

The BTE with a B-field

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Introduction

Electrical measurements in the presence of a B-field are widely-used for characterizing semiconductors.

Question: How does the current equation change in the presence of a B-field?

Answer:
$$J_x = \sigma_n \mathcal{E}_x \rightarrow \vec{J} = [\sigma(\vec{B})] \vec{\mathcal{E}} = J_i = \sigma_{ij}(\vec{B}) \mathcal{E}_j$$

The BTE with a B-field...

$$\frac{\partial f}{\partial t} + \vec{v} \cdot \nabla_r f + \vec{F}_e \cdot \nabla_p f = \left. \frac{df}{dt} \right|_{coll}$$

steady-state with RTA:

$$\vec{v} \cdot \nabla_r f + \vec{F}_e \cdot \nabla_p f = -\frac{\delta f}{\tau_m}$$

$$\vec{F}_e = -q\vec{E} - q\vec{v} \times \vec{B}$$

spatially uniform:

$$-q\vec{E} \cdot \nabla_p f - q(\vec{v} \times \vec{B}) \cdot \nabla_p f = -\delta f / \tau_m$$

$$\nabla_p f \rightarrow \nabla_p f_S ?$$

The BTE with a B-field...

$$-q\vec{E} \cdot \nabla_p f_S - q(\vec{v} \times \vec{B}) \cdot \nabla_p f_S = -\delta f / \tau_m$$

OK here

But not here!

$$\nabla_p f_S = \frac{\partial f_S}{\partial E} \nabla_p E = \frac{\partial f_S}{\partial E} \vec{v} \quad (\vec{v} \times \vec{B}) \cdot \vec{v} = 0!$$

$$-q\vec{E} \cdot \nabla_p f_S - q(\vec{v} \times \vec{B}) \cdot \nabla_p (\delta f) = -\delta f / \tau_m$$

a much more difficult equation to solve

One approach...

$$-q\vec{E} \cdot \nabla_p f_S - q(\vec{v} \times \vec{B}) \cdot \nabla_p f = -\delta f / \tau_m$$

1) First, assume no B-field:

$$-q\vec{E} \cdot \nabla_p f_S = -\delta f_1 / \tau_m \quad \delta f_1 = \tau_m \left(-\frac{\partial f_S}{\partial E} \right) \vec{v} \cdot (-q\vec{E})$$

2) Then use this solution to solve for the additional part due to the B-field:

$$-q(\vec{v} \times \vec{B}) \cdot \nabla_p \delta f_1 = -\delta f_2 / \tau_m$$

3) The total solution is:

$$\delta f_{tot} = \delta f_1 + \delta f_2$$

Comments...

$$-q\vec{E} \cdot \nabla_p f_S - q(\vec{v} \times \vec{B}) \cdot \nabla_p \delta f = -\delta f / \tau_m$$

$$\delta f_{tot} = \delta f_1 + \delta f_2$$

- 1) This approach works and gives us terms **linear** in B . See Chapter 4, Sec. 4 in Lundstrom, *Fundamentals of Carrier Transport*, 2nd Ed., Cambridge, 2000.
- 2) Now, we can use δf_{tot} in the BTE to get an even better solution. This gives us additional terms that are **quadratic** in B .

Another approach...

Recall that without the B-field: $-q\vec{E} \cdot \nabla_p f_S = -\delta f / \tau_m$

The solution was: $\delta f = \tau_m \left(-\frac{\partial f_0}{\partial E} \right) \vec{v} \cdot (-q\vec{E})$

So with a B-field: $-q\vec{E} \cdot \nabla_p f_S - q(\vec{v} \times \vec{B}) \cdot \nabla_p (\delta f) = -\delta f / \tau_m$

Assume a solution of the form: $\delta f = \tau_m \left(-\frac{\partial f_S}{\partial E} \right) \vec{v} \cdot \vec{G}$

And find the unknown vector, \vec{G}

The solution with a B-field...

$$\vec{G} = \frac{-q\vec{E} - (q^2\tau_m/m^*)(\vec{B} \times \vec{E}) - q(q\tau_m/m^*)^2(\vec{E} \cdot \vec{B})\vec{B}}{1 + (\omega_c\tau_m)^2}$$

cyclotron frequency: $\omega_c = \frac{qB}{m^*}$ low B-field: $\omega_c\tau_m \ll 1$

(An electron gets only a little way along its orbit, and then it scatters.)

Assume a planar geometry with the electric field in the x-y plane and a z-directed, **small B-field** normal to the plane.

$$\vec{G} = -q\vec{E} - (q^2\tau_m/m^*)(\vec{B} \times \vec{E})$$

G lies in the x-y plane.

The 2D current equation...

$$\vec{J}_n = \frac{1}{A} \sum_{\vec{k}} (-q) \vec{v} (f_S + \delta f) = \frac{1}{A} \sum_{\vec{k}} (-q) \vec{v} (\delta f) \quad \delta f = \tau_m \left(-\frac{\partial f_S}{\partial E} \right) \vec{v} \cdot \vec{G}$$

Result:

$$\vec{J}_n = \sigma_S \vec{E} - \sigma_S \mu_H (\vec{E} \times \vec{B})$$

$$\omega_c \tau_m \ll 1$$

$$\sigma_S = n_S q \mu_n$$

$$\mu_H = \mu_n r_H$$

Hall mobility

$$\mu_n \equiv \frac{q \langle \langle \tau_m \rangle \rangle}{m^*}$$

$$r_H \equiv \frac{\langle \langle \tau_m^2 \rangle \rangle}{\langle \langle \tau_m \rangle \rangle^2}$$

Hall factor

Average scattering times...

$$\mu_n \equiv \frac{q \langle\langle \tau_m \rangle\rangle}{m^*}$$

$$\langle\langle \tau_m \rangle\rangle \equiv \frac{\langle E \tau(E) \rangle}{\langle E \rangle} \quad \text{“transport average”}$$

$$\langle E \tau(E) \rangle = \frac{\sum_{\vec{k}} E \tau(E) f_S(E)}{\sum_{\vec{k}} f_S(E)} \quad \langle E \rangle = \frac{\sum_{\vec{k}} E f_S(E)}{\sum_{\vec{k}} f_S(E)}$$

Power law scattering: $\tau_m(E) = \tau_0 (E/k_B T)^s$

$$\langle\langle \tau_m \rangle\rangle = \tau_0 \frac{\Gamma(s+5/2)}{\Gamma(5/2)} \quad \text{(for 3D electrons)}$$

Hall factor

$$r_H \equiv \frac{\langle\langle \tau_m^2 \rangle\rangle}{\langle\langle \tau_m \rangle\rangle^2}$$

$$r_H = \frac{\Gamma(2s + 5/2)\Gamma(5/2)}{\Gamma(s + 5/2)^2}$$

ADP scattering: $s = -1/2$

II scattering: $s = 3/2$

$$1.18 < r_H < 1.93$$

(for 3D electrons)

Exercise

Assume power law scattering and 2D electrons. Work out the following two quantities in terms of the characteristic exponent, s .

$$\langle\langle\tau_m\rangle\rangle \quad r_H \equiv \frac{\langle\langle\tau_m^2\rangle\rangle}{\langle\langle\tau_m\rangle\rangle^2}$$

The magnetoconductivity tensor...

$$\vec{J}_n = \sigma_S \vec{E} - \sigma_S \mu_H (\vec{E} \times \vec{B}) \quad \text{vector notation}$$

$$\begin{pmatrix} J_{nx} \\ J_{ny} \end{pmatrix} = \begin{bmatrix} \sigma_S & -\sigma_S \mu_H B_z \\ +\sigma_S \mu_H B_z & \sigma_S \end{bmatrix} \begin{pmatrix} E_x \\ E_y \end{pmatrix}$$

$$J_i = \sigma_{ij}(\vec{B}) E_j \quad \text{indicial notation}$$

Diagonal components unaffected.
Off-diagonal components introduced.

Tensors and indicial notation

$$\vec{J} = [\sigma] \vec{\mathcal{E}}$$

$$\begin{bmatrix} J_x \\ J_y \\ J_z \end{bmatrix} = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} \begin{bmatrix} \mathcal{E}_x \\ \mathcal{E}_y \\ \mathcal{E}_z \end{bmatrix}$$

$$J_i = \sum_{j=1}^3 \sigma_{ij} \mathcal{E}_j$$

“indicial notation”

$$J_i = \sum_{j=1}^3 \sigma_{ij} \mathcal{E}_j \equiv \sigma_{ij} \mathcal{E}_j$$

“summation convention”

Diagonal tensors

$$\vec{J} = \sigma_0 \vec{E}$$

$$\begin{bmatrix} J_x \\ J_y \\ J_z \end{bmatrix} = \begin{bmatrix} \sigma_0 & 0 & 0 \\ 0 & \sigma_0 & 0 \\ 0 & 0 & \sigma_0 \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} \quad J_i = \sigma_0 E_i$$

“Kronecker delta”

$$\begin{aligned} \sigma_{ij} &= \sigma_0 \delta_{ij} \\ \delta_{ij} &= 1 \quad (i = j) \\ &= 0 \quad (i \neq j) \end{aligned}$$

$$[\sigma] = \sigma_0 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Cross products

Vector notation: $\vec{J}_n = \sigma_S \vec{E} - \sigma_S \mu_H (\vec{E} \times \vec{B})$

Indicial notation: ???

Alternating unit tensor

$$\vec{C} = \vec{E} \times \vec{B} \quad \vec{C} = \begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ \mathcal{E}_x & \mathcal{E}_y & \mathcal{E}_z \\ B_x & B_y & B_z \end{bmatrix} = \hat{x}(\mathcal{E}_y B_z - \mathcal{E}_z B_y) + \dots$$

We write cross-products with an “alternating unit tensor”:

$$C_i = \varepsilon_{ijk} \mathcal{E}_j B_k$$

$$\varepsilon_{ijk} = +1(i, j, k \text{ cyclic})$$

$$C_x = \varepsilon_{xjk} \mathcal{E}_j B_k$$

$$= -1(i, j, k \text{ anti-cyclic})$$

$$= \varepsilon_{xyz} \mathcal{E}_y B_z + \varepsilon_{xzy} \mathcal{E}_z B_y$$

$$= 0(\text{otherwise})$$

$$= \mathcal{E}_y B_z - \mathcal{E}_z B_y$$

Current equation

$$\vec{J}_n = \sigma_n \vec{E} - (\sigma_n \mu_n r_H) \vec{E} \times \vec{B}$$

Vector

$$J_i = \sigma_n E_i - \sigma_n \mu_H \epsilon_{ijk} E_j B_k$$

Indicial

The BTE with a B-field

See Chapter 4, Sec. 4 in Lundstrom, *Fundamentals of Carrier Transport*, 2nd Ed., Cambridge, 2000.

See Chapter 7 in Lundstrom and Jeong, *Near-Equilibrium Transport*, World Scientific, 2013.

Questions

$$\vec{J}_n = \sigma_S \vec{E} - \sigma_S \mu_H (\vec{E} \times \vec{B})$$

$$r_H \equiv \frac{\langle\langle \tau_m^2 \rangle\rangle}{\langle\langle \tau_m \rangle\rangle^2}$$

$$\tau_m(E) = \tau_0 (E/k_B T)^s$$

$$r_H = \frac{\Gamma(2s + 5/2)\Gamma(5/2)}{\Gamma(s + 5/2)^2} \quad (3D)$$

