}) = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1) \rightarrow I_{F0} e^{qV_{BE}/k_B T} + \alpha_R I_{R0}$$

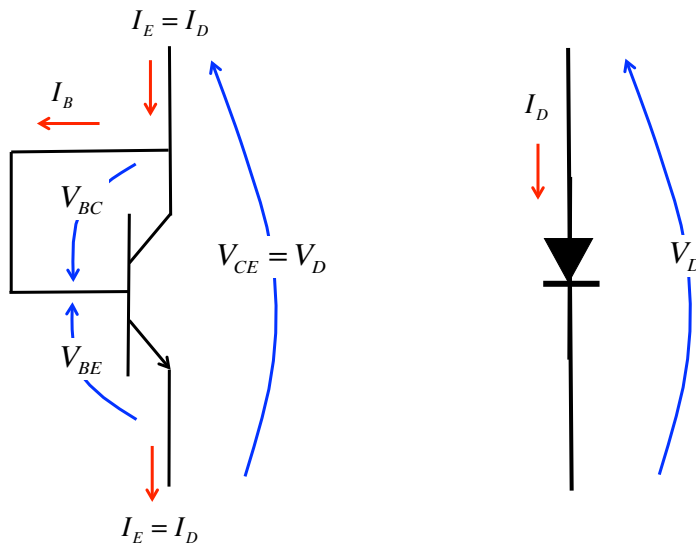
$$I_B(V_{BE}, V_{BC}) = I_E(V_{BE}, V_{BC}) - I_C(V_{BE}, V_{BC}) \rightarrow (1 - \alpha_F) I_{F0} e^{qV_{BE}/k_B T} - (1 - \alpha_R) I_{R0}$$

$$I_C \approx \alpha_F I_{F0} e^{qV_{BE}/k_B T}$$

$$I_B \approx (1 - \alpha_F) I_{F0} e^{qV_{BE}/k_B T} = \frac{(1 - \alpha_F)}{\alpha_F} I_C = \frac{1}{\beta_{dc}} I_C$$

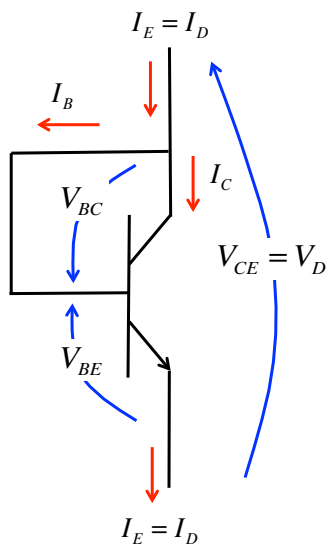


## What is $I_D$ ?



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## What is $I_D$ ?



$$I_C = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

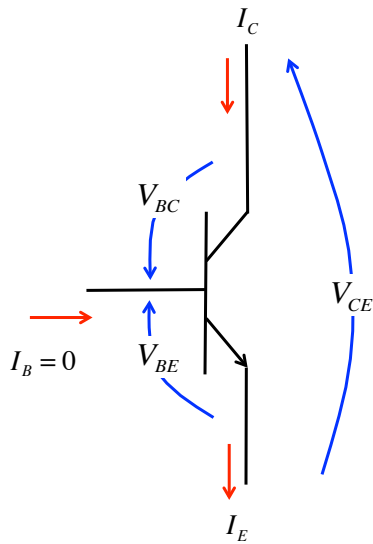
$$V_{BC} = 0$$

$$I_E = I_{F0} (e^{qV_{BE}/k_B T} - 1)$$

$$I_D = I_{F0} (e^{qV_D/k_B T} - 1)$$

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## What is $I_C$ ?



$$I_C = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

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## Ebers-Moll model

$$I_C(V_{BE}, V_{BC}) = \alpha_F I_{F0} (e^{qV_{BE}/k_B T} - 1) - I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_E(V_{BE}, V_{BC}) = I_{F0} (e^{qV_{BE}/k_B T} - 1) - \alpha_R I_{R0} (e^{qV_{BC}/k_B T} - 1)$$

$$I_B(V_{BE}, V_{BC}) = I_E(V_{BE}, V_{BC}) - I_C(V_{BE}, V_{BC})$$

$$\alpha_F I_{F0} = \alpha_R I_{R0}$$

See Pierret SDF, Chapter 11, sec. 11.1.4

## Ebers-Moll model (ii)

$$I_{F0} = qA \left( \frac{D_{nB}}{W_B} \frac{n_i^2}{N_{AB}} + \frac{D_{pE}}{W_E} \frac{n_i^2}{N_{DE}} \right)$$

$$I_{R0} = qA \left( \frac{D_{nB}}{W_B} \frac{n_i^2}{N_{AB}} + \frac{D_{pC}}{W_C} \frac{n_i^2}{N_{DC}} \right)$$

$$\alpha_F = \gamma_F \alpha_T \quad \alpha_R = \gamma_R \alpha_T$$

$$\alpha_F I_{F0} = \alpha_R I_{R0} \rightarrow \alpha_R = \alpha_F \frac{I_{F0}}{I_{R0}}$$