SELF-HEATING EFFECTS IN SOI DEVICES AND GAN HEMTS

Dragica Vasileska, ASU

Thanks to …

Katerina Raleva, Stephen M. Goodnick, Mihail Nedjalkov, Arif Hossain, Balaji Padmanabhan, Manan Gada, Seung Kyung Yoo

Motivation Thermal Effects Previous Work Done in Thermal Modeling The ASU Model for Addressing Self-Heating **Conclusions**

Motivation

Transistor Scaling

Thermal Effects and Scaling

Transistor Scaling: Moore's Law

Gordon Moore "every 1.5 years complexity doubles"

www.intel.com

Transistor Scaling: Dennard's Law

R. **Dennard**, et al., *IEEE Journal of Solid State Circuits*, vol. SC-9, no. 5, pp. 256-268, Oct. 1974.

Multi-Gate Transistors Implementation

Multi-Gate Fin Transistor:

- ++ Self Aligned structure for S/D
- **Non-Planar structure**

 $Zdevice = 2*Hsi + Wsi$

Multi-Gate Fin Transistor

www.intel.com

More Than Moore and Beyond CMOS

ITRS-ERD vision of the role of Beyond CMOS and More than Moore elements to form future extended CMOS platforms (2010).

www.itrs.com

2020 and Beyond …

- **- Advanced component technology + advanced system design**
- **- Beyond CMOS + advanced More than Moore integration with More Moore For systems 2020 and beyond**

Thermal Effects and Scaling

- □ Intel VP Patrick Gelsinger (ISSCC 2001)
	- **If scaling continues at present pace, by 2005, high** speed processors would have power density of nuclear reactor, by 2010, a rocket nozzle, and by 2015, surface of sun.
	- \blacksquare "Business as usual will not work in the future."
- \square Intel stock dropped 8% on the next day
- \Box But attention to power is increasing

Thermal Design Power

- The **thermal design power (TDP)**, sometimes called **thermal design point**, refers to the maximum amount of [power](http://en.wikipedia.org/wiki/Electric_power) the cooling system [in a computer is requi](http://en.wikipedia.org/wiki/Computer_cooling)red to [dissipate](http://en.wikipedia.org/wiki/Dissipation).
- For example, a [laptop](http://en.wikipedia.org/wiki/Laptop)'s [CPU](http://en.wikipedia.org/wiki/Microprocessor) cooling system may be designed for a 20 [watt](http://en.wikipedia.org/wiki/Watt) TDP, which means that it can dissipate up to 20 watts of **[heat](http://en.wikipedia.org/wiki/Heat)** without exceeding the maximum [junction temperature](http://en.wikipedia.org/wiki/Junction_temperature) for the [computer chip.](http://en.wikipedia.org/wiki/Computer_chip)

Thermal Effects

Electro-Thermal Effects

Thermo-Electric Effects

Analogy Between Electrical and Thermal Variables

Electro-Thermal Effects

D Joule Heating:

- When an electric current flows through a solid or liquid with finite conductivity, electric energy is converted to heat through resistive losses in the material.
- \blacksquare The heat is generated on the microscale when the conduction electrons transfer energy to the conductors atoms through collisions.
- \blacksquare Joule heating is in some cases unwanted, and efforts are made to reduce it.
	- **However, many applications rely on Joule heating;**
		- some of these use the effect directly, such as cooking plates,
		- while other applications, such as microvalves for fluid control, use the effect indirectly through thermal expansion.

Why Electro-Thermal Effects in Devices?

Reason for Observation of Self-Heating MUSTs in the Theoretical Model

Fully depleted (FD) body

[E. Pop, R.W Dutton, K.E. Goodson, "Analytic Band Monte Carlo Model for Electron](http://poplab.ece.illinois.edu/pdfs/epop-jap-v96nov04.pdf) Transport in Si Including Acoustic and Optical Phonon Dispersion," *J. Appl. Phys.* **96**, 4998 (2004)

Implementation of Electro-Thermal Effects in Commercial Simulators

- Silvaco ATLAS implements **Wachutka** model for lattice heating which accounts for:
	- **D** Joule heating
	- **O** Cooling due to carrier generation and recombination
	- **Peltier and Thomson effects**

Wachutka, G.K., "Rigorous Thermodynamic Treatment of Heat Generation in Semiconductor Device Modeling", *IEEE Trans., Computer-Aided Design* Vol. 9, No. 11 (1990): 1141-1149.

Heat Generation Model

In the past, the heat generation model was simply:

$$
H = (J_n + J_p) \bullet E
$$

Presently:

 $\begin{aligned} \text{ration Model} \ \text{heat generation model was simply:} \ \begin{aligned} H & = (J_n + J_p) \text{e} \ \text{d}t & = \text{e} \end{aligned} \end{aligned}$ $\big(J_n\nabla P_n\big)\!-\!T_L\big(J_p\nabla P_p\big)\!+\,\longrightarrow\,\quad$ Peltier and Joule-Thomson effects 2 $|\mathbf{r}|^2$ $\begin{CD} \begin{CD} \textbf{eration} & \textbf{P} \ \textbf{eration} & \textbf{P} \ \textbf{H} & = (\textbf{J}_n + \textbf{J}_n) \ \textbf{H$ st, the heat generation

st, the heat generation
 $H = (J_n + J_n)$
 $\left. \begin{array}{l} \frac{|J_p|^2}{i\mu_p p} - \frac{1}{\mu_p p} \end{array} \right\}$
 $\left[T_L \left(\frac{\partial \phi_n}{\partial T_{n,p}} \right) - \phi_n - T_L \left(\frac{\partial \phi_p}{\partial T_{n,p}} \right) \right]$
 $\left. \begin{array}{l} \text{Ric} \\ \text{Ric} \end{array} \right] + P_n \left. \begin{array}{l} \nabla$ are past, then I_n of I_n of $I_{n,n}$ if $\frac{|J_n|^2}{\mu_n n} + \frac{|J_p|^2}{q\mu_p p}$
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wachutka, G.K., "Rige $p \mid \left| \begin{array}{c} \mathbf{p} \\ \mathbf{p} \end{array} \right|$ at Generatic

e past, the heat get
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ently:
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 $\frac{L}{L} (J_n \nabla P_n) - T_L (J_p \nabla P_p) + \frac{1}{L} \left[\frac{\partial \phi_n}{\partial T_{n,p}} \right] - \phi_n - T_L \left[\frac{\partial \phi_n}{\partial T_{n,p}} \right] + P_n \left[\nabla \cdot J_n - T_L \right]$ *n p L n L p n p n p n p L n n L p p n p n p* $H = \frac{|J_n|^2}{\sqrt{J_p}} + \frac{|J_p|^2}{\sqrt{J_p}}$ $\begin{split} \textbf{at} \textbf{ Generation}\ \textbf{e} &\textbf{post, the heat gene}\ \textbf{H} &= \left(J_n + \frac{|J_n|^2}{q\mu_n n} + \frac{|J_p|^2}{q\mu_p p} - \frac{|J_n|^2}{q\mu_n n} + \frac{|J_p|^2}{q\mu_p p} \end{split}$ $\begin{split} \textsf{at} \quad \textsf{Generation} \quad \textsf{M} \ \textsf{a} \ \textsf{e} \ \textsf{past}, \ \textsf{the \, heat \, general} \ \textsf{f} \ = \ & (J_n + J_p \ \textsf{sently:} \ \frac{\left|J_n\right|^2}{q\mu_n n} + \frac{\left|J_p\right|^2}{q\mu_p p} - \sum_{\textsf{J}\text{ot} \in \mathcal{A}} \ \textsf{I}_L(J_n \nabla P_n) - T_L\big(J_p \nabla P_p\big) + \sum_{\textsf{P} \in \mathcal{A}} \ \textsf{f}_L(J_n \nabla P_n) - T_L\Big$ **Neinanning Constrainer (September 2014)**
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** *T***_{***L***}** $\left[\frac{\partial \phi_n}{\partial T_{n,p}}\right]^{-1} + P_n\left[\frac{\partial \phi_n}{\partial T_{n,p}}\right]^{-1} \longrightarrow$ **Joule heating term
** *T***_L (J_n \nabla P_n) - T_L (J_p \nabla P_p) 11 Generation Model**
 e past, the heat generation model was simply:
 $H = (J_n + J_p) \cdot E$
 ently:
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 $\frac{|I_n|^2}{\mu_n n} + \frac{|J_\rho|^2}{q \mu_\rho p}$ \longrightarrow Politier and Joule-Thomson $+q(R-G)\left|T_{L}\left(\frac{\partial\phi_{n}}{\partial T_{n,p}}\right)-\phi_{n}-T_{L}\left(\frac{\partial\phi_{p}}{\partial T_{n,p}}\right)+\phi_{p}\right|-\qquad\qquad\qquad$ at generation model was simply:
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 \rightarrow Joule heating term
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 $\phi_n-T_L\left(\frac{\partial \phi_p}{\partial T_{n,p}}\right)+\phi_p$ Pecombination and
 $-T_L\left[\left(\frac{\partial \phi_p}{\partial T_{n,p}}\right)+P_p\right]\nabla \$ $-T_L\left[\left(\frac{\partial \phi_n}{\partial T_{n,n}}\right) + P_n\left|\nabla \bullet J_n - T_L\right|\left(\frac{\partial \phi_p}{\partial T_{n,n}}\right) + P_p\left|\nabla \bullet J_p\right|\right]$ early **Generation Model**

the past, the heat generation model was simply:
 $H = (J_n + J_p) \cdot E$

esently:
 $= \frac{|J_n|^2}{q\mu_n n} + \frac{|J_p|^2}{q\mu_p n}$ \longrightarrow Joue heating term
 $-T_L(J_n \nabla P_n) - T_L(J_p \nabla P_p) + \longrightarrow$ Peltier and Joule-Thomson effects
 call Generation Model

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 $H = (J_n + J_p) \cdot E$

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ssently:
** $H = (J_n + J_p) \cdot E$ **

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** \Rightarrow **Joule heating term
** $-T_L(J_n \nabla P_n) - T_L(J_p \nabla P_p) + \Rightarrow$ **Pelitier and Joule-Th Configured to the comparison of the comparison of the past** $H = (J_n + J_p) \cdot E$ **

ssently:
** $H = (J_n + J_p) \cdot E$ **

ssently:
** $\frac{|J_n|^2}{q\mu_n n} + \frac{|J_p|^2}{q\mu_p p} -$ **
** \Rightarrow **Joule heating term
** $-T_L(J_n \nabla P_n) - T_L(J_p \nabla P_p) + \Rightarrow$ **Pelitier and Joule-Th The Soule heating term** Recombination and Generation heating and cooling terms

Wachutka, G.K., "Rigorous Thermodynamic Treatment of Heat Generation in Semiconductor Device Modeling", *IEEE Trans., Computer-Aided Design* Vol. 9, No. 11 (1990): 1141-1149.

Non-Isothermal Current Densities

When SILVACO GIGA module is being invoked, the electron and hole current densities are modified to account for spatially varying lattice temperatures: *p p p p L* **J follow Fig 11 and 10**
 J g GIGA module is being invoked, the

es are modified to account for spatia
 $J_n = -q\mu_n n \left(\nabla \phi_n + P_n \nabla T_L \right)$
 $J_p = -q\mu_p p \left(\nabla \phi_p + P_p \nabla T_L \right)$

I P_p are absolute thermoelectric powe

late **Jthermal Current D**
 *J***_n = -q** $\mu_n n (\nabla \phi_n + P_n \nabla T_L)$ **
** *J***_n = -q** $\mu_n n (\nabla \phi_n + P_n \nabla T_L)$ **
** *J***_p = -q** $\mu_p p (\nabla \phi_p + P_p \nabla T_L)$ **
** *P***_p are absolute thermoelectric powers

lated using:
** *P***_{= -}\frac{k_B}{\sqrt{2}} (\frac{5}{2} + \ln(\frac{N** Figure 11 Densities

module is being invoked, the electron and hole

odified to account for spatially varying lattice
 $\mu_n n (\nabla \phi_n + P_n \nabla T_L)$
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module is being invoked, the electron and hole

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absolute thermoelectric powers for electrons and hol **nermal Current Densities**
BIGA module is being invoked, the electron and hole
are modified to account for spatially varying lattice
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SIGA module is being invoked, the electron and hole

re modified to account for spatially varying lattice
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are absolute thermoelectric po Fig. 12

Fig. 12

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 $\mu_n n (\nabla \phi_n + P_n \nabla T_L)$
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GIGA module is being invoked, the electron and hole

are modified to account for spatially varying lattice
 $=-q\mu_n n (\nabla \phi_n + P_n \nabla T_L)$
 $=-q\mu_p p (\nabla \phi_p + P_p \nabla T_L)$

are absolute thermoelectric pow rmal Current Densities

module is being invoked, the electron and hole

odified to account for spatially varying lattice
 $\mu_n n (\nabla \phi_n + P_n \nabla T_L)$
 $\mu_p p (\nabla \phi_p + P_p \nabla T_L)$

absolute thermoelectric powers for electrons and **Defined Current Densities**

GIGA module is being invoked, the electron and hole

are modified to account for spatially varying lattice
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 $=-q\mu_p p (\nabla \phi_p + P_p \nabla T_L)$

are absolute thermoelectric po

 n n n n L

□ Where P_n and P_p are absolute thermoelectric powers for electrons and holes and are calculated using:

5 ln 2 5 ln 2 *B c n n B v p p k N P KSN Q n k N P KSP Q p*

Wachutka, G.K., "Rigorous Thermodynamic Treatment of Heat Generation in Semiconductor Device Modeling", *IEEE Trans., Computer-Aided Design* Vol. 9, No. 11 (1990): 1141-1149.

Thermo-Electric Effects

When an electric current is passed through a conductor having a temperature gradient over its length, heat will be either absorbed by or expelled from the conductor.

> Thomson effect

Thermoelectric effect

Seebeck

effect

Seebeck effect is coupling of two potentials, the electrochemical potential and the temperature.

> Peltier illustrated that heat flux and electrical current can be coupled.

Peltier effect

Thermo-Electric Effects Explained

- □ When any two metals are connected together, a voltage is developed which is a function of the temperatures of the junctions and (mainly) the difference in temperatures.
- \Box It was later found that the Seebeck voltage is the sum of two effects: the *Peltier effect*, and the *Thompson effect.*
	- \blacksquare The **Peltier effect** explains a voltage generated in a junction of two metal wires.
	- **The Thompson effect** explains a voltage generated by the temperature gradient in the wires.

Peltier Effect: ZT Factor Over the Years

$$
ZT = S^2T \sigma/\kappa
$$

- \Box The 7T of a thermoelectric material is a dimensionless unit that is used to compare the efficiencies of various materials.
- \Box ZT is determined by three physical parameters:
	- the thermopower S (also known as Seebeck factor),
	- the electrical conductivity $σ$, the thermal conductivity $k = k_e + k_{ph}$ where the k_{e} and k_{ph} are the thermal conductivities of electrons and phonons, respectively,
	- and the absolute temperature T

Analogy Between Electrical and Thermal Variables

$$
J = \sigma E = -\sigma \frac{dV}{dx}
$$
: current density

$$
F = -\kappa \frac{dT}{dx}
$$
: heat flux

$$
\begin{cases} J \Leftrightarrow F \\ V \Leftrightarrow T \\ \sigma \Leftrightarrow \kappa \end{cases}
$$

Previous Work Done in Thermal Modeling

Previous Work in Thermal Modeling

- □ Mostly, the previous work performed and related to thermal modeling can be split into:
	- **□** Solutions of the Phonon Boltzmann Transport Equation
	- **■** Analysis of self-heating effects in devices

Phonon BTE Solvers

- *Peterson* performed a Monte Carlo Simulation for phonons in the Debye approximation and using single relaxation time
- *Mazumder and Majumdar* followed Peterson approach but included the dispersion relation and the different acoustic polarization branches
	- **Limit: The N and the U processes are not treated** separately although they do not contribute the same way to the thermal conductivity

^{*} Peterson, R. B. (1994). "Direct Simulation of Phonon-Mediated Heat Transfer in a Debye Crystal." *Journal of Heat Transfer*, Vol. 116(4), pp. 815-822.

^{*} Mazumder, S. and Majumdar, A. (2001). "Monte Carlo Study of Phonon Transport in Solid Thin Films Including Dispersion and Polarization." *Journal of Heat Transfer*, Vol.123(4), pp. 749-759.

Phonon BTE Solvers, Cont'd

□ Lacroix further generalized the model:

By incorporation of N and U processes

T Transient conditions are also being considered

Lacroix, D., Joulain, K. and Lemonnier, D. (2005). "Monte Carlo Transient Phonon Transport in Silicon and Germanium at Nanoscales." *Physical Review B*, Vol. 72(6), pp. 064305/1-11.

Modeling Self-Heating in Devices

Work of *Eric Pop, Goodson, Robert Dutton*

- Non-parabolic model with analytical phonon dispersion
- **E** study heat transfer and energy conversion processes at nanoscales. Applications include semiconductor devices and packaging, thermoelectric and photonic energy conversion, and microfluidic heat exchangers.

Work of *Kelsall and Sadi*

E Nanoscale transistors, GaN HEMTs

Popova Sapka Ski Resort, Tetovo, Republic of Macedonia

The ASU Model to Addressing Self-Heating

Theoretical Model

Application of the Model to Modeling of:

FD SOI Devices, Dual Gate Structures, SOD and SOAlN Devices

Nanowire Transistors

GaN HEMTs

Theoretical Model

Theoretical Model
\n
$$
\left(\frac{\partial}{\partial t} + v_e(k) \cdot \nabla_r + \frac{e}{\hbar} E(r) \cdot \nabla_k \right) f = \sum_{\{w_{e,q}^{k+q} \to k+w_{a,q}^{k+q} \to k-w_{e,q}^{k+q} - w_{e,q}^{k+q} - w_{a,q}^{k+q} \} }{\left(\frac{\partial}{\partial t} + v_p(q) \cdot \nabla_r \right) g = \sum_{k} \left\{ w_{e,q}^{k+q+1} - w_{a,q}^{k+q+1} \right\} + \left(\frac{\partial g}{\partial t} \right)_{p-p}
$$
\nJ. Lai and A. Majumdar, "Concurrent thermal and electrical modeling of submicrometer silicon devices", J.
\nAppl. Phys., Vol. 79, 7353 (1996).
\n
$$
C_{LO} \frac{\partial T_{LO}}{\partial t} = \frac{3nk_B}{2} \left(\frac{T_e - T_L}{\tau_{e-LO}} \right) + \frac{nm^* v_d^2}{2\tau_{e-LO}} - C_{LO} \left(\frac{T_{LO} - T_A}{\tau_{LO-A}} \right),
$$
\n
$$
C_A \frac{\partial T_A}{\partial t} = \nabla \cdot (k_A \nabla T_A) + C_{LO} \left(\frac{T_{LO} - T_A}{\tau_{LO-A}} \right) + \frac{3nk_B}{2} \left(\frac{T_e - T_L}{\tau_{e-L}} \right).
$$

J. Lai and A. Majumdar, "Concurent thermal and electrical modeling of submicrometer silicon devices", J.

$$
\text{Appl. Phys. , Vol. 79, 7353 (1996).}
$$
\n
$$
C_{LO} \frac{\partial T_{LO}}{\partial t} = \frac{3nk_B}{2} \left(\frac{T_e - T_L}{\tau_{e-LO}} \right) + \frac{nm \cdot v_d^2}{2\tau_{e-LO}} - C_{LO} \left(\frac{T_{LO} - T_A}{\tau_{LO-A}} \right),
$$
\n
$$
C_A \frac{\partial T_A}{\partial t} = \nabla \cdot (k_A \nabla T_A) + C_{LO} \left(\frac{T_{LO} - T_A}{\tau_{LO-A}} \right) + \frac{3nk_B}{2} \left(\frac{T_e - T_L}{\tau_{e-L}} \right).
$$

K. Raleva, D. Vasileska, S. M. Goodnick and M. Nedjalkov, Modeling Thermal Effects in Nanodevices, IEEE Transactions on Electron Devices, vol. 55, issue 6, pp. 1306-1316, June 2008.

Theoretical Model …

Heat Diffusion

Gain term due to optical phonons

Gain term due to electrons (omitted if acoustic phonon scattering is treated as elastic scattering process)

Theoretical Model …

K. Raleva, D. Vasileska, S. M. Goodnick and M. Nedjalkov, Modeling Thermal Effects in Nanodevices, IEEE Transactions on Electron Devices, vol. 55, issue 6, pp. 1306-1316, June 2008.

Theoretical Model …

□ Gummel cycles

K. Raleva, D. Vasileska, S. M. Goodnick and M. Nedjalkov, Modeling Thermal Effects in Nanodevices, IEEE Transactions on Electron Devices, vol. 55, issue 6, pp. 1306-1316, June 2008.

Theoretical Model: Thermal Conductivity

 \Box Solid transmit thermal energy by two modes, either one of which, or both, may operate.

- 1. In all solids, energy may be transferred by means of elastic vibrations of the lattice moving through the crystal in the form of waves .
- 2. In some solids , notably metals , free electrons moving through the lattice also carry energy in a manner similar to thermal conduction by a True gas phase .

Thermal Conductivity:
$$
k = k_e + k_p
$$

Thermal Conductivity

$$
k_p = \frac{1}{3} C \times I
$$

8
Specific heat
Sound velocity

If $T > \Theta$, **C** ~ *constant* If $T \ll \Theta$, **C** ~ T ^d (d: dimension) Specific heat :

Mean free path:
$$
\frac{1}{l} = \frac{1}{l_{st}} + \frac{1}{l_{um}}
$$

 l_{st} \sim constant Static scattering (phonon -- defect, boundary):

Umklapp phonon scattering: $I_{\text{U}m} \sim e^{\Theta/T}$

Thermal Conductivity of Thin Films

Analytical Model for Thin Films

$$
\kappa(z) = \kappa_0(T) \int_0^{\pi/2} \sin^3 \theta \left\{ 1 - \exp\left(-\frac{a}{2\lambda(T)\cos\theta} \right) \cosh\left(\frac{a - 2z}{2\lambda(T)\cos\theta} \right) \right\} d\theta
$$

 $\lambda(T) = \lambda_0(300/T)$

$$
\kappa_0(T) = \frac{135}{a + bT + cT^2}
$$
 W/m/K

Metals", Advances in Physics, Vol. 1, no. 1, Jan. 1952, reprinted in Advances in Physics, Vol. 50, pp. 499-537, 2001.

• M. Asheghi,., M. N. Touzelbaev., K. E. Goodson, Y. K. Leung, and S. S. Wong., "Temperature Dependent Thermal Conductivity of Single-Crystal Silicon Layers in SOI Substrates," ASME Journal of Heat Transfer, Vol.120, pp. 30-33, 1998.

Theoretical Model – Phonon Dispersions

E. Pop, R.W Dutton, K.E. Goodson, ["Analytic Band Monte Carlo Model for Electron Transport in Si Including Acoustic and Optical Phonon Dispersion,](http://poplab.ece.illinois.edu/pdfs/epop-jap-v96nov04.pdf)" *J. Appl. Phys.* **96**, 4998 (2004)
Phonon Dispersions: Proof of Concept

Drift Velocity in Silicon at T=77K Mobility at T=77K

Phonon Dispersions: Proof of Concept

Drift Velocity in Silicon at T=300K Mobility at T=300K

FULLY DEPLETED SOI DEVICES

Lake Powell, Arizona

Simulation Results: FD SOI Devices

□ 25 nm Channel Length Device

K. Raleva, D. Vasileska, S. M. Goodnick and T. Dzekov, "Modeling thermal effects in nano-devices", *Journal of Computational Electronics, DOI 10.1007/s10825-008-0189-3 © Springer Science+Business Media LLC 2008, J. Computational Electronics,* Vol. 7, pp. 226-230 (2008).

Carriers are in the velocity overshoot

Heat Dissipation Across Technology Nodes

Parameter is the temperature on the Gate Electrode.

Neumann Boundary Conditions are imposed at the Artificial Boundaries and the Source and Drain contacts

Can We Lower Self-Heating Effects?

 Dual-Gate Devices □ SOI vs. SOD vs. SOAIN

S.M. Goodnick, D. Vasileska, K. Raleva, "Is Dual Gate Device Better From a Thermal Perspective?", *Proceedings of 2008 SISPAD Conference*, pp. 125 - 128.

K. Raleva, D. Vasileska, S. M. Goodnick, Is SOD Technology the Solution to Heating Problems in SOI Devices?, Electron Device Letters, IEEE, Volume 29, Issue 6, June 2008 Page(s):621 - 624.

Dual-Gate SOI Devices

S.M. Goodnick, D. Vasileska, K. Raleva, "Is Dual Gate Device Better From a Thermal Perspective?", *Proceedings of the 2008 SISPAD Conference*, pp. 125 - 128.

A Closer Look …

Single gate lattice temperature profile

temperature profile

Where Does the Benefit of the DG Structure Come From?

25nm FD SOI nMOSFET

25nm DG SOI nMOSFET

For almost the same Current degradation DG devices offer **1.5-1.7** times more current

SOI vs. SOD vs. SOAlN

Silicon-On-Diamond and Silicon-On-Aluminum Nitride (SOAlN) Technologies as viable alternatives to Silicon-On-Insulator Devices

Standard Si technology

SOD technology

Current Degradation

K. Raleva, D. Vasileska, S. M. Goodnick, Is SOD Technology the Solution to Heating Problems in SOI Devices?, Electron Device Letters, IEEE, Volume 29, Issue 6, June 2008 Page(s):621 - 624.

Heat Spreading

NANOWIRE TRANSISTORS

Lake Powell, Arizona

Nanowires – The Role of the Contacts

D. Vasileska, A. Hossain and S. M. Goodnick, *ECS Transactions*, Volume 31, No. 1, pp. 83-91 (September 2010).

Nanowires – Unintentional Dopant

Gate Contact

SINGLE IMPURITY IMPACT

Screening of the source charges Reduces the impact of the negative trap.

Maximal impact

Unintentional Dopant

GaN HEMTS

Rainbow Bridge, Arizona

Why GaN HEMTs?

Promising Microwave Power Device

Simulation Results: GaN HEMTs

□ Why GaN HEMTs?

• Where Gallium Nitride Outstrips **Other Semiconductor Materials**

^a The compounds are loosely known as indium-based.

Problems With GaN HEMTs

Current Collapse induced in GaN HEMT device characteristics as a result of shortterm (*~10 hours***) DC bias stress**.

Trapping of hot electrons by trap/defect sites in the AlGaN buffer layer as well as GaN substrate reduces the net polarization charge.

> J. A. del Alamo and J. Joh, GaN HEMT reliability, Microelectronics Reliability, Volume 49, Issues 9-11, September-November 2009, Pages 1200-1206.

Problems With GaN HEMTs …

MODELING REQUIREMENTS

INCORPORATION OF ELECTROMECHANICAL COUPLING direct **Stress** piezoelectric σ_{jk} effect Piezoelectric Moduli Piezoelectric Constants

SELF-HEATING EFFECT

GaN HEMTs Basics

□ Wurtzite AlGaN/GaN Ga-face N-face Ga 00001 70001 **Substrate Substrate**

AlGaN/GaN grown on sapphire by MOCVD is always Ga-faced, but material grown by MBE can have either Ga- or N-faced surface depending on the existence of AIN nucleation layer.

GaN HEMTs Basics …

□ Spontaneous and Piezoelectric Polarization Charge

□ What is different in GaN HEMTs ...

Depth, nm

\square Large sheet electron densities

heterostructures vs. Al content *x*

Electro-mechanical coupling model developed at ASU

Energy relaxation processes

Acoustic and optical phonon bath

Energy balance Equation Solver for Phonons

Optical Phonon Lifetime \rightarrow function of carrier density n(i,j)

Carrier density dependant phonon lifetimes results in an indirect dependence of the choice of SCATTERING MECHANISM on the CARRIER DENSITIES

Flow-chart of Electro-thermal simulator

Exchange of variables between solvers

Modifications to our existing Monte Carlo Simulator

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- **Temperature dependent Scattering Tables.**
- **Averaging and smoothing of electron density, drift velocity and electron energy for solving phonon balance equations.**
- **Density dependent phonon lifetimes – analytical model fitted to experimental values.**

Simulated structure

 $\leftarrow 0.25$ um \rightarrow

Gate

J. A. del Alamo structure

Source

I_d-V_G Characteristic

I_d-V_d characteristic

Electron temperature map

Acoustic phonon temperature map

Current collapse

Supporting Evidence: Id-Vd curve

Mechanism responsible for current collapse

Length of the device (nm)

Electric Field Profile in the device with (a) 0.05 µm and (b) 0.4 µm shield lengths respectively

Vertical component of the Electric field at the gate drain edge Vs. field plate length

 $0.3_{0.9}$

 0.8

 0.7

 0.6

 0.5

Distance along the Length of the Device (um)

 0.4

 0.3

 0.2

 0.1

350

300

 $\overline{\mathbf{0}}$

Electric Field Profile in the device for a shield length of 0.1 µm (a) 20 nm and (b) 60 nm shield dielectric lengths respectively

Electric Field Profile in the device for a shield length of 0.4 µm (a) 20 nm and (b) 60 nm shield dielectric lengths respectively

Vertical component of the Electric field at the gate drain edge Vs. shield dielectric thickness for varying field plate length

• As the shield length increases, the electric field near the critical gate-drain edge reduces. This is because, as the shield electrode length increases, it spreads the electric field over a wider region.

• As the shield dielectric thickness increases, its ability to capacitively couple the electric field with the structure reduces. This results in increase in the electric field near the gate drain edge for a given shield plate length.

• As the field near the gate-drain edge reduces, the potential for electron trapping in the defect sites also reduces and improves the reliability performance of the device structure.

the field plate length is increased the electric field at the gate edge is reduced.

• We also observe that the electric field at the shield edge keeps increasing as its length increases. This is due to the fact that the edge of the shield plate is getting closer to the drain electrode.

Effective Electric field in the AlGaN Layer for various field plate lengths

PROPOSED RESEARCH AT ASU

Proposed Tasks

- Creation of regional scattering tables near the PITS and CRACKS
- Formulation of DEFORMATION POTENTIAL THEORY from results obtained with first principle calculations

Basic Elements of Device Simulation Proposed Research …

- **Develop theoretical understanding for the formation of cracks in GaN HEMTs**
- **Approach:**
	- **Semiconductor device simulation** to get the electric field profiles in the critical device region
	- Use these external fields into the **molecular dynamics calculations** to see if they are sufficient to nucleate a crack or a permanent defect

– **The transport module coupled to the electromagnetic fields solver**

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- Self-heating effects are important factor that must be accounted for as they limit device lifetime
- **I** In ultra-nanoscale devices, due to the ballistic transport of the carriers, the heat dissipation occurs at the contacts **(thermal Landauer picture)**
- **In GaN HEMTs heat plays** considerable role with respect of the observation of the current collapse phenomena by modifying the vertical electric fields

Lake Ohrid, Republic of Macedonia

Conclusions

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