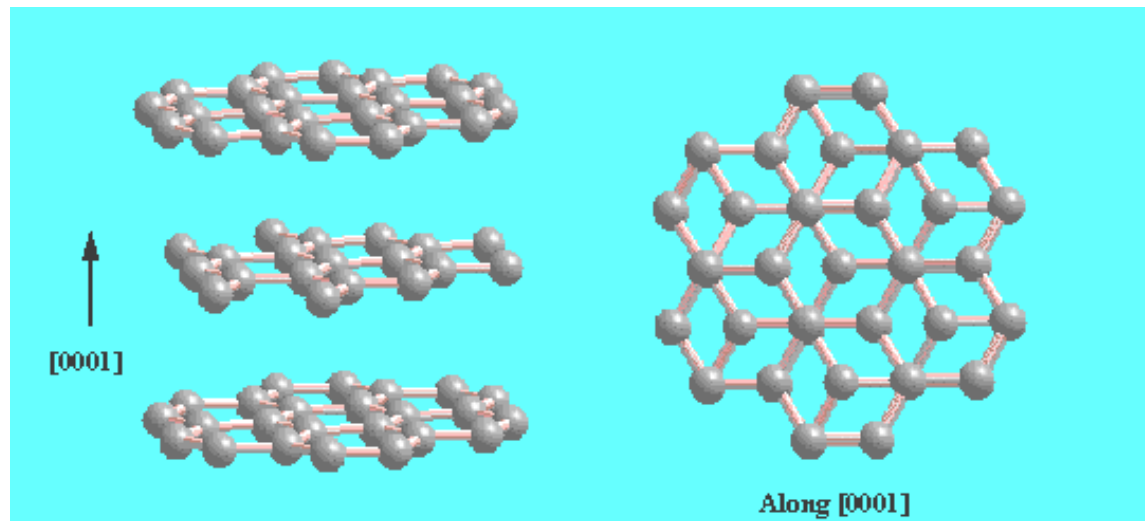

Structure and Mechanical Properties of sp^2 -bonded Nanotubes

B. G. Demczyk

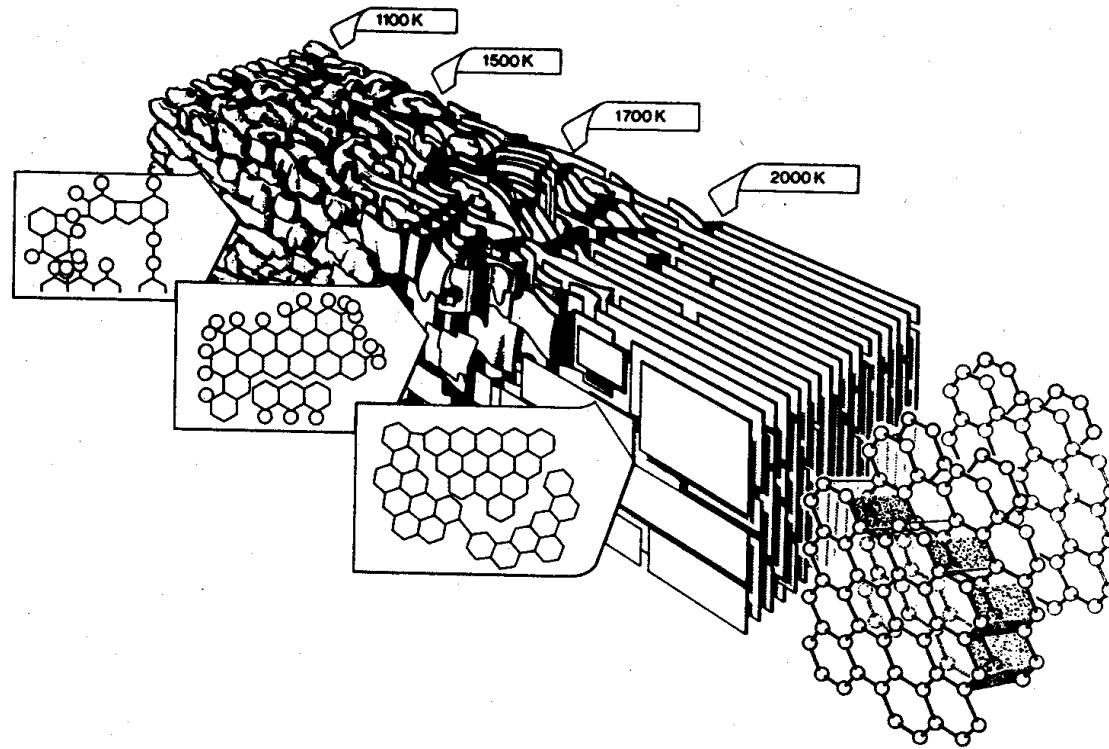
Graphite Structure



B.L. = 0.142 nm (diamond, 0.154 nm)

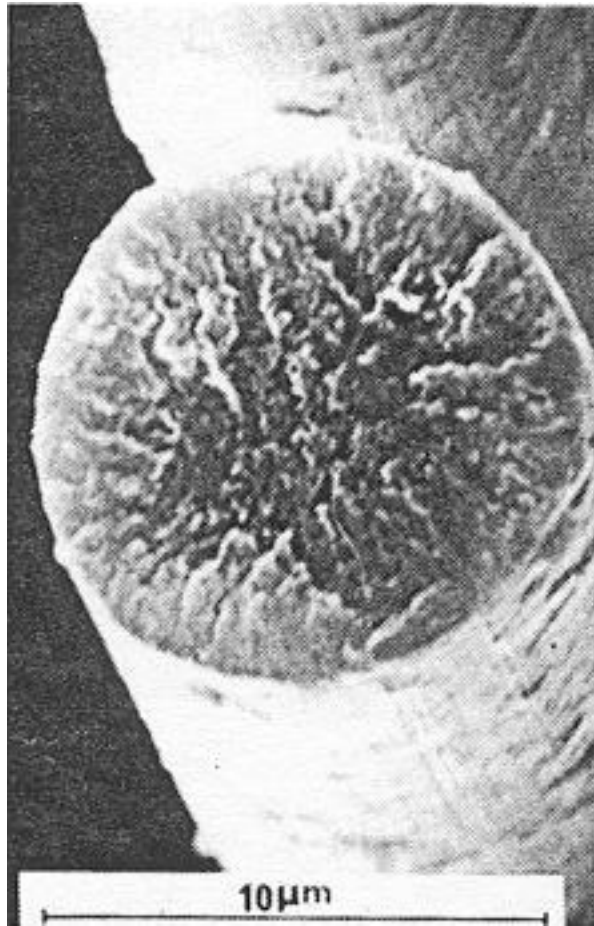
Crystal structure of graphite. The in-plane C-C covalent bond strength is the highest found in nature, but the van der Waals layer to layer bonds are weak.

Carbon Fiber

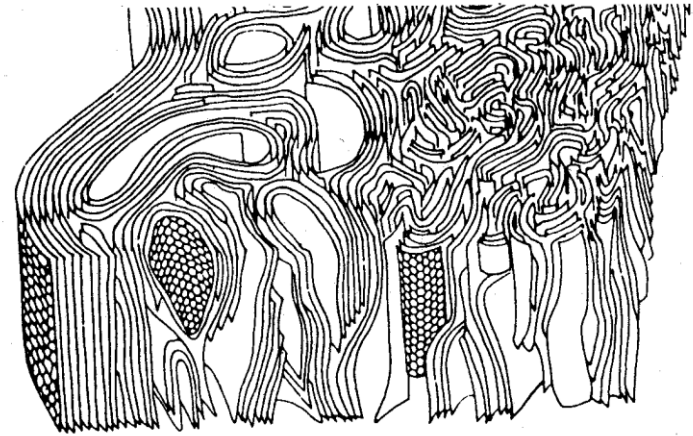


Schematic idealized structure of a carbon fiber, where the strong C-C bonds lie along the length of the fiber.

Carbon Fibers



SEM Image



Defect Structure



Tensile Strength

Cohesive Strength

(0.33 TPa) $\sigma_c = E\lambda / 2\pi a_o (\approx E / \pi)$

E = Young's Modulus (1026 GPa)

λ = interatomic force period ($\sim a_o / 2$)

a_o = interatomic separation (0.213 nm)

Fracture Strength (Orowan-Polanyi)

(0.14-0.18 TPa) $\sigma_f = \sqrt{E\gamma} / a (\approx E / 7 - E / 5)^*$

γ = Surface energy (4.2 J/m²)

a = interplanar separation

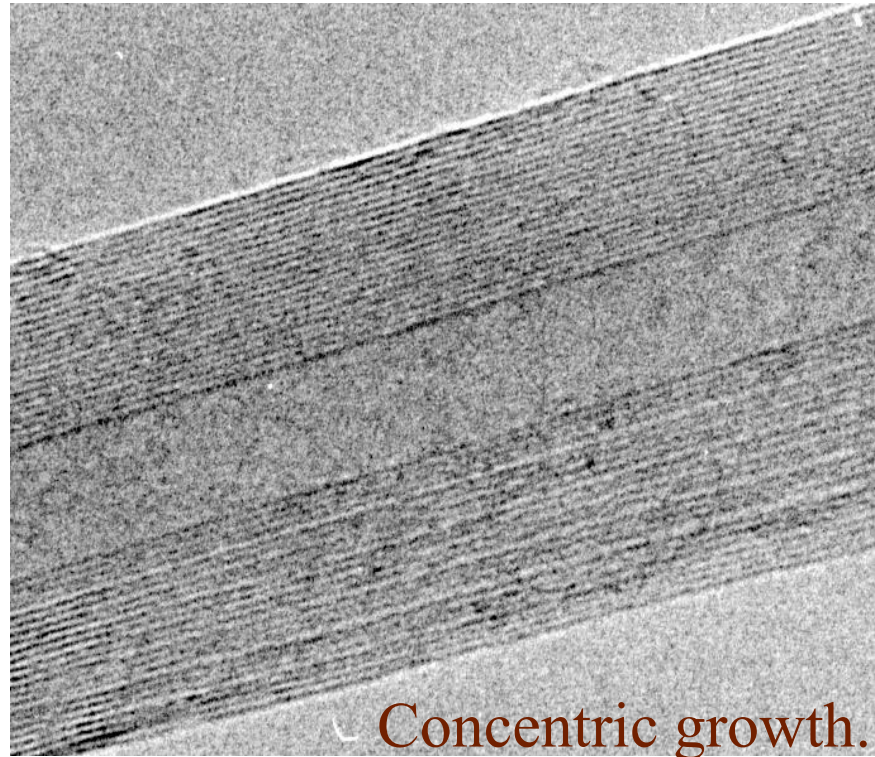
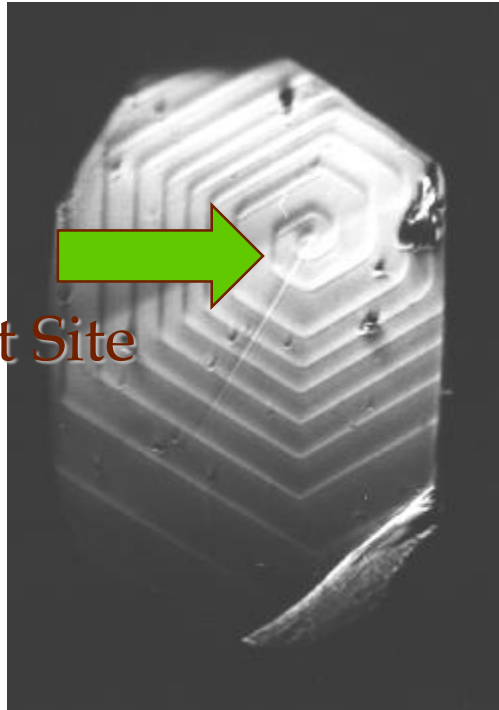
*Rep. Prog. Phys. 12 185 (1949).

Relative Strengths of Carbon Fibers

Steel	1-2 GPa
Carbon Fiber	2-5 GPa
Carbon Whisker	up to 20 GPa
Carbon Nano tube	~ 300 GPa
Theoretical (C-C bond) Strength	>1000 GPa

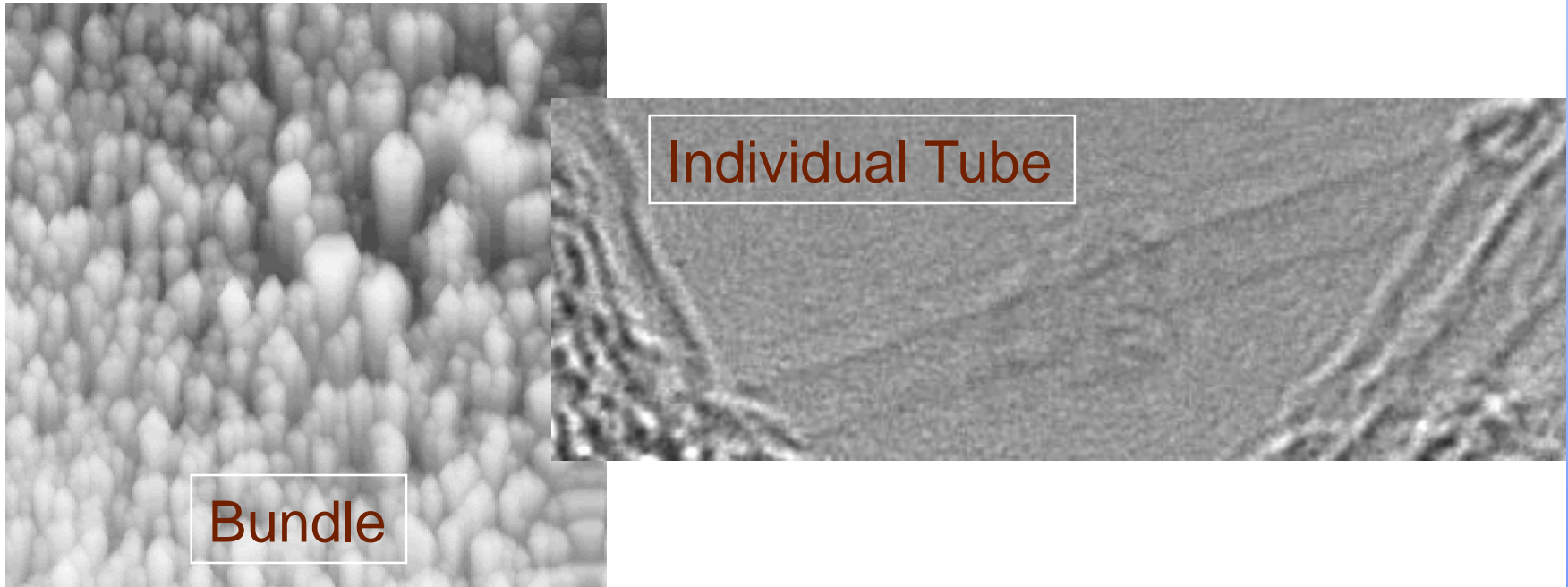
=> structural defects limit U.T.S

Fine Fibers (Whiskers) and Nanotubes



The continuity of atomic planes along the tube axis enhance the mechanical strength.

Single Wall Carbon Tube



CVD grown (~ 600 °C): $C_2H_4 \rightarrow (Fe(Mo)) \rightarrow C(s) + H_2$
- "nanoswitch" (Nantero); transistor (Nanõmix)

Ia. Multi-Walled C Nanotube Structure (Historical-U. Mich.)

■ Nanotube Growth:

➤ Arc (110A, 30-45VDC) between graphite rods in He atm (320 Torr)

■ (J. Cryst. Growth. 141 304 (1994))

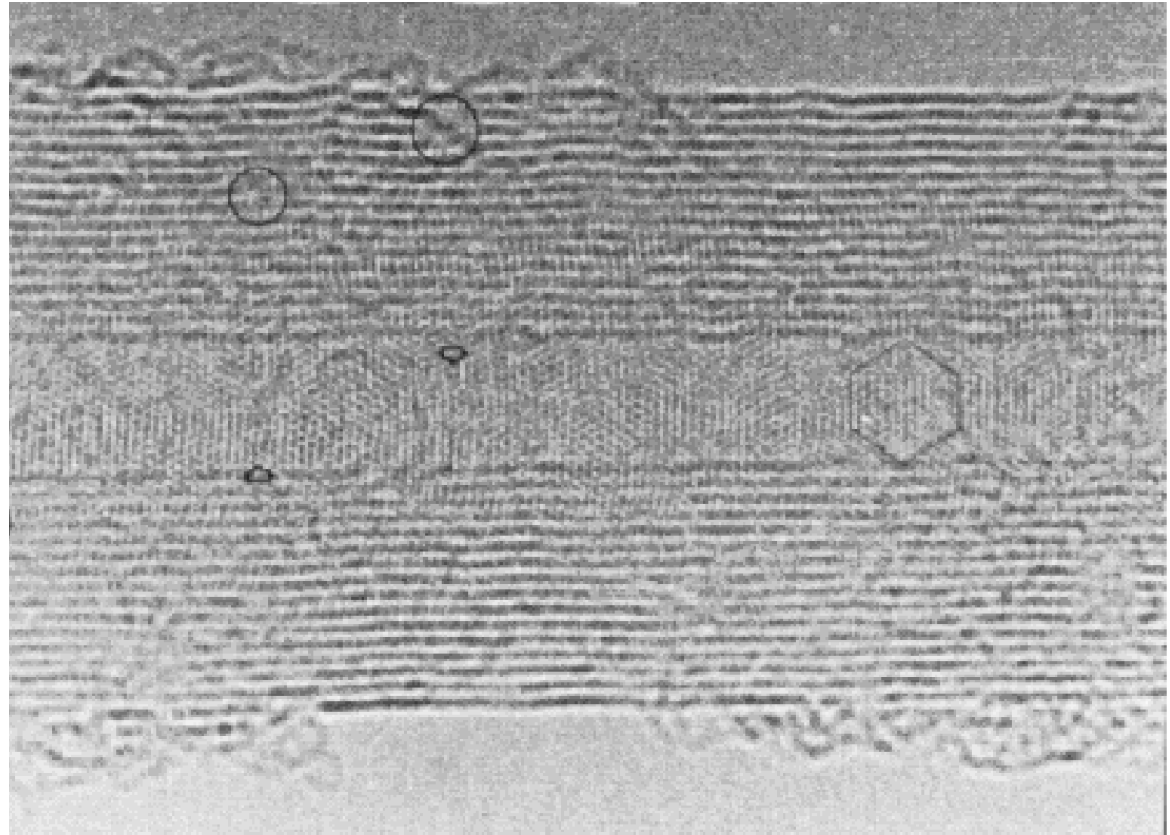
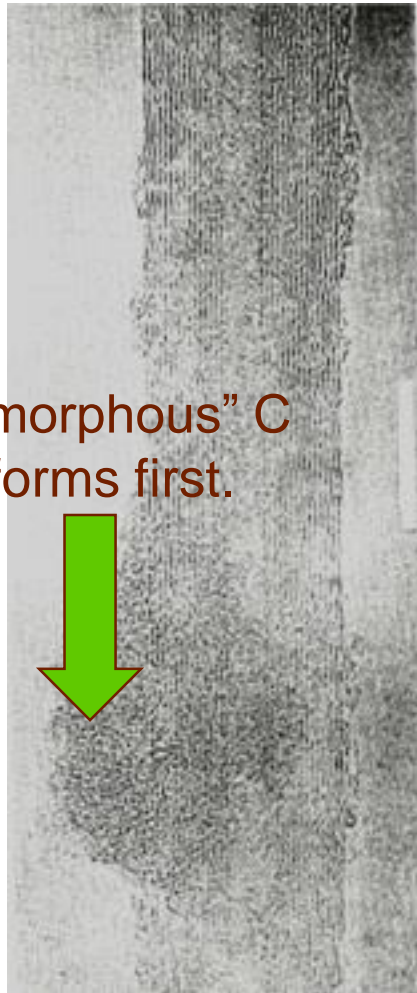
■ Nanotube HRTEM Characterization

➤ JEOL 4000EX* LaB₆ (400 kV)

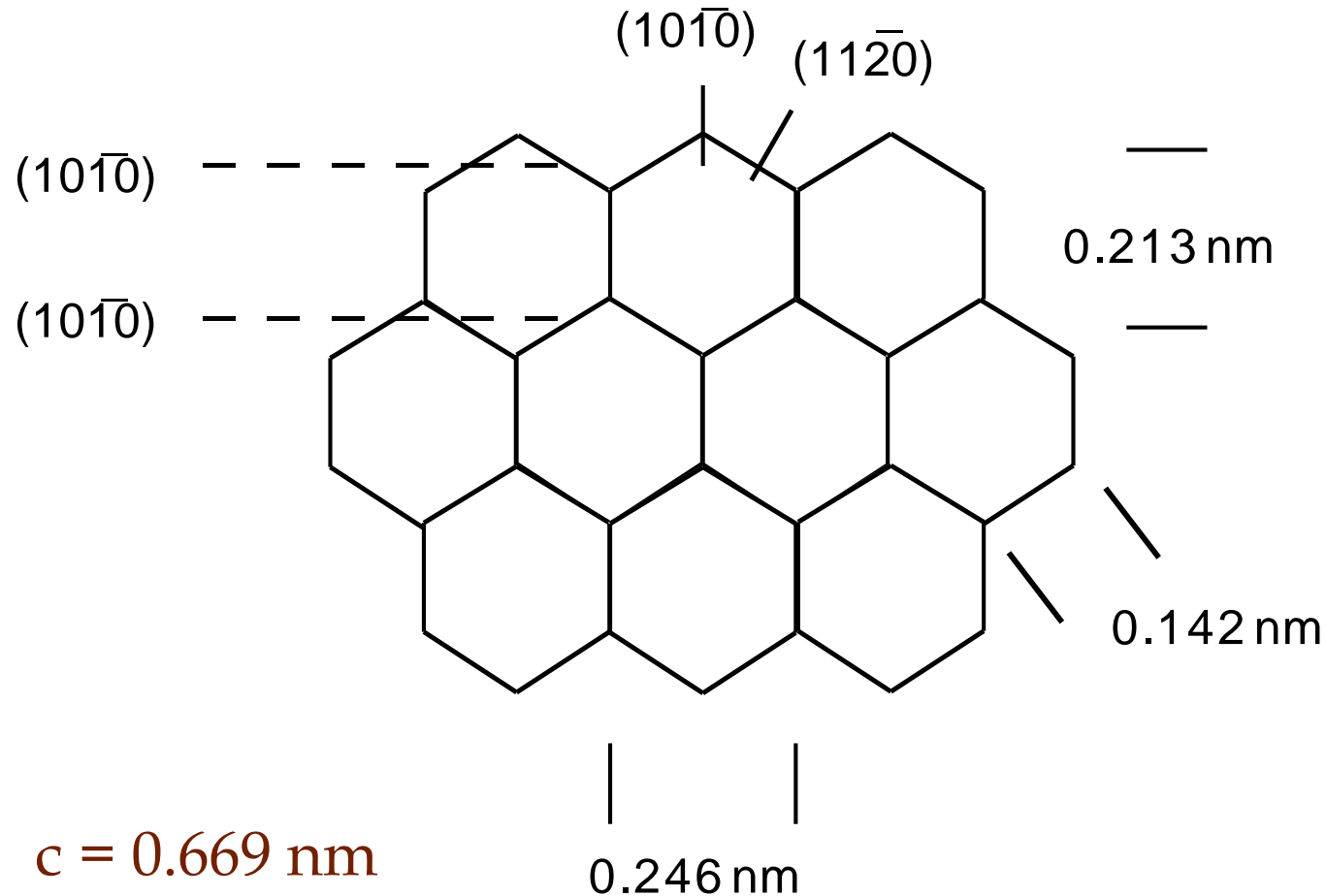
- 0.175 nm point resolution

*-commercial ARM

Nanotube HREM Images



Graphene Structure

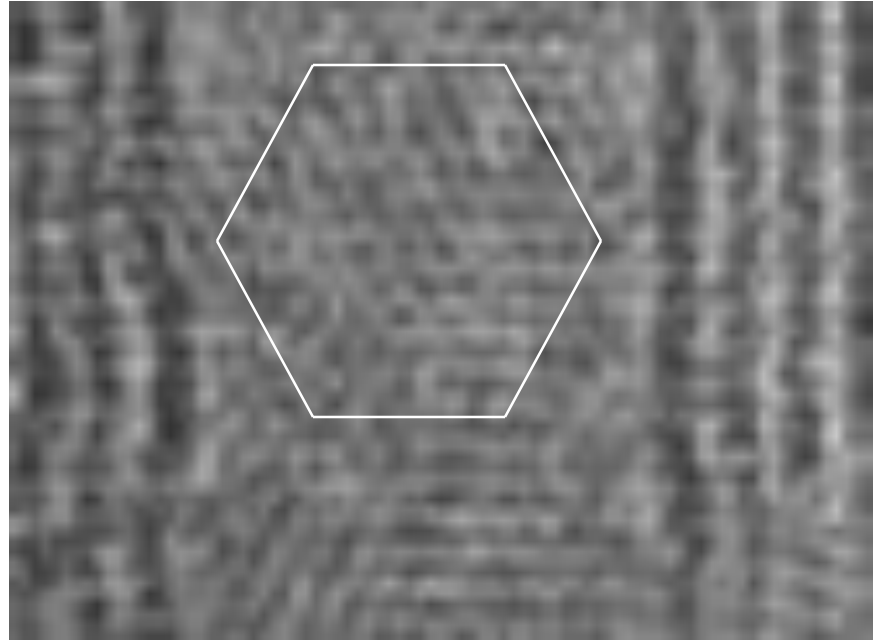
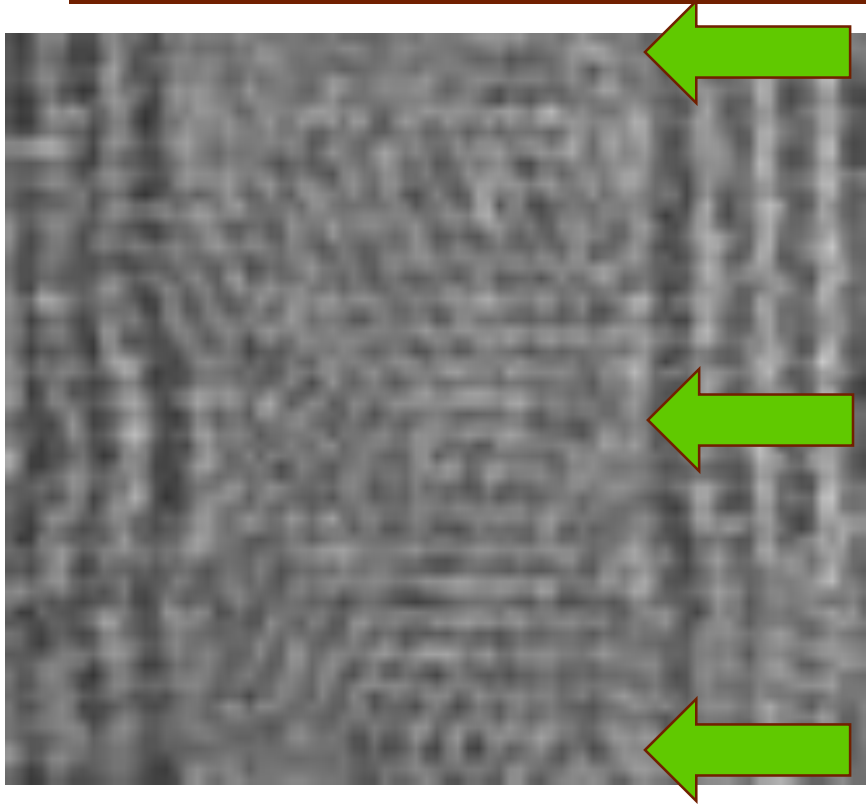


But in the Microscope...



... due to instrument resolution limit (0.175 nm)

Moire Patterns



$$D = \frac{d_1 d_2}{(d_1^2 + d_2^2 - 2d_1 d_2 \cos \alpha)^{0.5}}$$

=>Evidence of helicity variation ($\pm 3^\circ$) within tube.

Helicity (to maintain closure)

■ Initial cylinder circumference

$$(OX_1) : \quad 2\pi r_o = n_o a$$

- r_o - radius of inner cylinder
- n_o - # of edge sharing hexagons

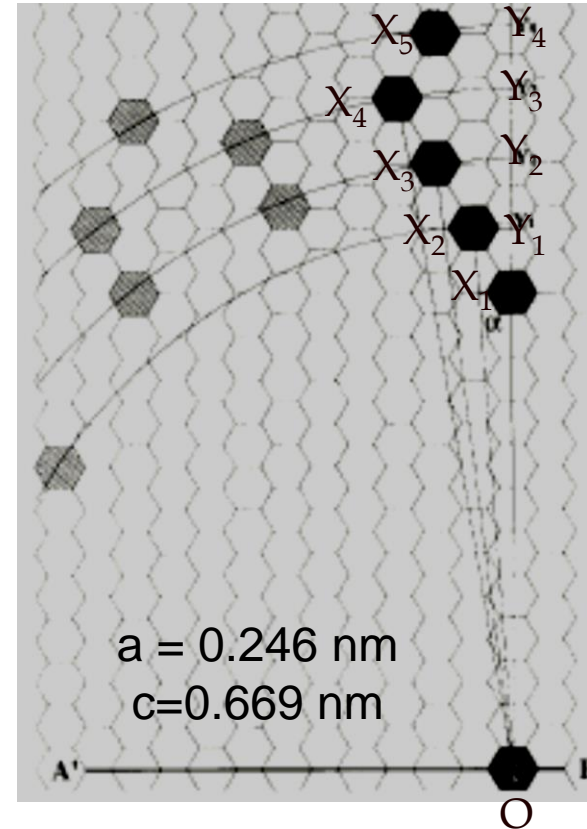
➤ Next:

$$OY_1 = n_o a + \pi c \quad (O \rightarrow X_2)$$

➤ $\alpha_1 = \tan^{-1}(X_2 Y_1 / OY_1) = \text{helicity}$

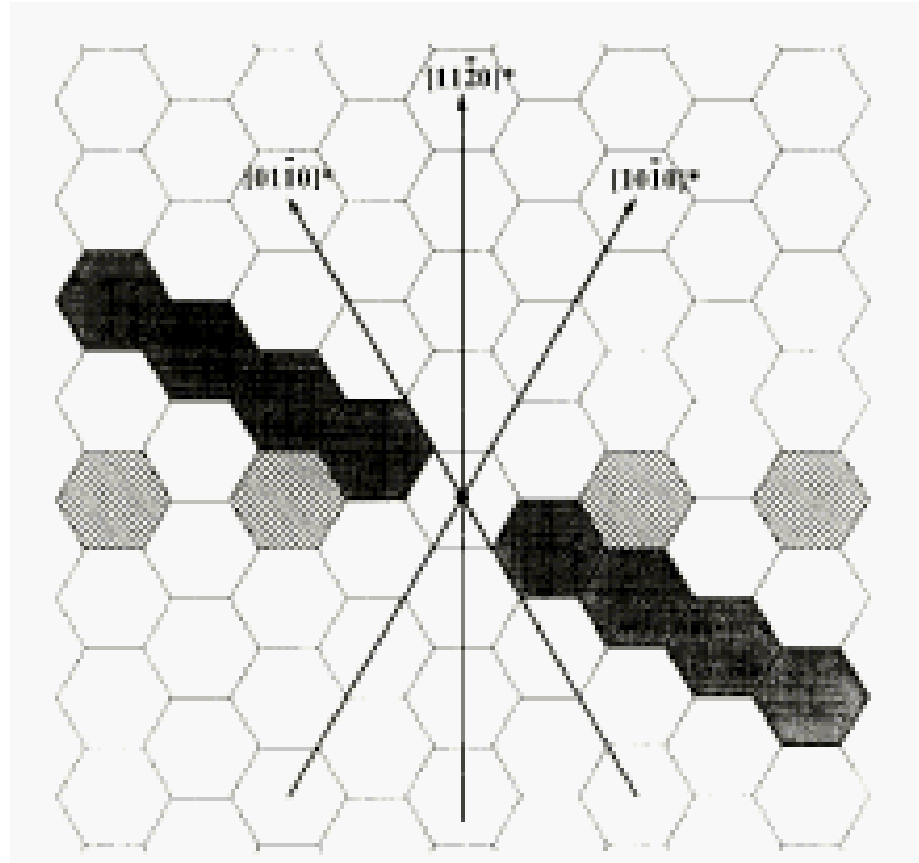
➤ Then:

$$OY_2 = n_o a + 2\pi c \quad (O \rightarrow X_3)$$



\Rightarrow Get both nonhelical and helical tubes

2 Ways to “Roll-up” Graphene



“Zig-Zag” $(10\bar{1}0)$

$$n_z = \pi c/a (=8.43)$$

“Armchair” $(11\bar{2}0)$

$$n_a = 2\pi c/a\sqrt{3} (=9.86)$$

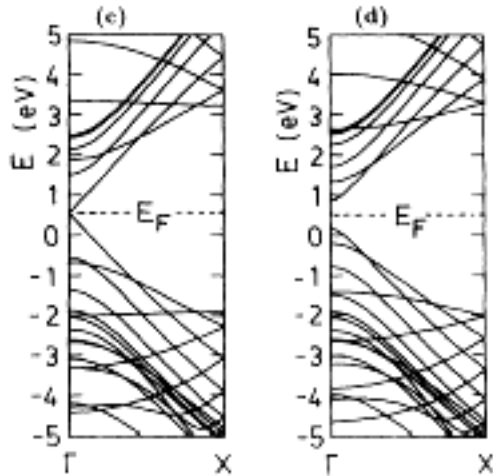
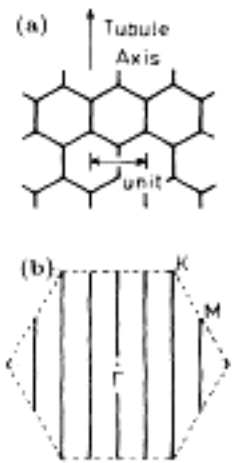
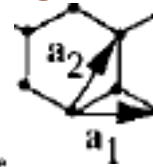
J. Cryst. Growth. 130 368 (1993).

$n_i = \#$ extra hexagon rows/tube

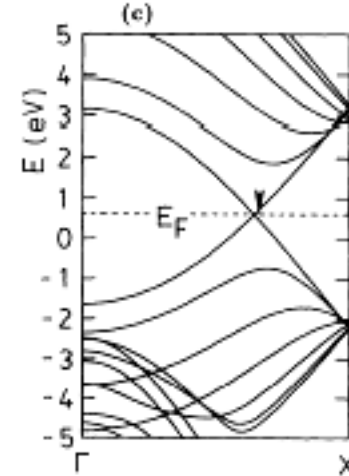
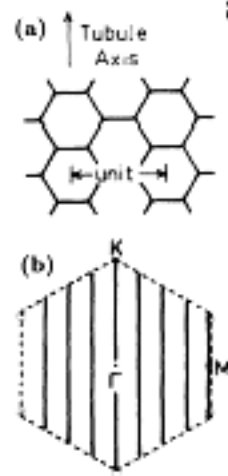
CNT Brillion Zone

“Roll-up” determines conducting properties

$$C = na_1 + ma_2$$



n or $m = 0$ (“zig-zag”)
 \Rightarrow metallic or semiconductor



$n = m$ (“armchair”)
 \Rightarrow metallic

(Local) Diffraction Information from HREM

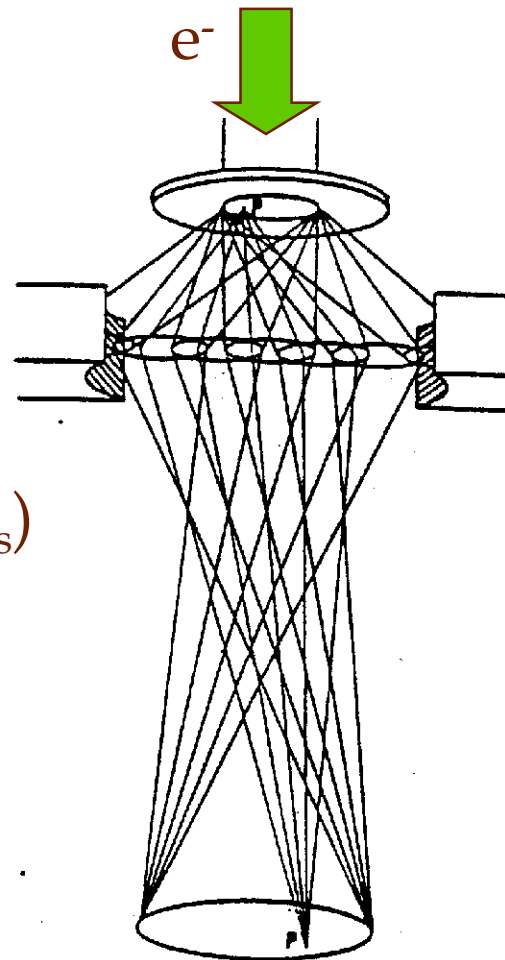
In-situ

Specimen, φ

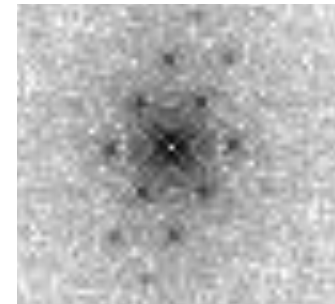
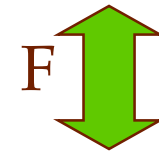
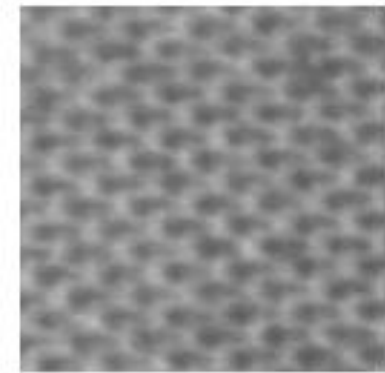
Objective Lens, φ_s

Diffraction Pattern, $f \approx F(\varphi_s)$

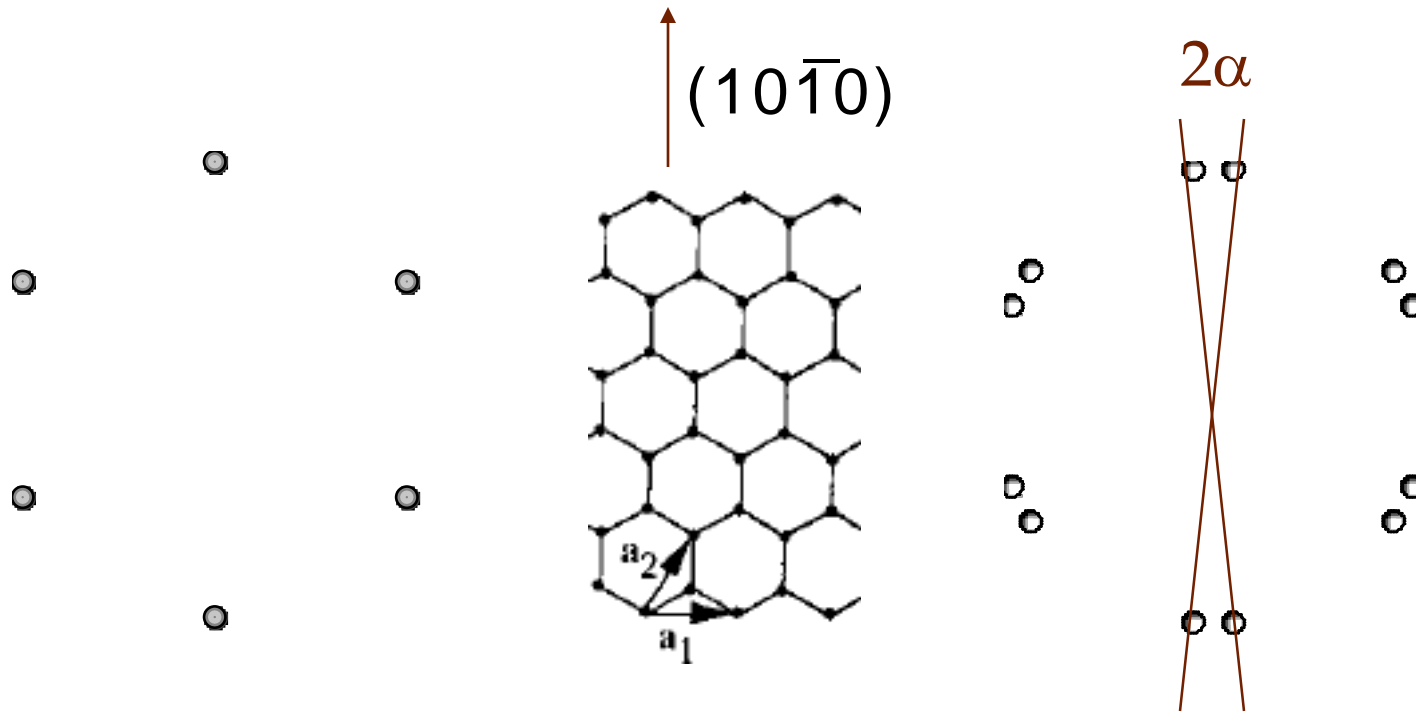
Image, $\varphi_m \approx F^{-1}(f)$



Ex-situ



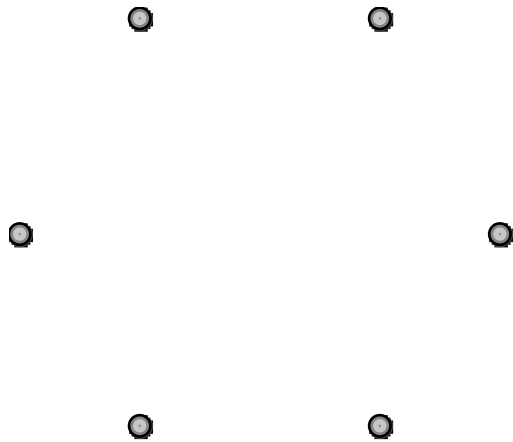
Diffraction-“Zig-Zag” Tubes



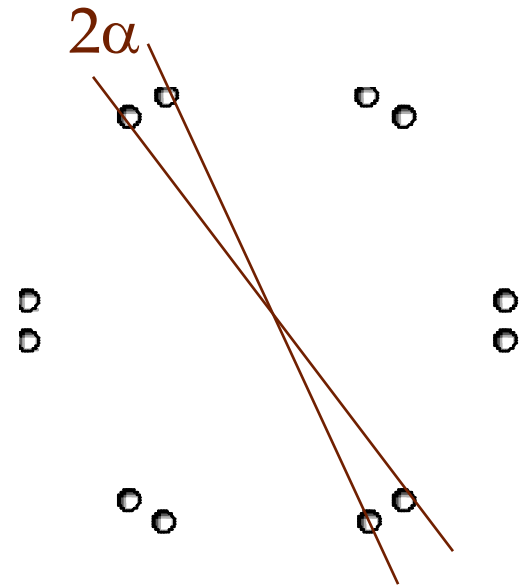
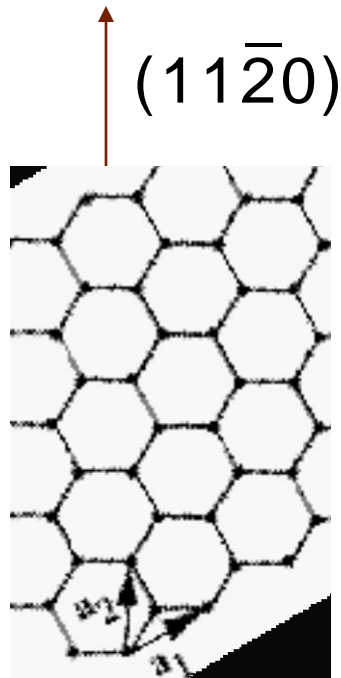
Non-Helical

Helicity, α

Diffraction-"Armchair" Tubes

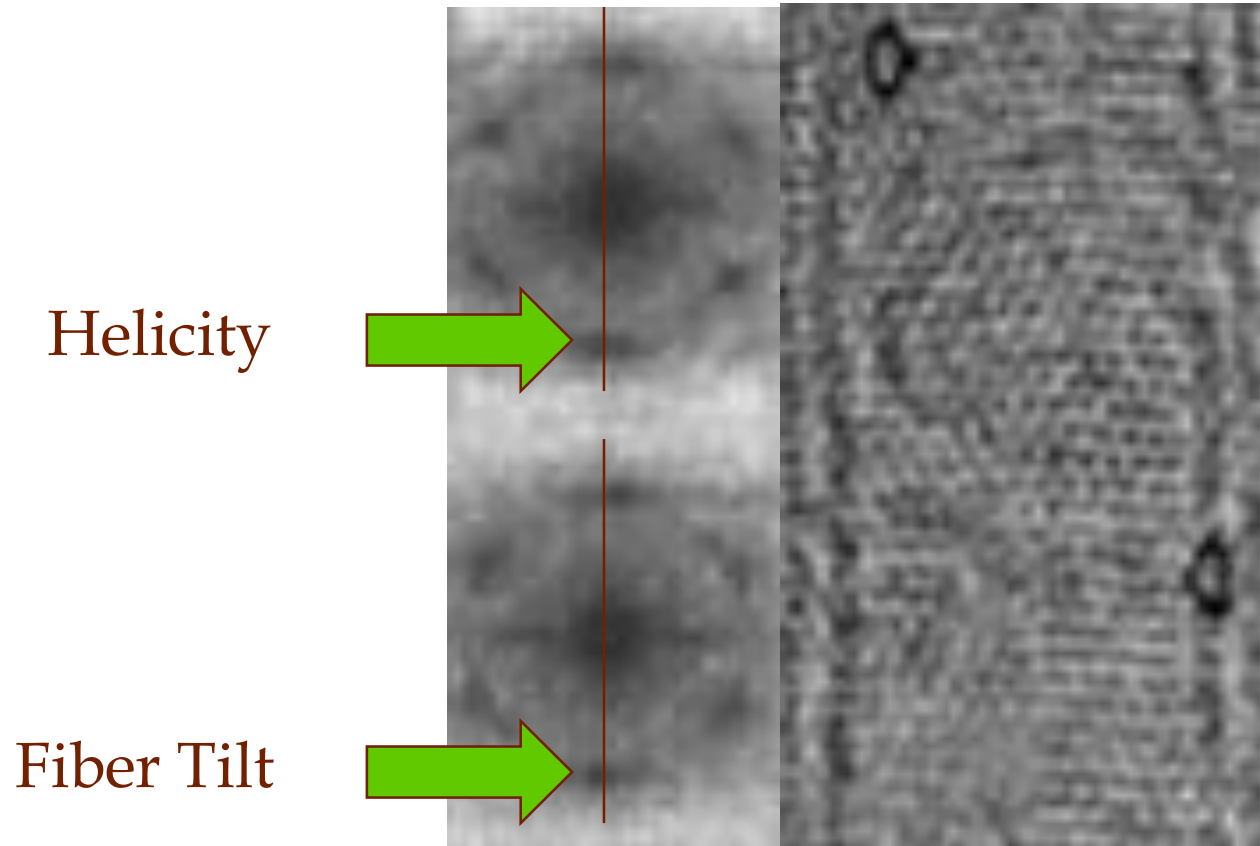


Non-Helical

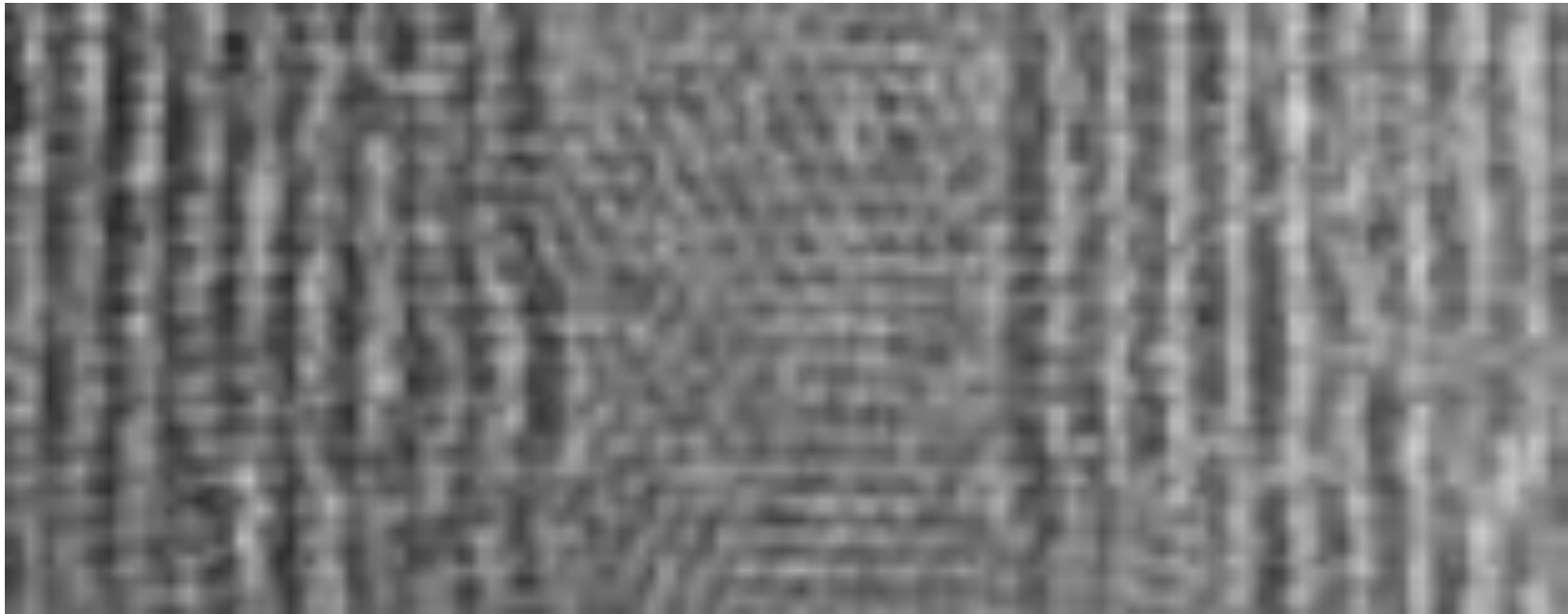
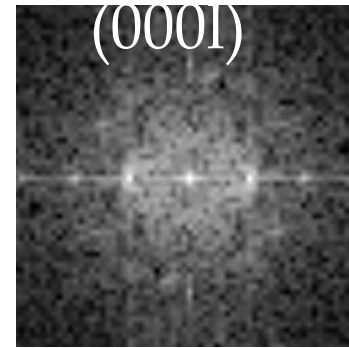
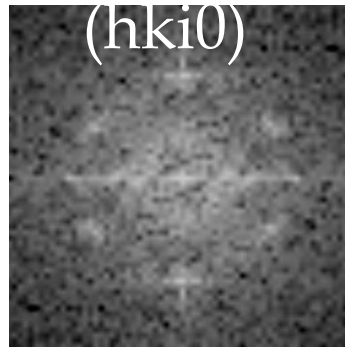
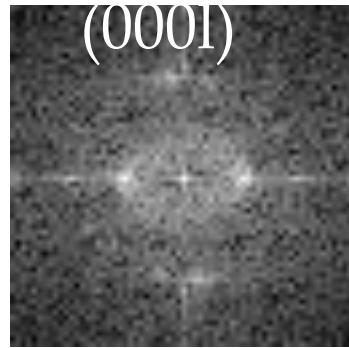


Helicity, α

Axially...

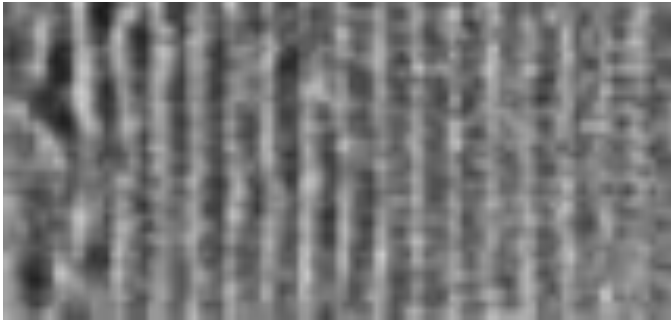


Radially...

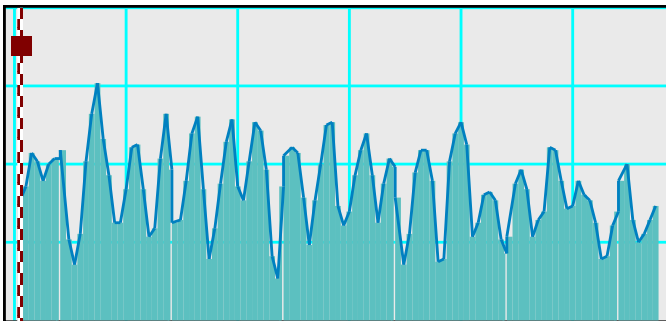


Spacing Variation

Over 300 pixels,
 $c = 0.375 \pm 0.004$ nm



=> gives overall nonhelical
fiber
every second tube has slight helicity



Tube #	d (nm)	n ($=\pi d/a$)	α ($=\tan^{-1}[\pi d/a]$)
1	3.17	40.5	1.2
2	3.91	50	0
3	4.66	59.5	0.8

CNT Structure Summary

- 10.0 (zig-zag) growth axis
 - 0.375nm *c-axis* spacing
 - To maintain overall zero helicity
- Helicity can vary not only in successive nanotubes, but also locally within a single tube

1b. CNT Structure (NCEM)

■ Nanotube Growth:

- Arc (60A, 30-45VDC) between B-doped C anode N₂ atm (380 T)

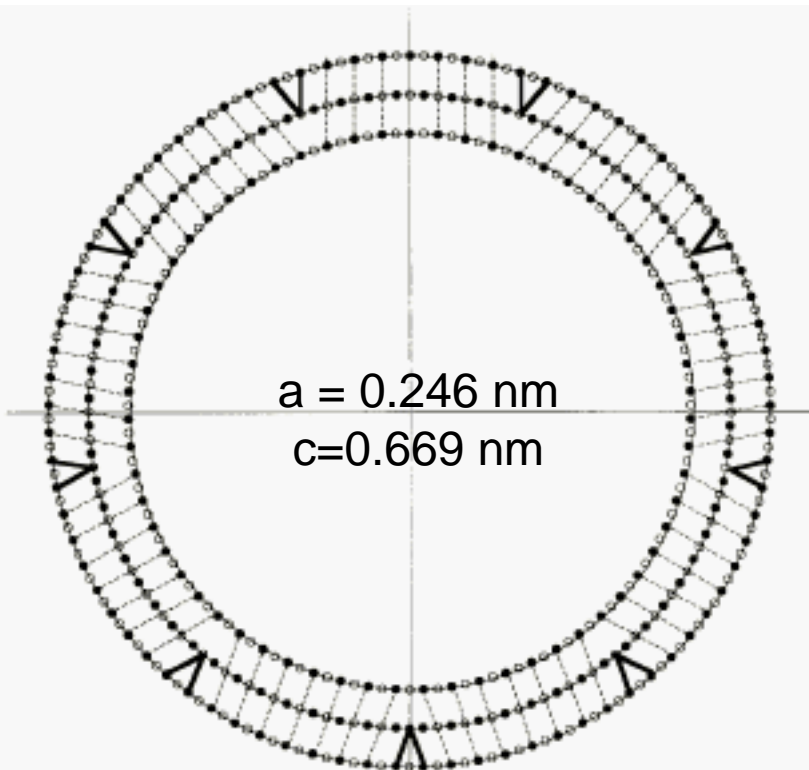
- (Chem. Phys. Lett. 260 465 (1996))

■ Nanotube HRTEM Characterization

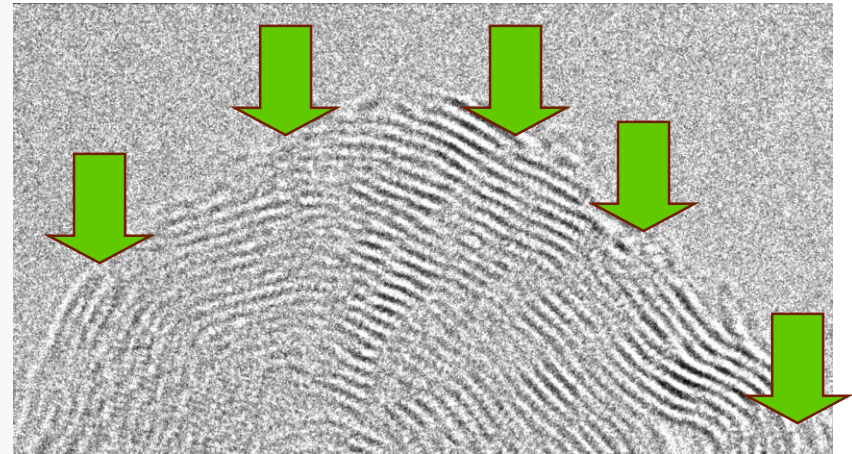
- Philips CM300 FEG (300 kV)
 - 0.17 nm point resolution
- Philips CM200 FEG (120 kV)
 - 0.24+ nm point resolution

Defect Formation

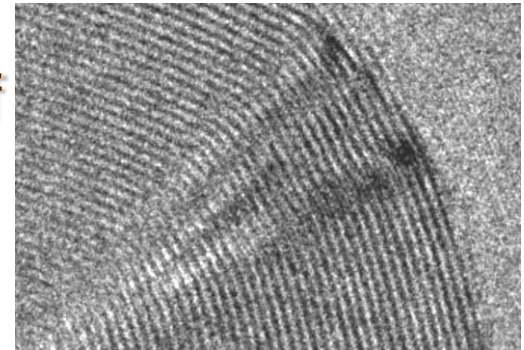
-in general, " πc " is unrelated to " a "
=> "interfacial" dislocations required for closure



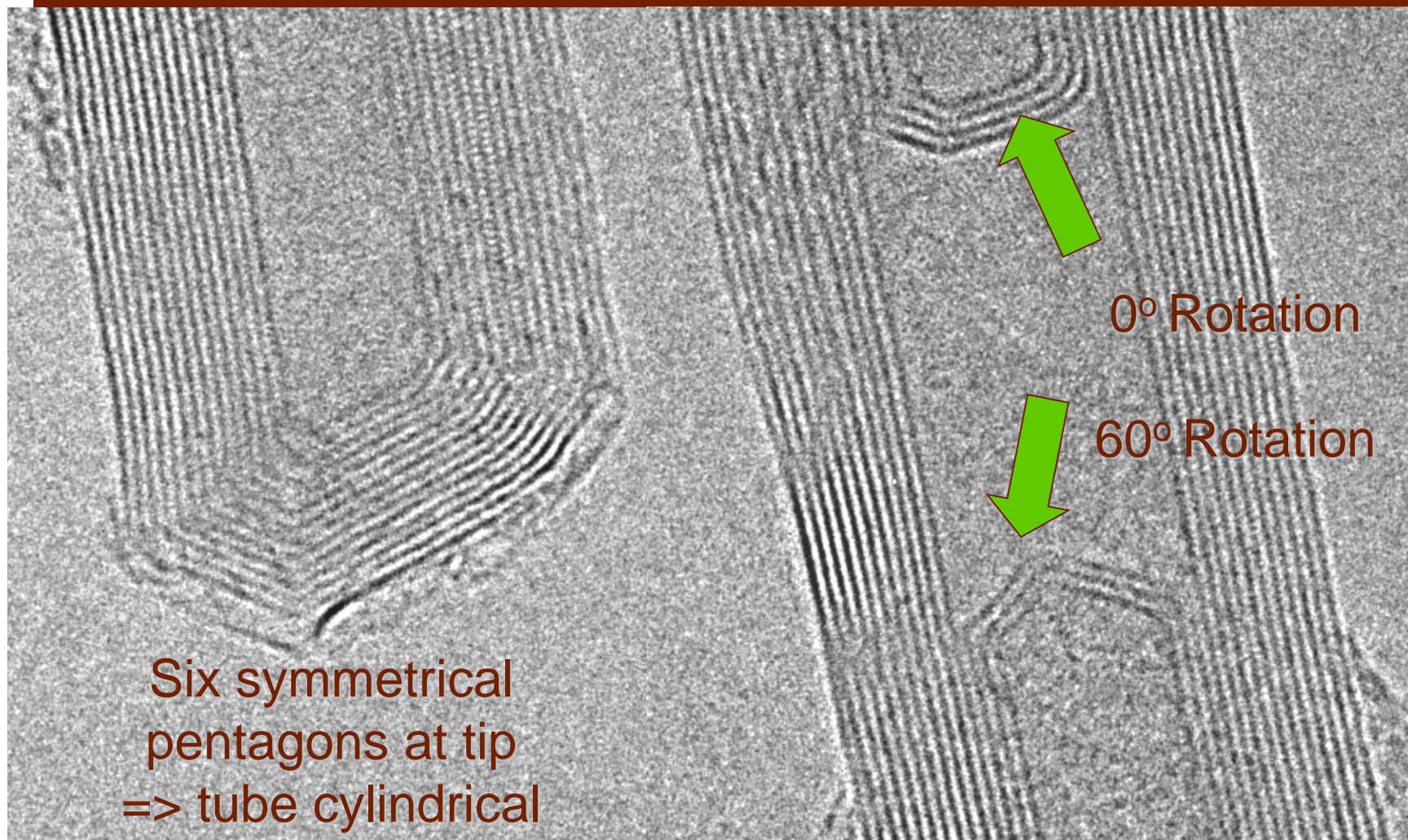
J. Cryst. Growth. 130 368 (1993).



Sideview of
"endcaps"

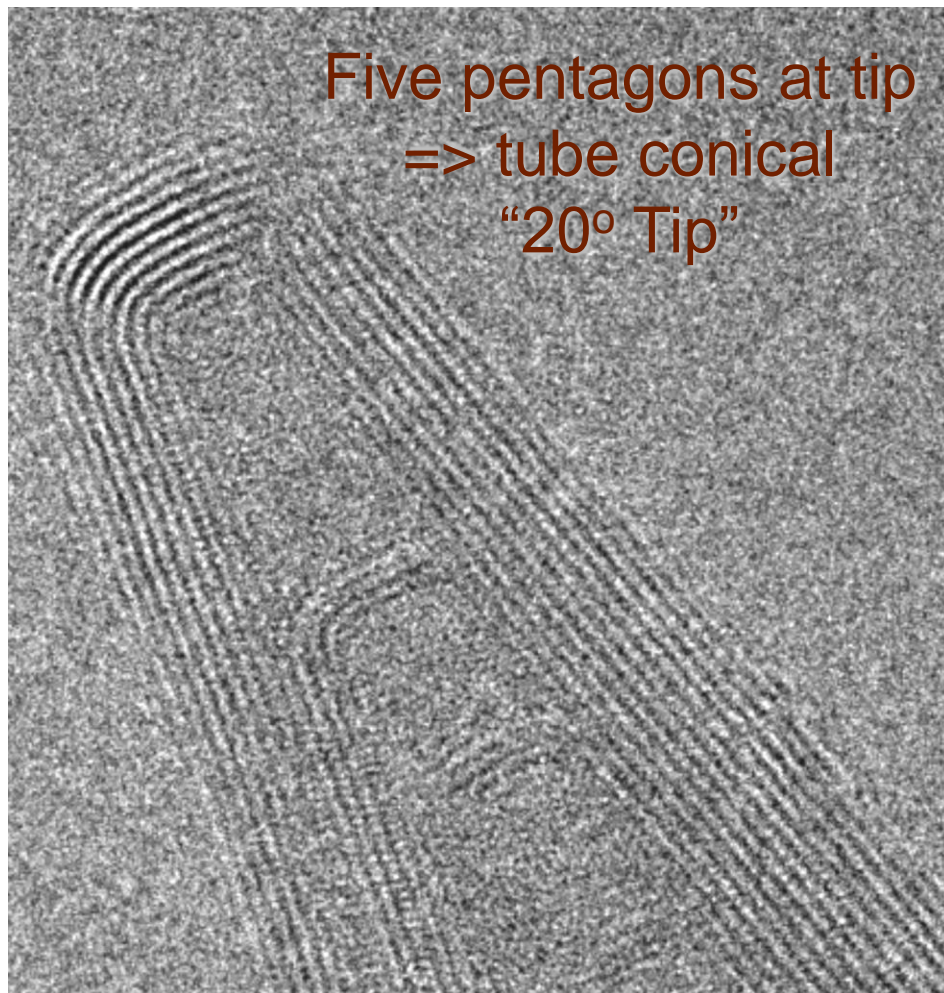


CNT Growth Termination-Normal

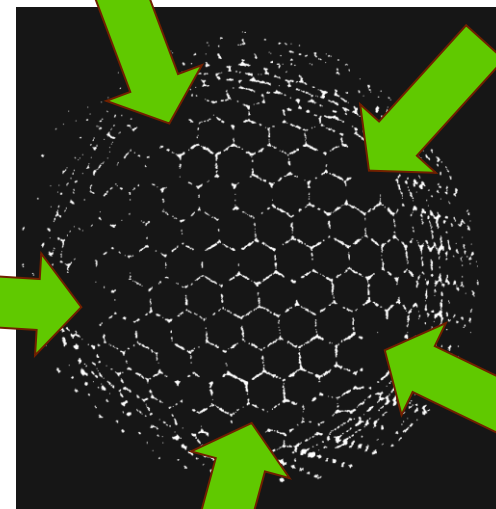


$$V + f = e + 2 \text{ (Euler)}$$

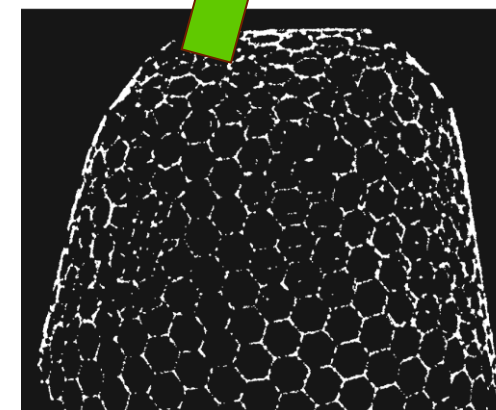
CNT Growth Termination-Early



Top View

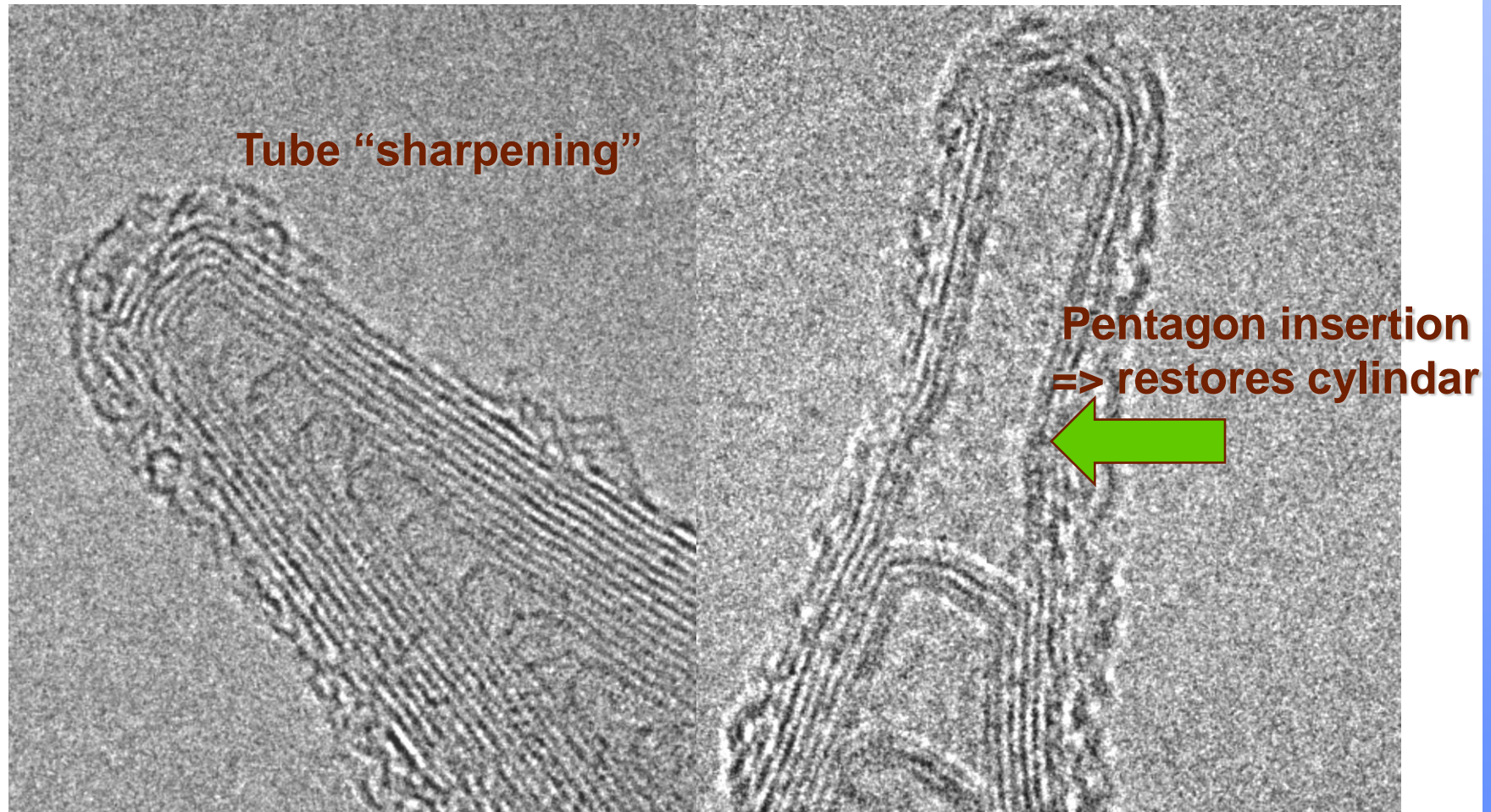


Side View



Elect. Micro. VIII 117 (1998).

CNT Growth Termination-Early



II. Tensile Testing of Multiwall C Nanotube

■ Nanotube Growth:

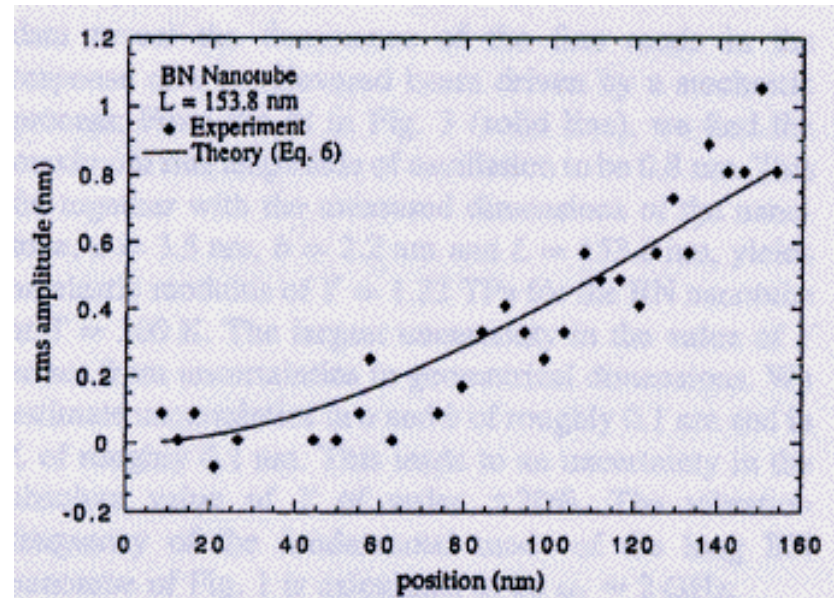
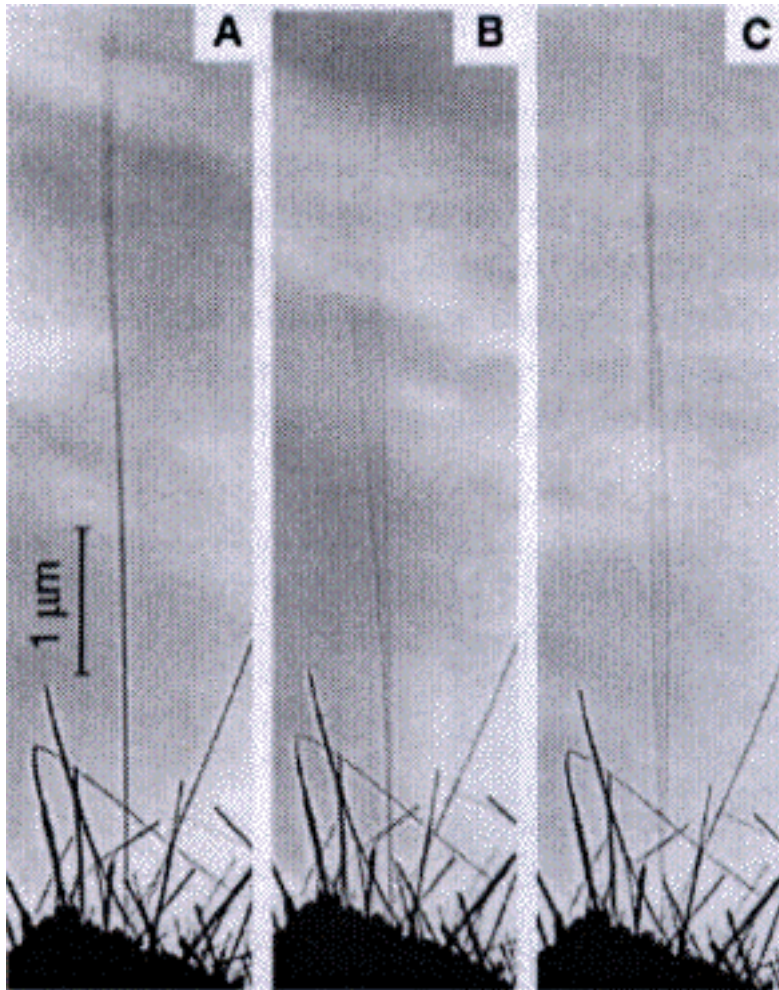
- Arc (60A, 30-45VDC) between B-doped C anode N₂ atm (380 T)

- (Chem. Phys. Lett. 260 465 (1996))

■ Nanotube TEM Characterization

- Topcon 002B (200kV)
- Piezoelectric Manipulation Stage

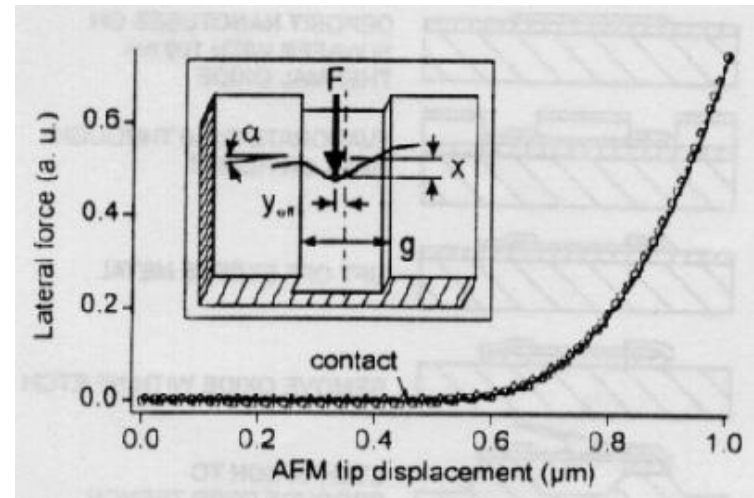
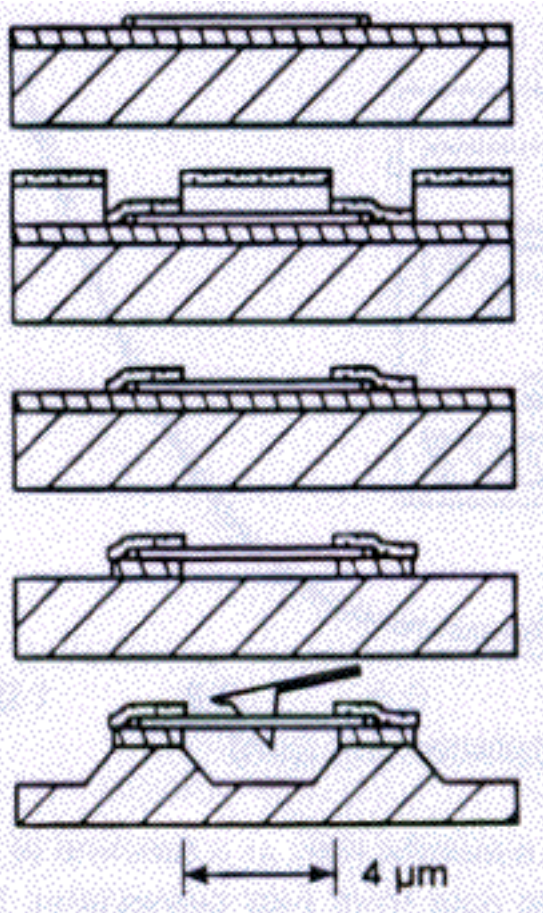
CNT Thermal Vibration (TEM)



$$v = \frac{\beta^2 D \sqrt{E}}{8\pi L^2 \sqrt{\rho}}$$

Sol. St. Comm. 105(5) 297 (1998).
J. Phys. Chem. Sol. 61 1025 (2000).

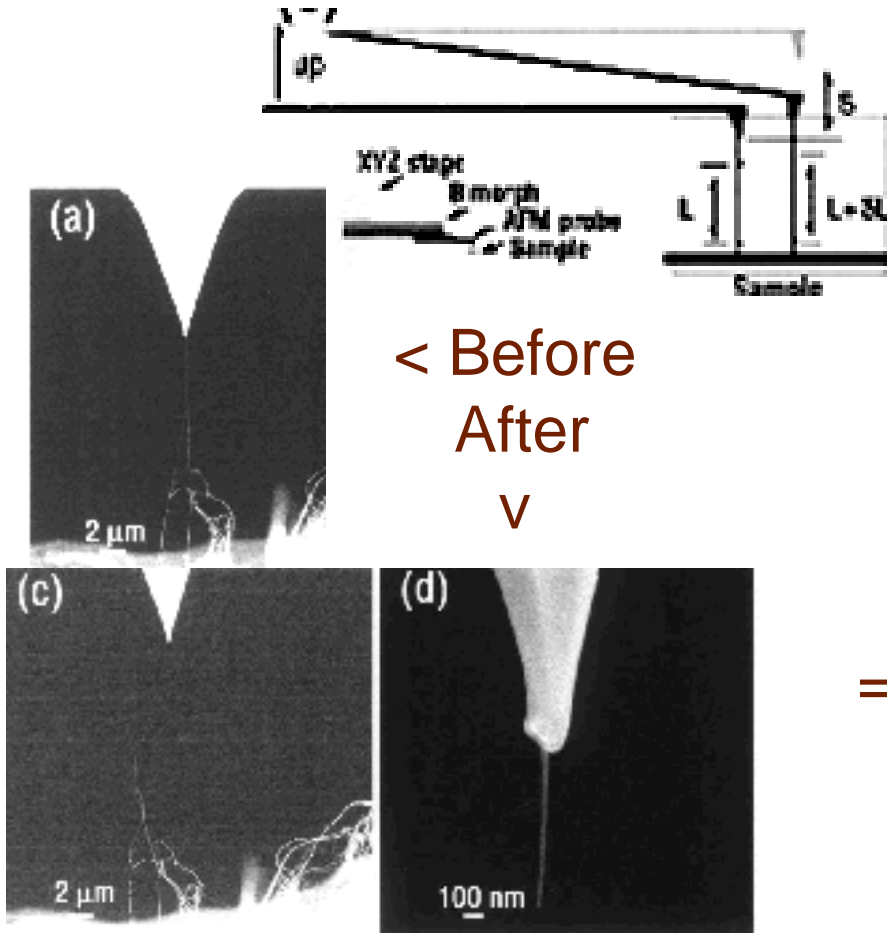
CNT Bending (AFM)



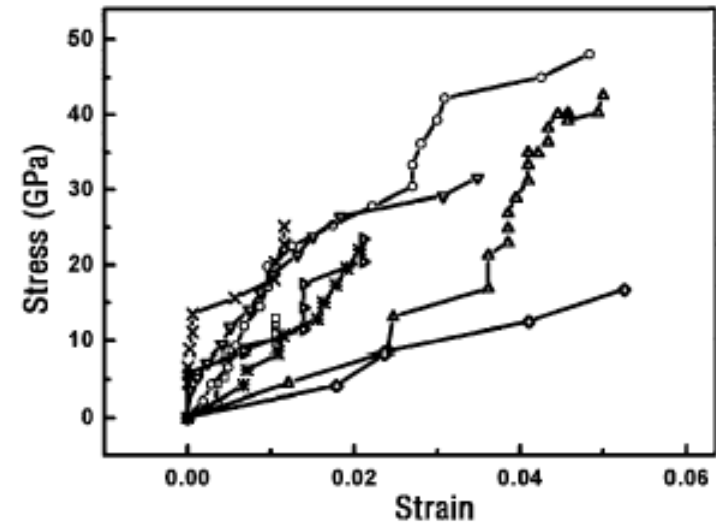
Force applied with probetip
=>strain (to failure) measured
- But section not round

Appl. Phys. Lett. 74 (25) 3803 (1999).
Phys. Rev. Lett. 82 (5) 944 (1999).

CNT Pulling (AFM/SEM)



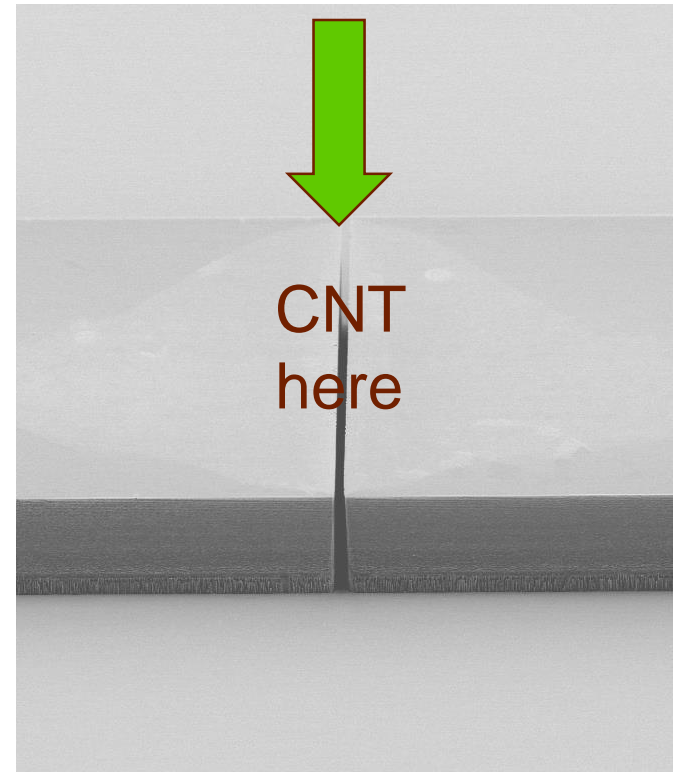
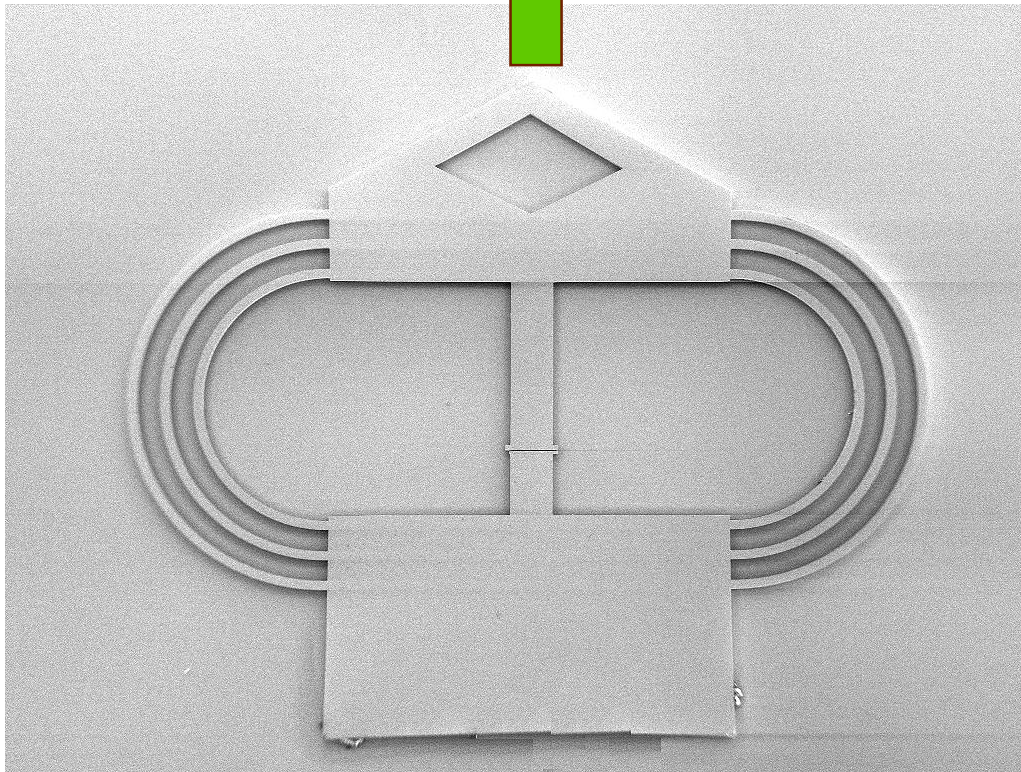
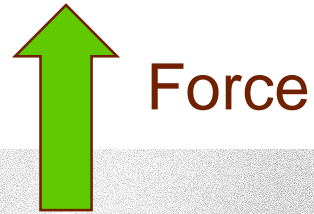
< Before
After
v



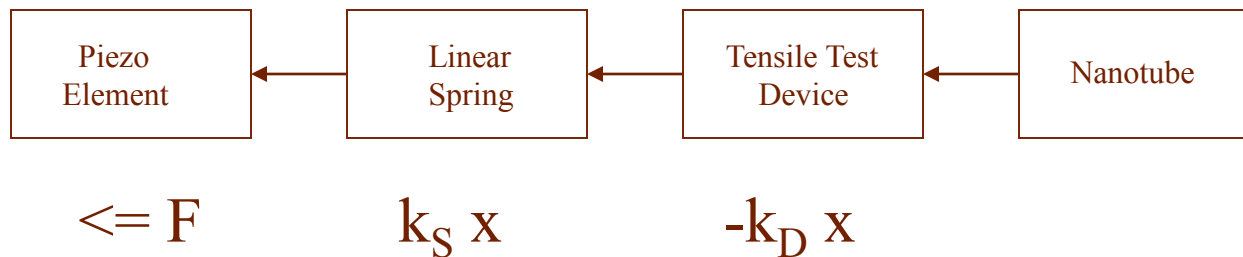
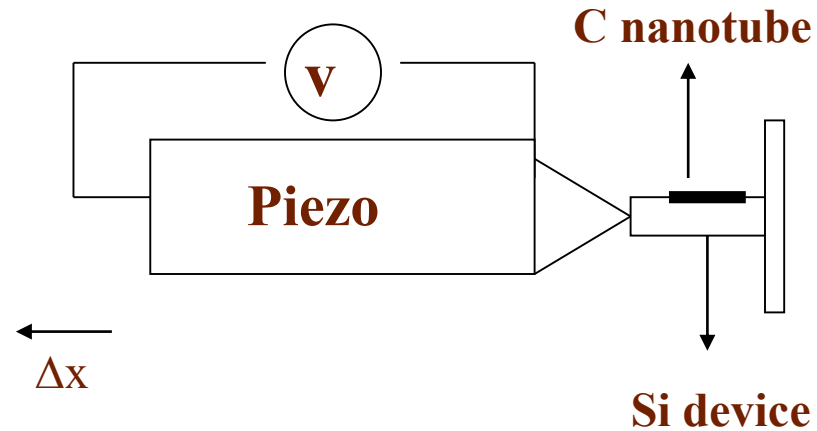
Tube pulled with probetip
=> strain (to failure) measured
- But both ends moving.

Phys. Rev. Lett. 84 (24) 555, (2000).
Science 287 637 (2000).

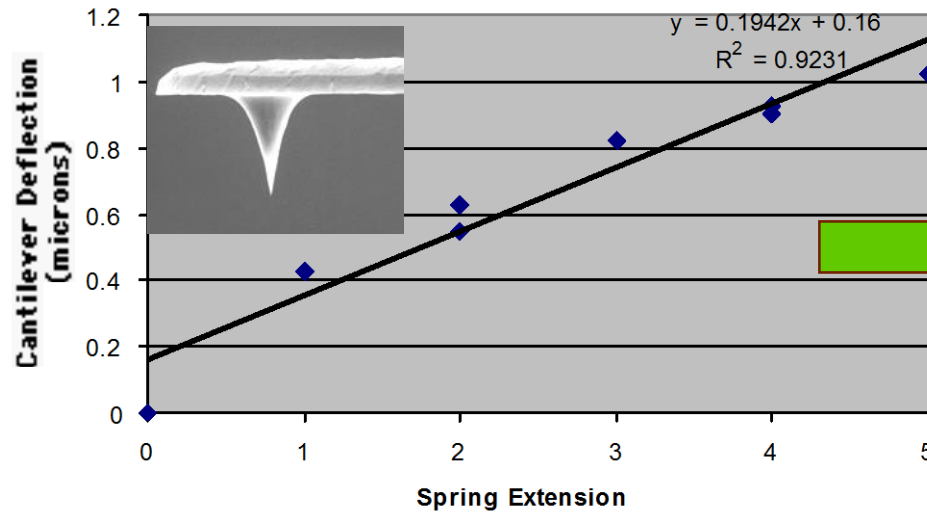
Microfabricated Tensile Stage



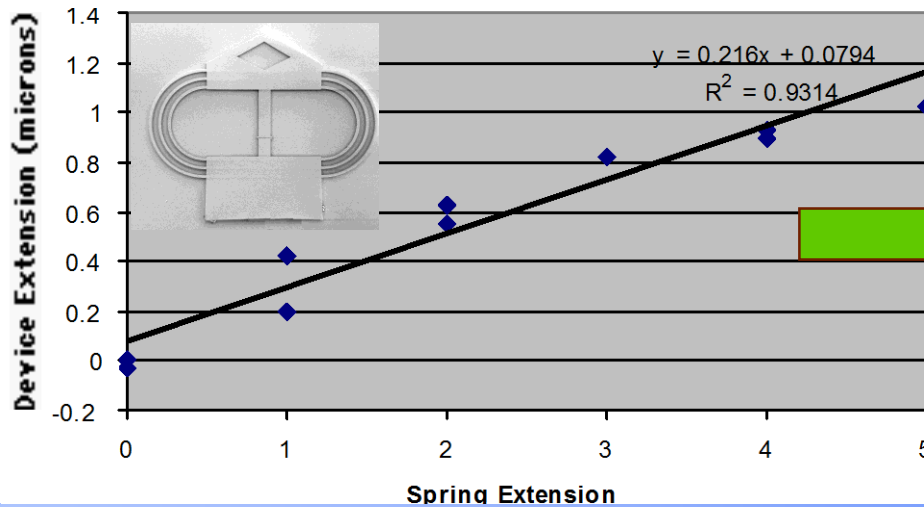
Experimental Setup



Force Calibration



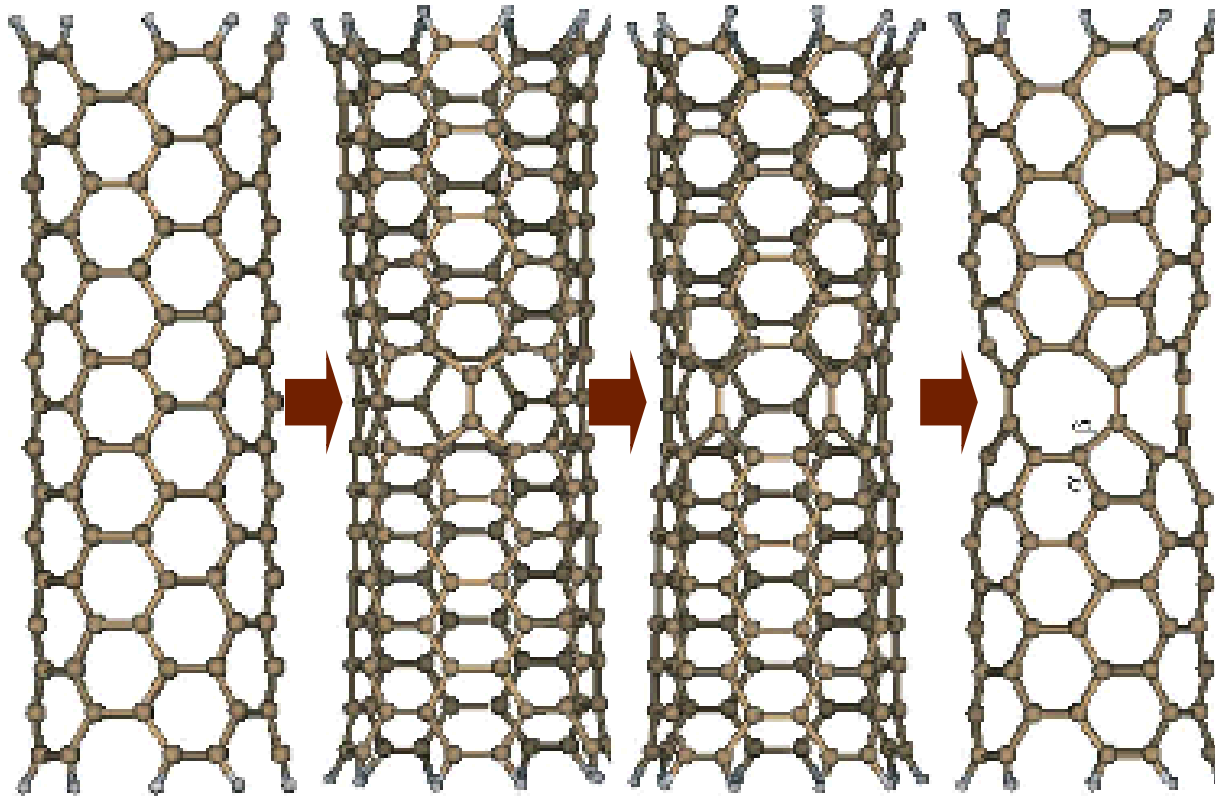
k_{spring}



k_{device}

CNT Fracture- Stone-Wales Transformation

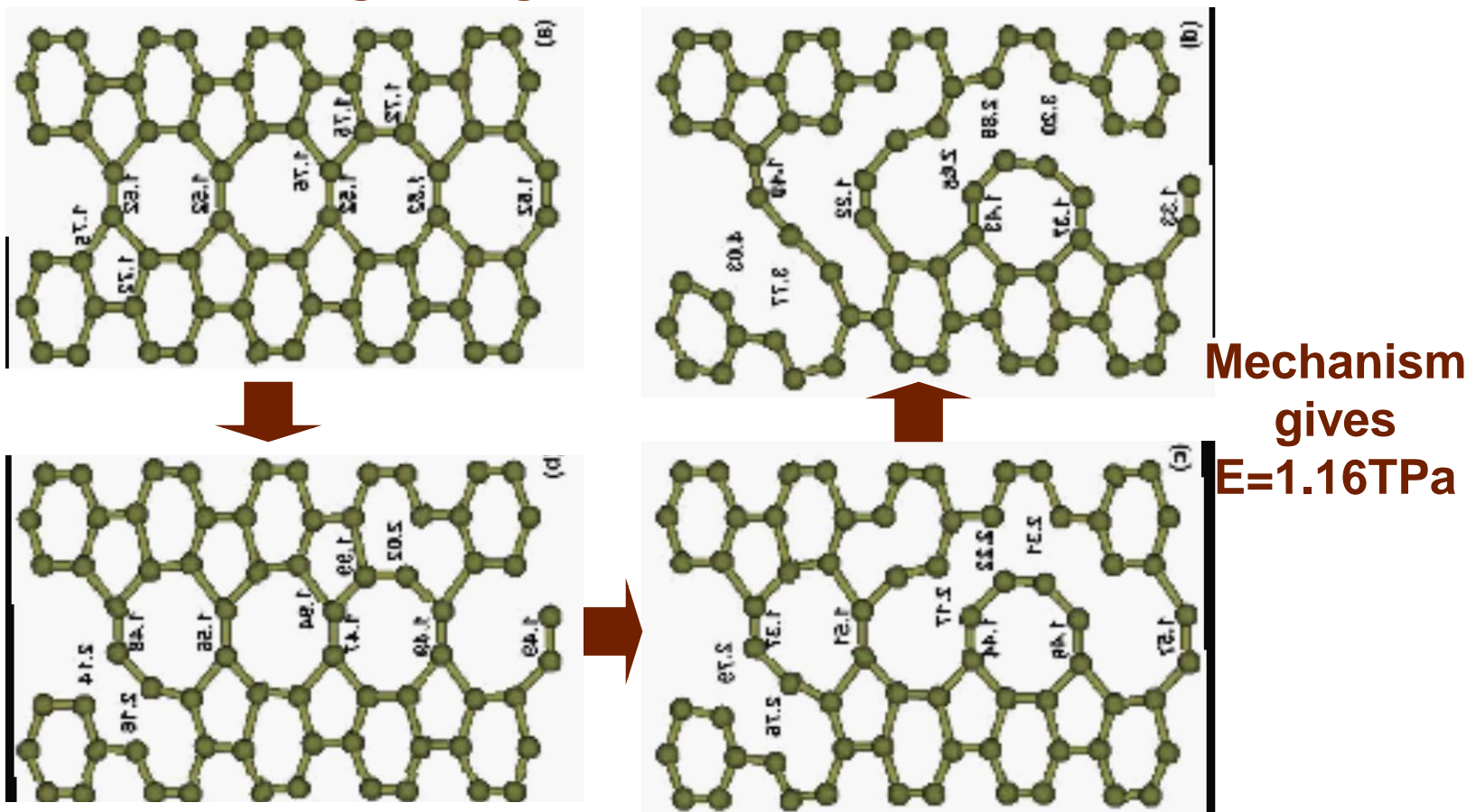
- C-C bond ruptured in 4 hexagons
=> 2 pentagon/heptagon pairs created
then larger (octagon) rings formed



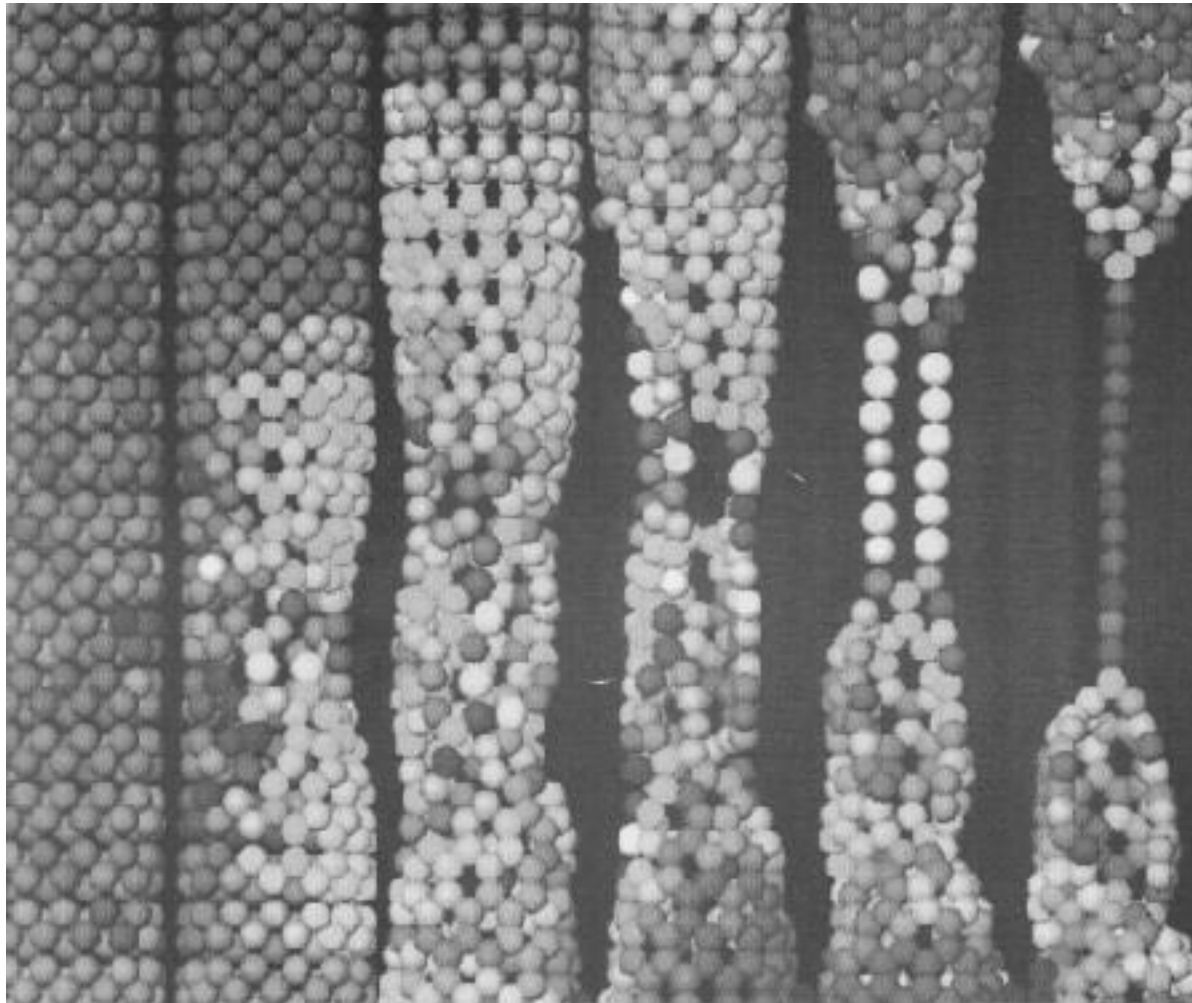
**Energetically
favored for
 $\varepsilon \sim 5\%$**

CNT Fracture-Bond Breaking

Octagon ring bonds break => tube narrows

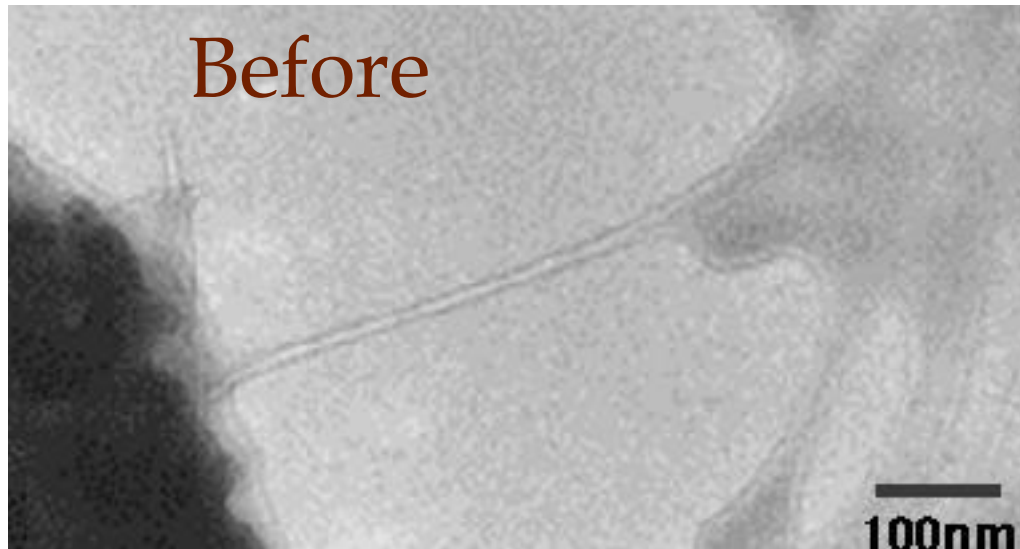


CNT Fracture-Narrowing to Failure



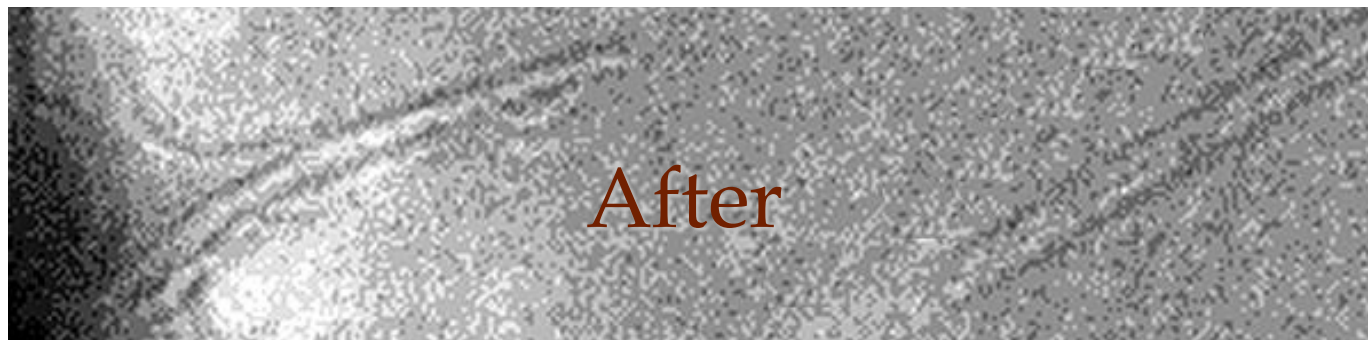
**Tube narrows
to
monatomic
layer
(in $\sim 10^{-10}$ sec)**

Nanotube Tensile Test

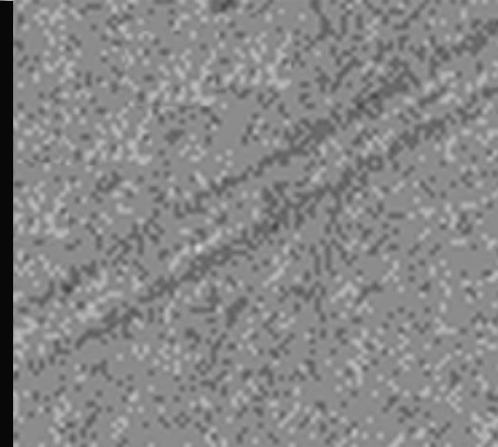
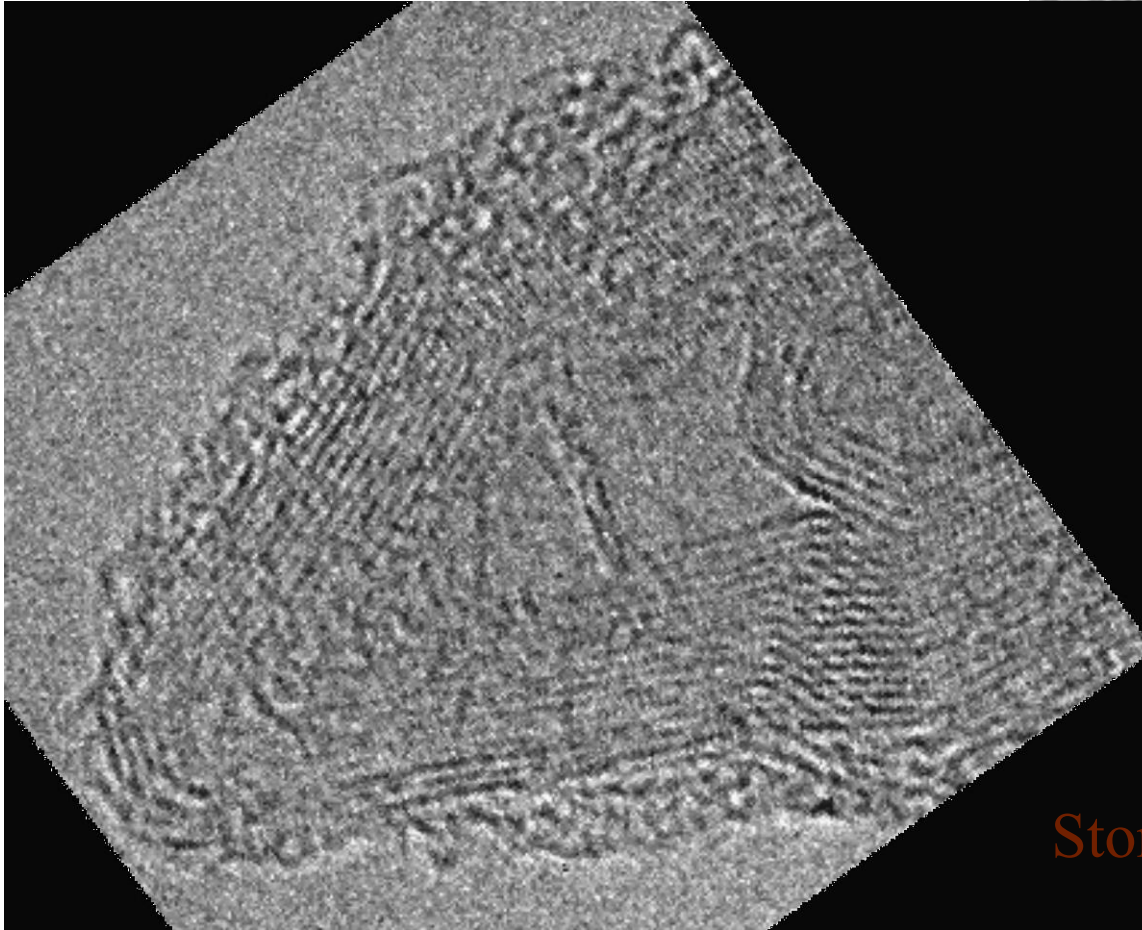


-for $F = 18 \mu\text{Nt}$,
 $A = 123 \text{ nm}^2$
 $\Rightarrow \sigma = 0.15 \text{ TPa}$

-consistent with
predictions and
Stone-Wales
mechanism

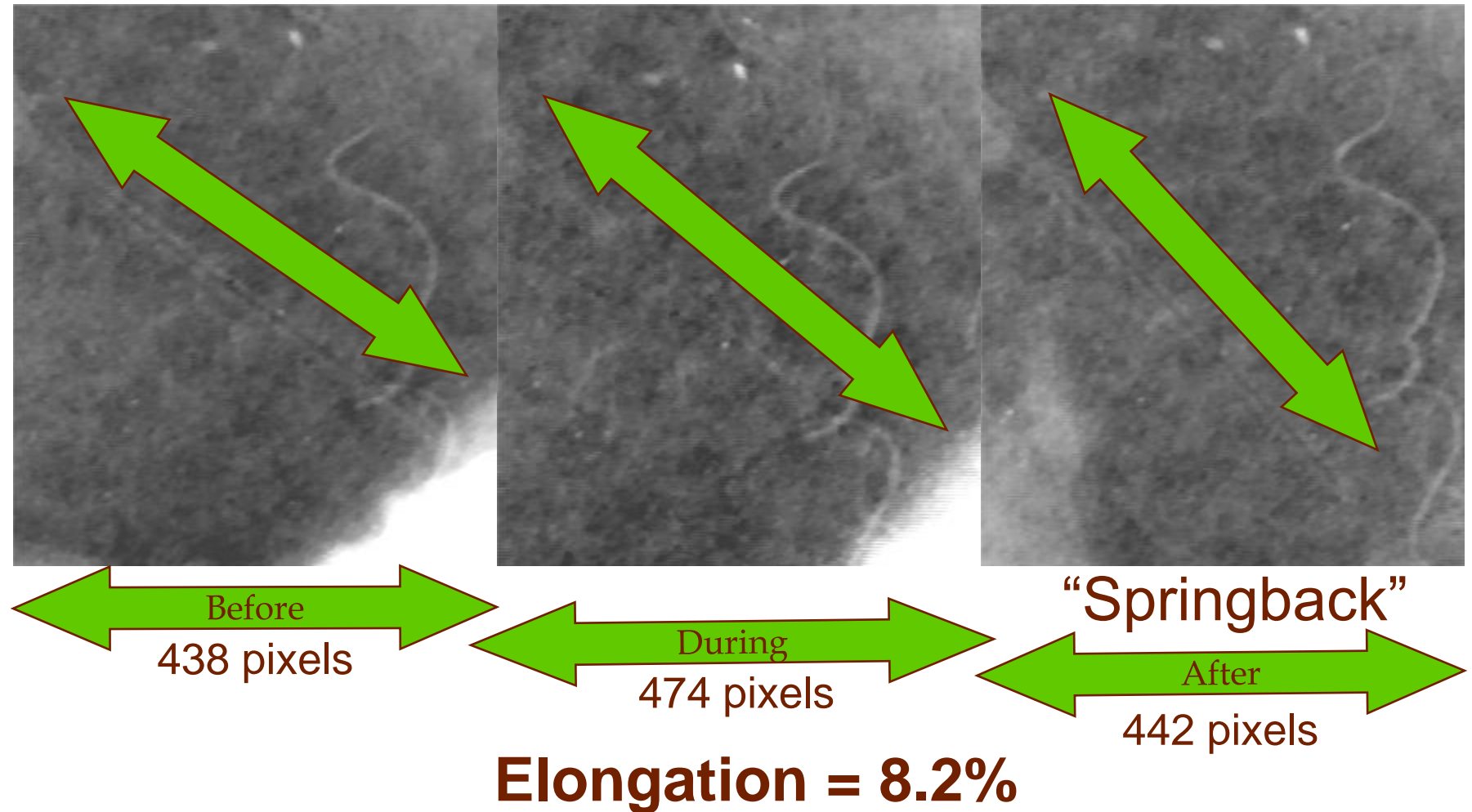


“Healed” Endcap

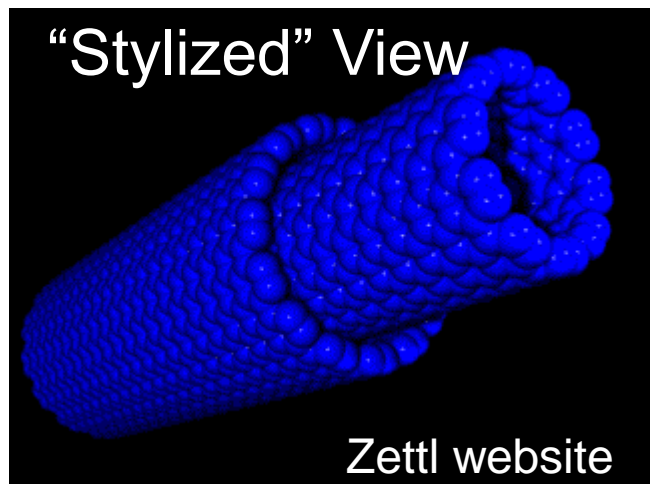
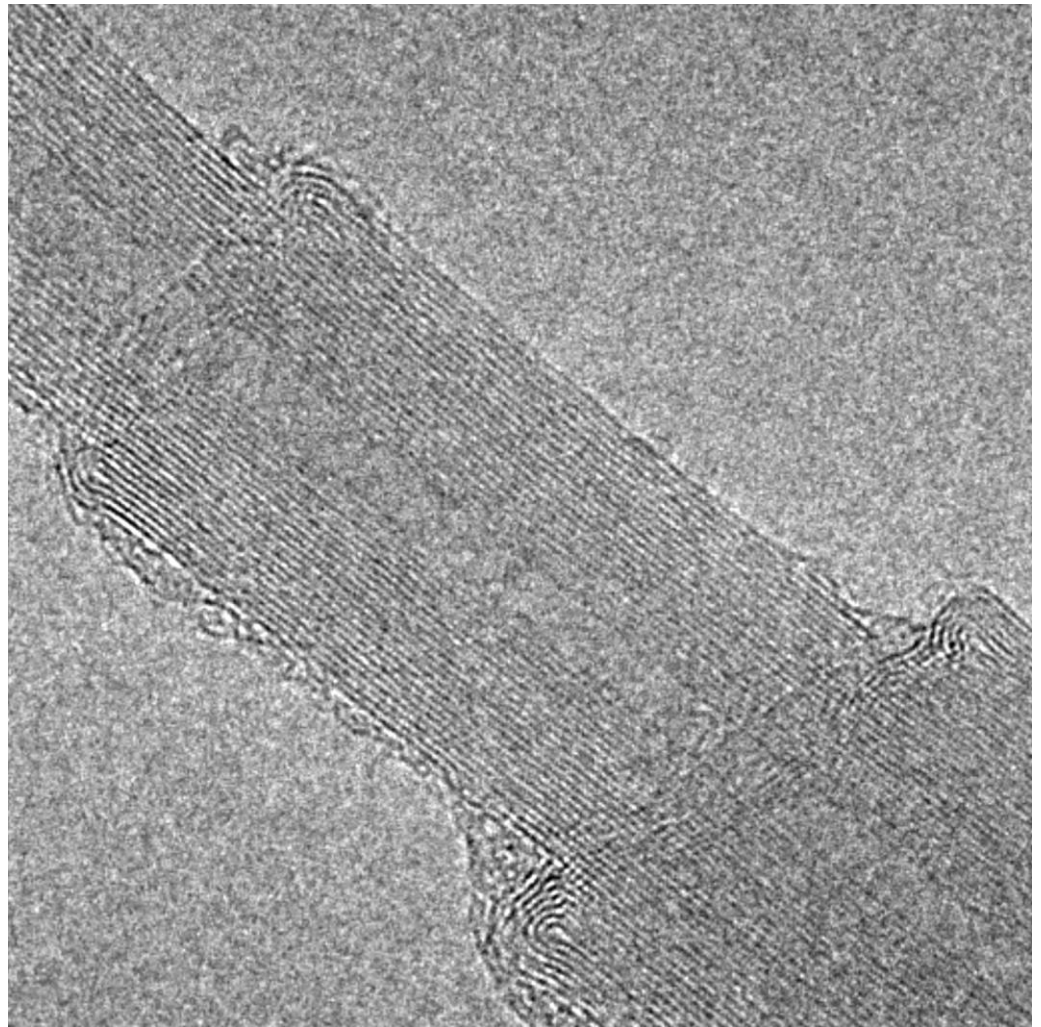
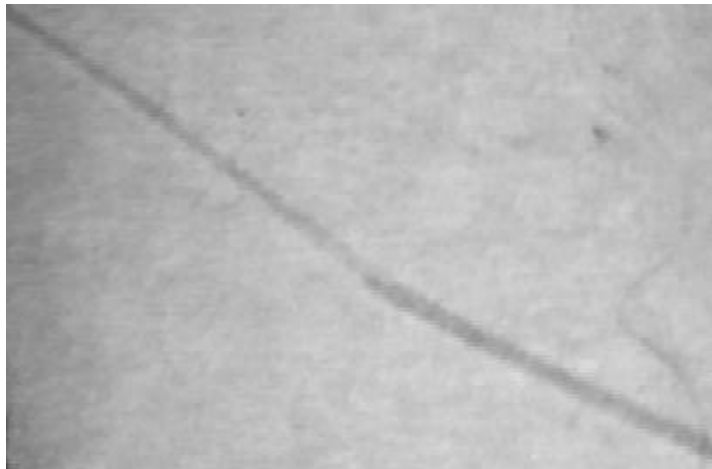


Consistent with
Stone-Wales mechanism

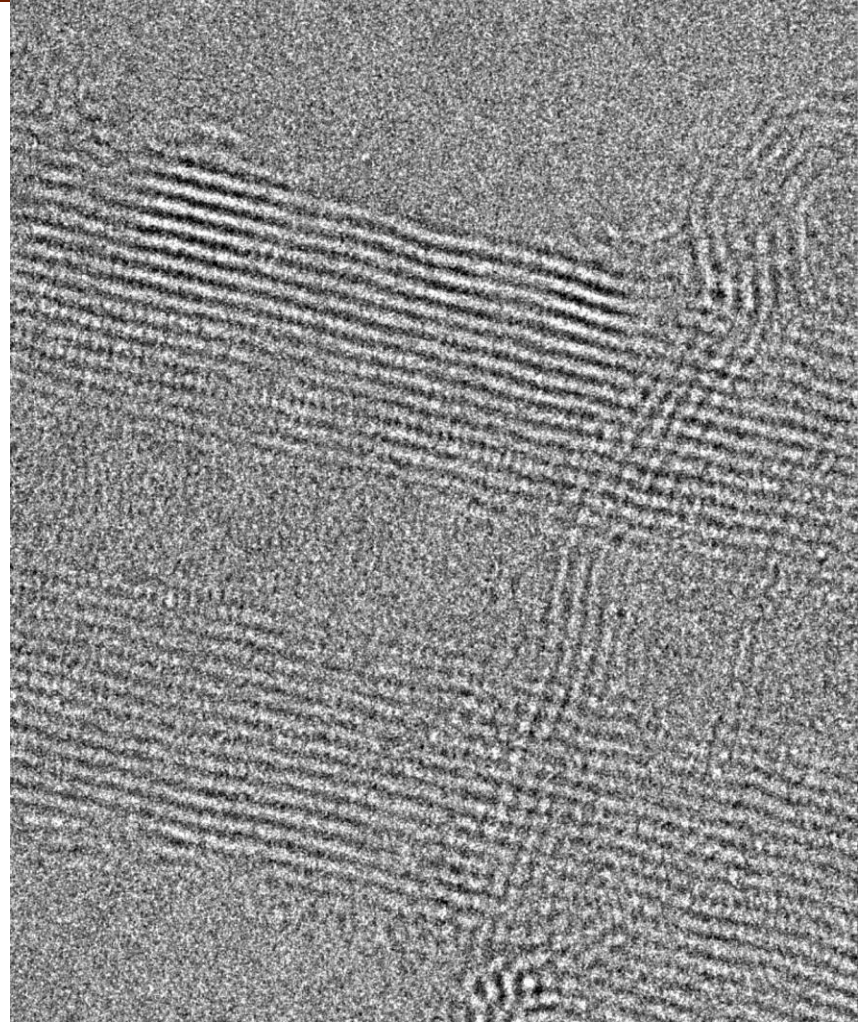
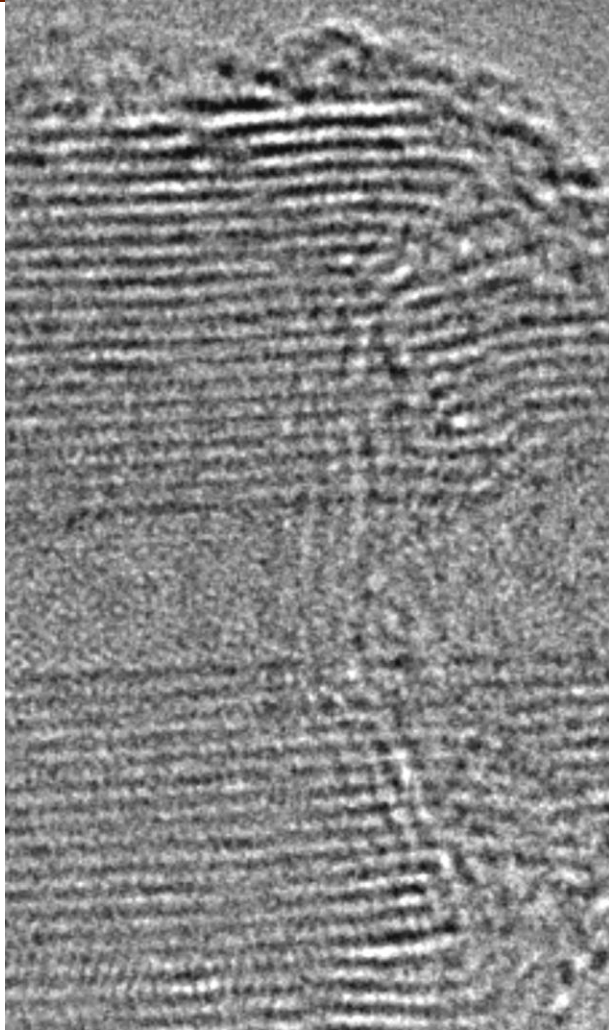
Elongation (major section)



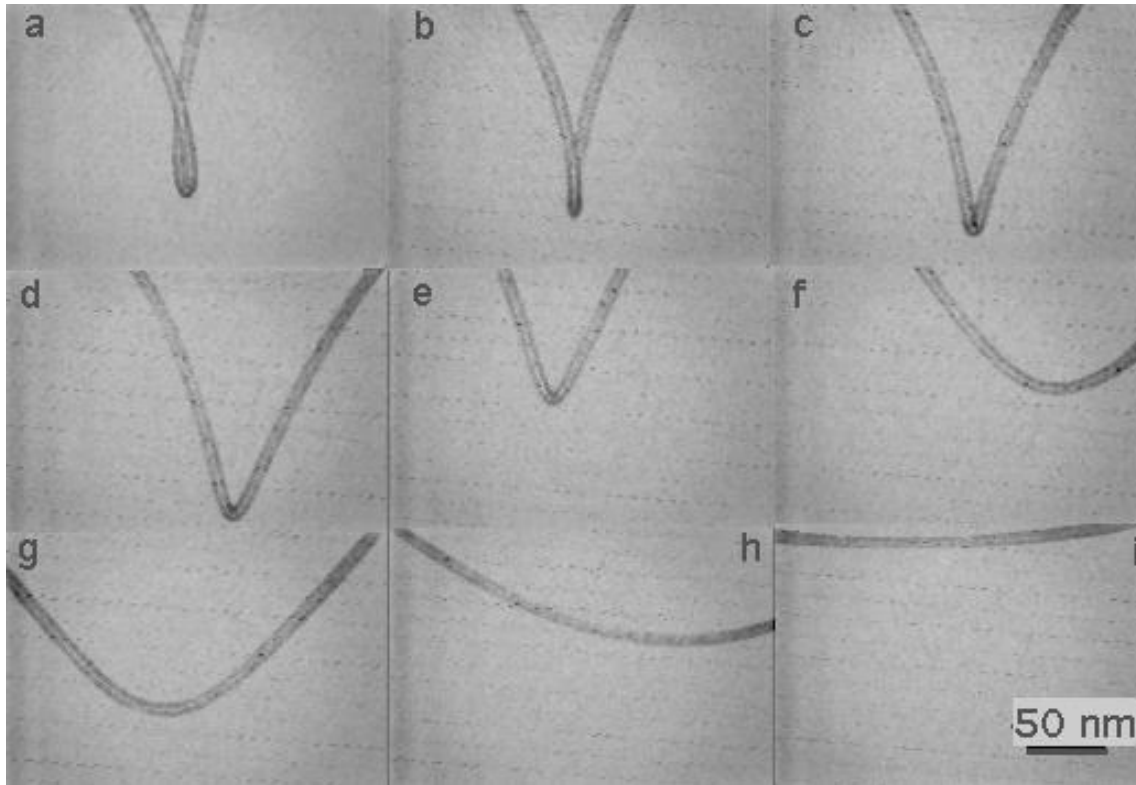
“Telescoping” Tubes



“Telescoping” Tubes (Grown-In)

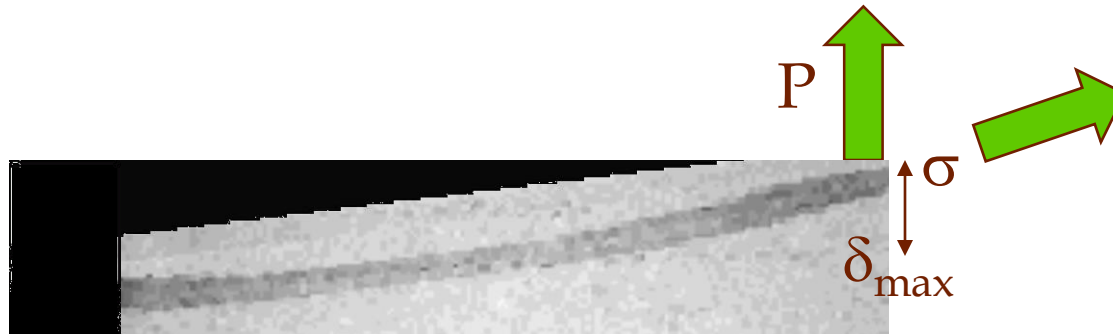


CNT Bending Sequence



Note strain contrast at sharp bends (b-e) and the lack of the same in the straightened tube (i).

Young's Modulus

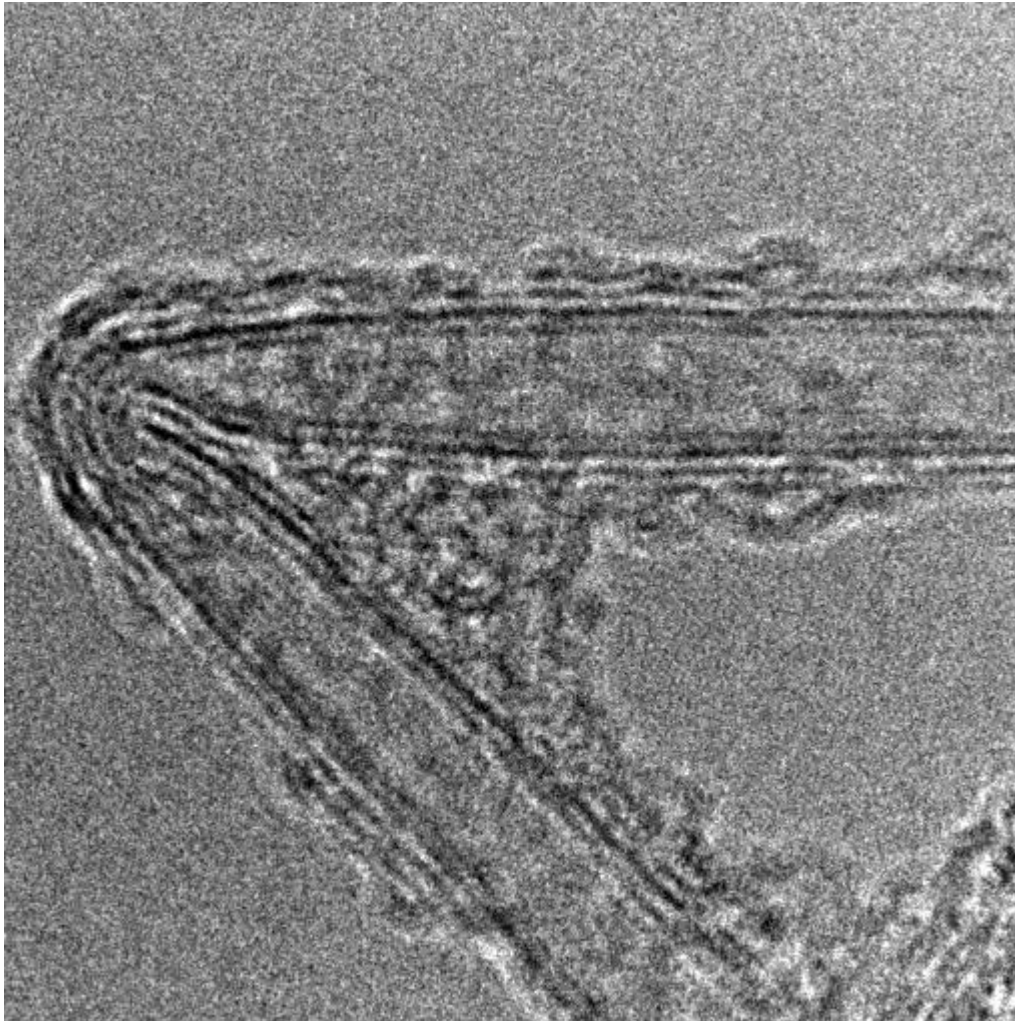


$$P = \sigma \tan \alpha$$

$$E = PL^3 / 3I\delta_{\max} \quad I = \pi tr^3$$

-for $P=10.9 \mu\text{Nt}$, $r=5.6 \text{ nm}$, $t=333 \text{ nm}$ (10 walls)
 $\Rightarrow E = 0.91 \text{ TPa}$

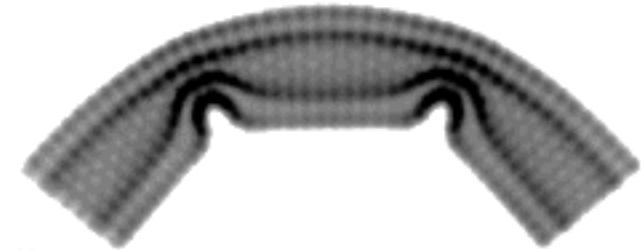
Bent Tube



High Strain



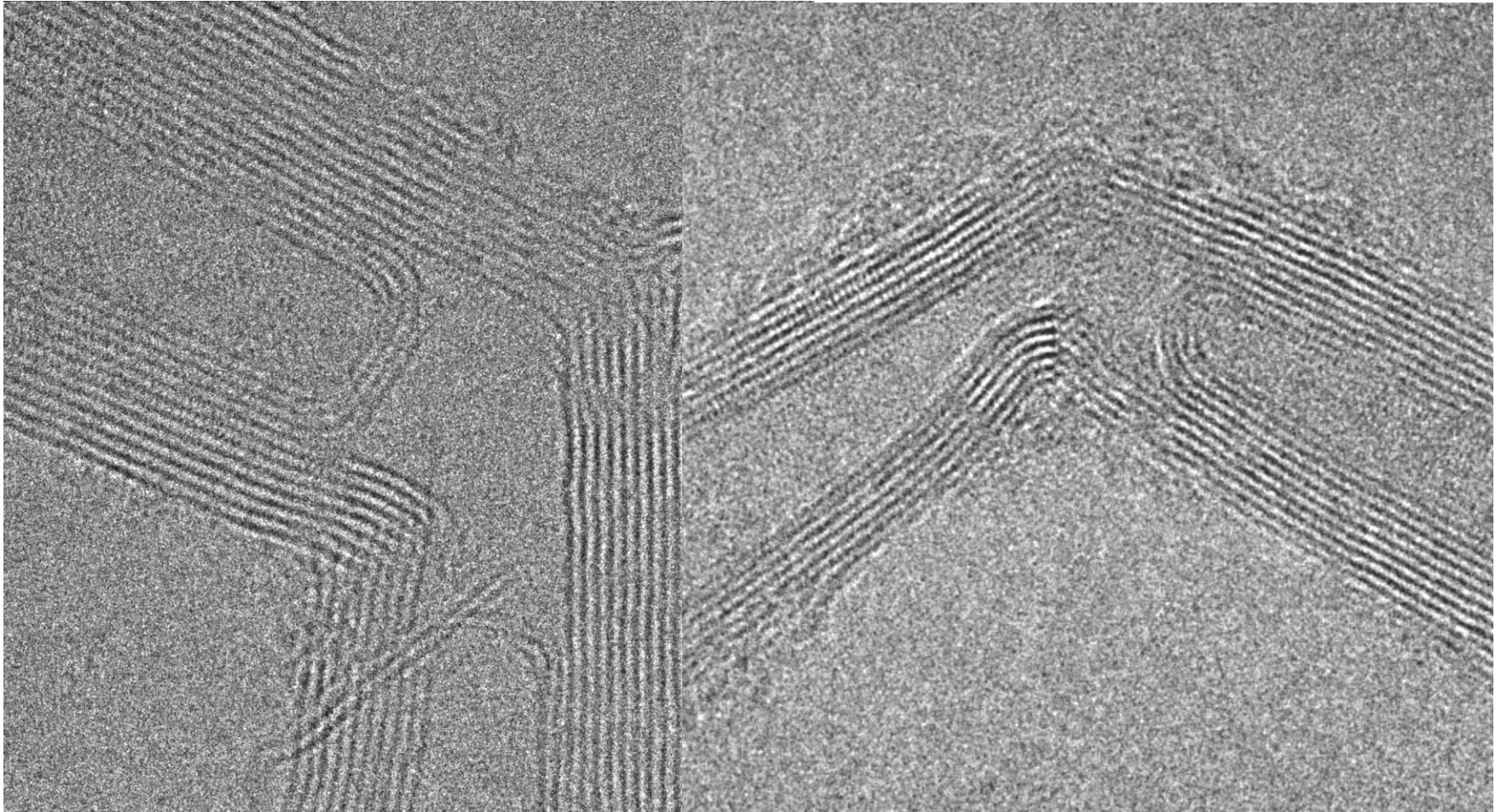
(b)



(a)

Higher Strain

Bent Tubes (Grown-In)



Multiwall CNT Mechanical Measurements

E (TPa)	σ_T (TPa)	Method
0.81 (50%)	----	AFM-2end s clamp ed [33]
1.28 (40%)	----	AFM-1end clamp ed [21]
1.26 (20%)	----	TEM- thermally v ibratingbea m [22]
0.1-1 ($\sim 1/R$) (30%)	----	TEM-electrostatic d eflexion [15]
0.27-0.95	0.01-0.06	Dual AFM cant ilev ers [34]
0.91 (20%)	0.15 (30%)	TEM -direct tension [this work]

E = Young' s Modulus, σ_T = tensile streng th, R = nano tube radius, () = unce rtain ty

Summary of *In-Situ* CNT Observations

■ Mechanical Properties:

➤ $\sigma_T = 0.15$ TPa, $E = 0.91$ TPa

■ Deformation Mechanisms:

➤ high strain rate

- outer tubes fracture

- partial pullout of inner tubes

➤ Low strain rate

- Full “telescoping”

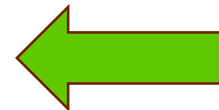
➤ Reversible ($>90^\circ$) bending

But CNT....

- Not chemically inert
 - React with metals (carbides)
- Cannot withstand shock loading
 - Form nanodiamonds
- Unstable at high T
 - **EXPENSIVE**
 - \$1500./gm (gold \$450./gm)



Inorganic tubes attractive



III. Structure Imaging of BN Nanotubes

■ Nanotube Growth:

- Arc (60A, 30-45VDC) synthesis in “dynamically stabilized” N₂ atm (380 T)
 - (Chem. Phys. Lett. 316 211 (2000))

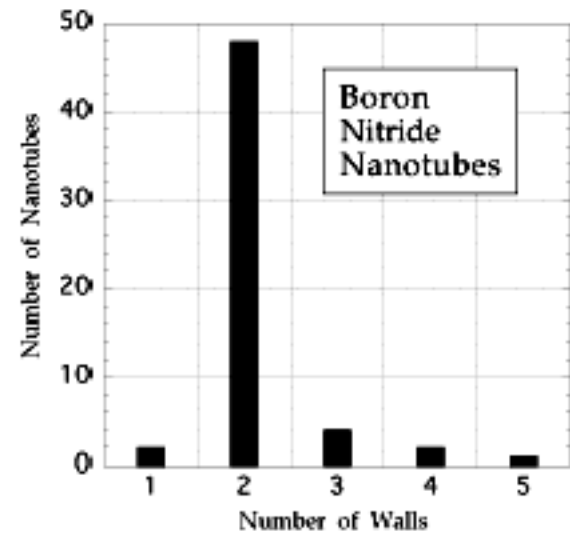
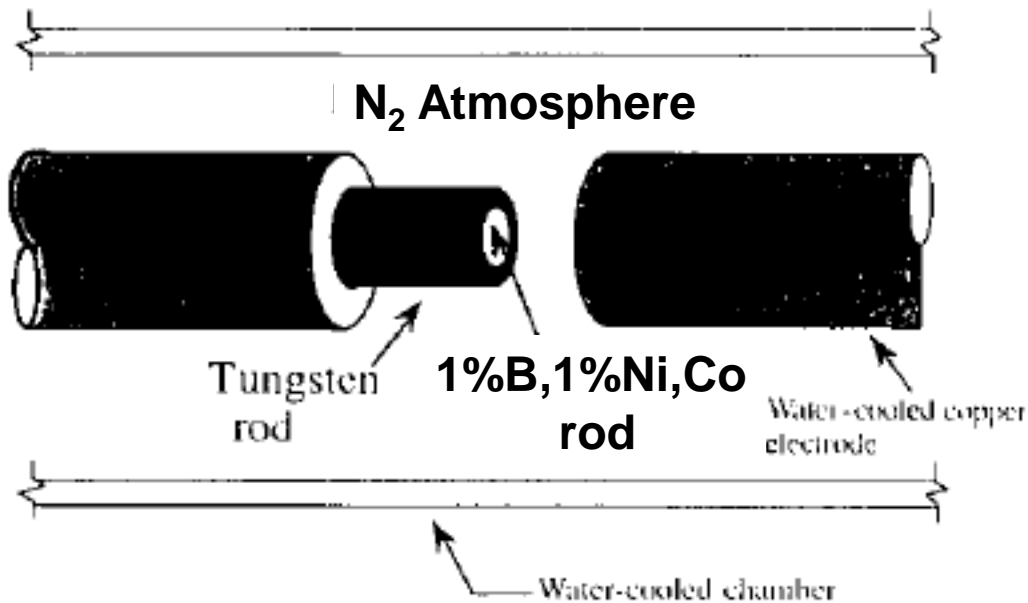
■ Nanotube HRTEM Characterization

- Philips CM300 FEG (300 kV)
 - 0.17 nm point resolution

Motivation

- Two (different size) atom tube structure
- Two walled (predominantly) nanotubes

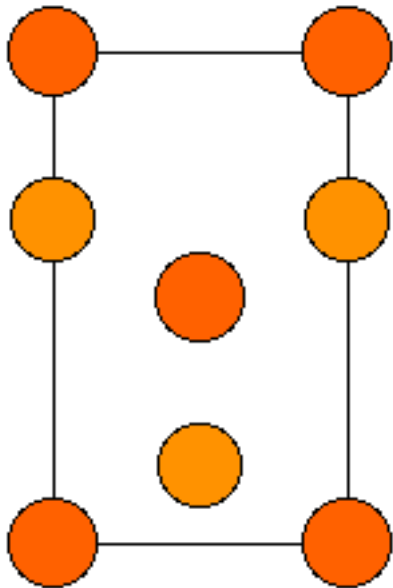
BN Nanotube Growth



adapted from
“Fullerines: Chemistry, Physics
and Technology”, Ch. 17 (2000).

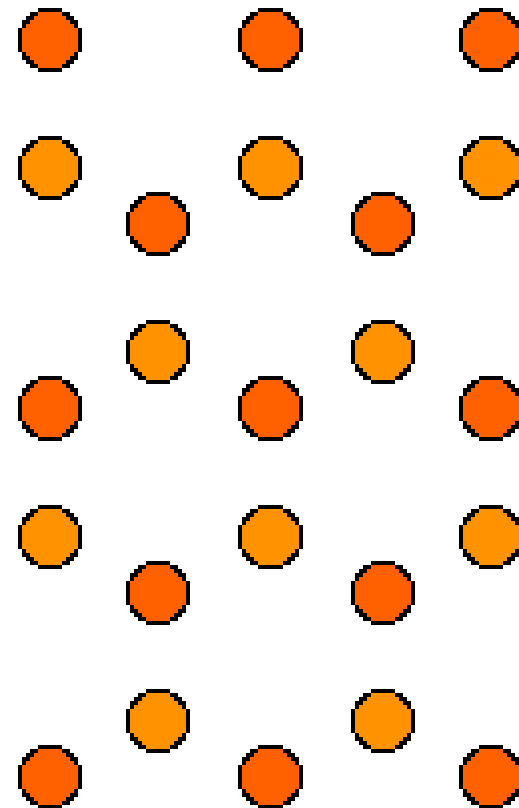
Chem. Phys. Lett. 382 133 (2003).



BN Structure



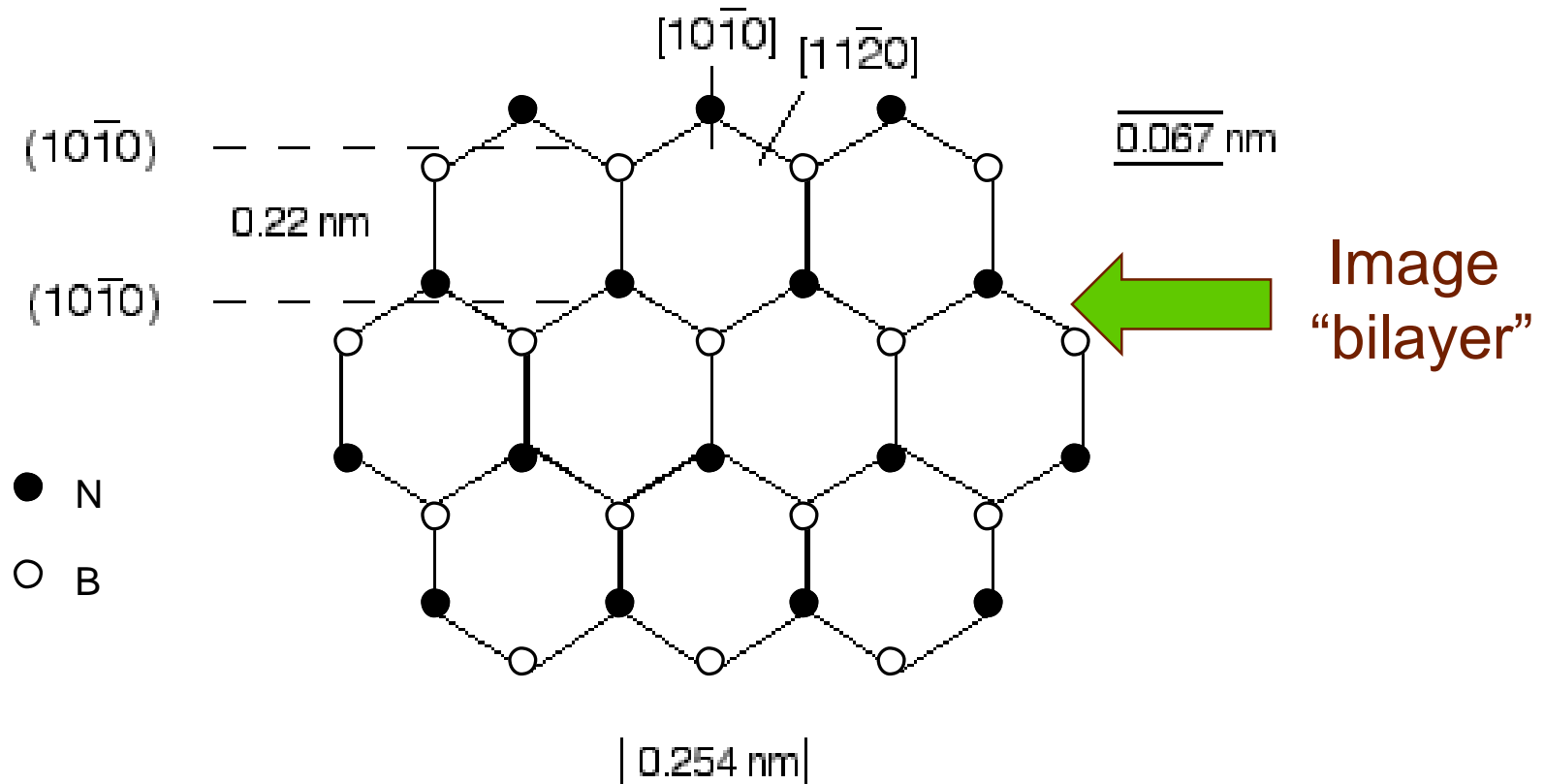
$a = 0.246 \text{ nm}$
 $c = 0.669 \text{ nm}$

Atomic Basis:
B: $(0,0,0)$ & $(.5,.5,0)$
N: $(.5, .1588,0)$ & $(0,.6588,0)$



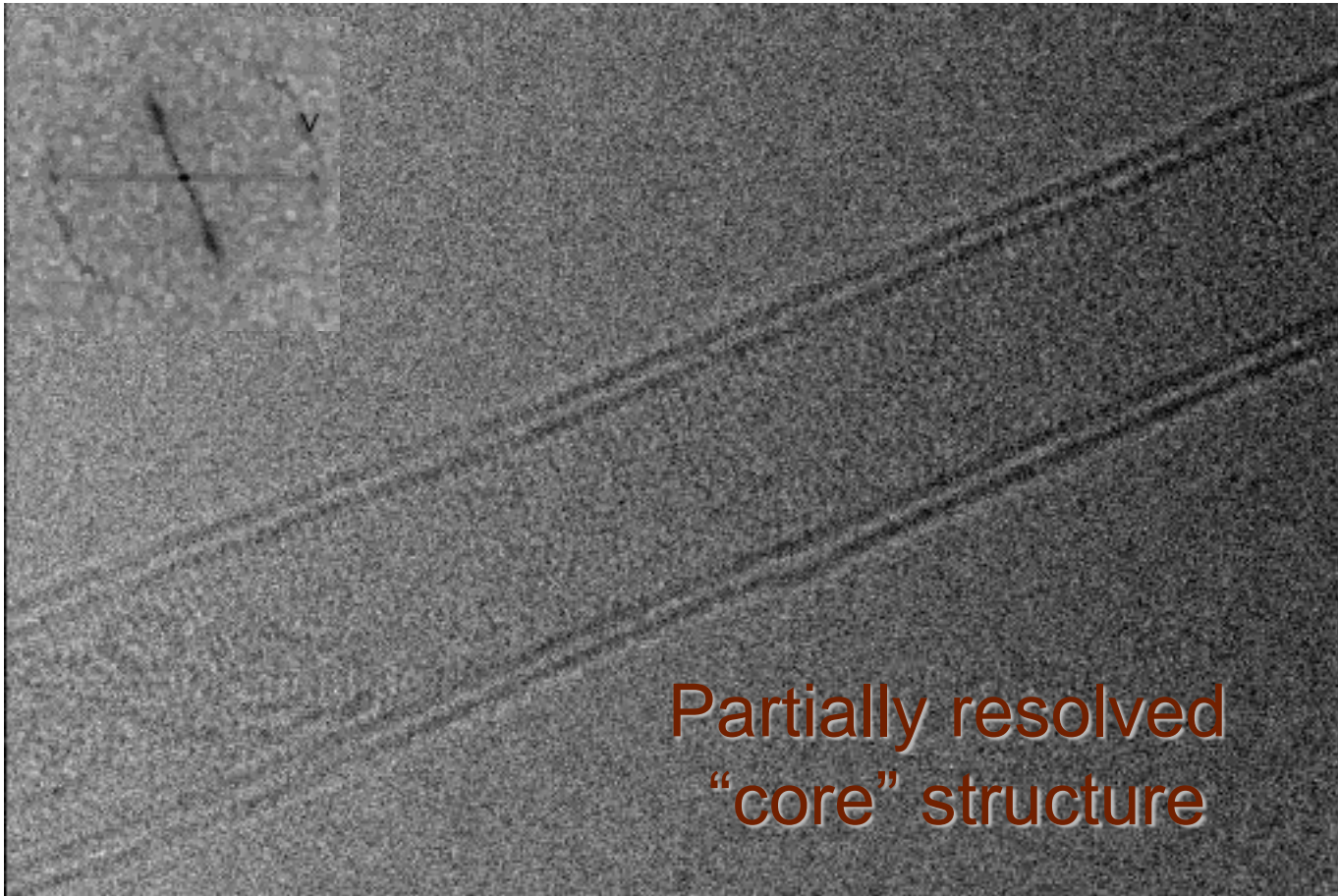
AtomTypes			
B		N	

BN Basal Plane



Schematic sketch of boron nitride basal plane, showing the $\{1\ 0\ 0\}$ bilayers.

Two Wall BN Tube



Results - 2 Wall BN Tube

■ Tube 1

➤ $\langle_{(00.2),(11.0)} = 83^\circ$

➤ Maxima at 37° and 19°

➤ $\langle 10.0 \rangle$ (zig-zag) tube axis

➤ $\sim 7^\circ$ chirality

“bilayer” = 0.22 nm
“sidewall” = 0.37 nm
(bulk = 0.34 nm)

■ Tube 2

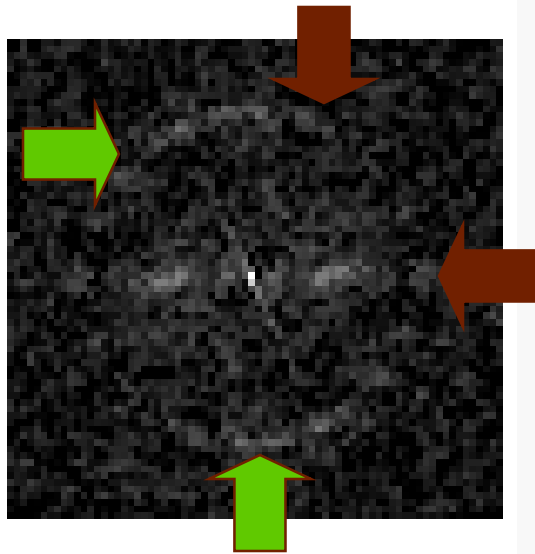
➤ $\langle_{(00.2),(01.0)} = 64^\circ$; $\langle_{(00.2),(11.0)} = 57^\circ$

➤ Maxima at $\pm 4^\circ$

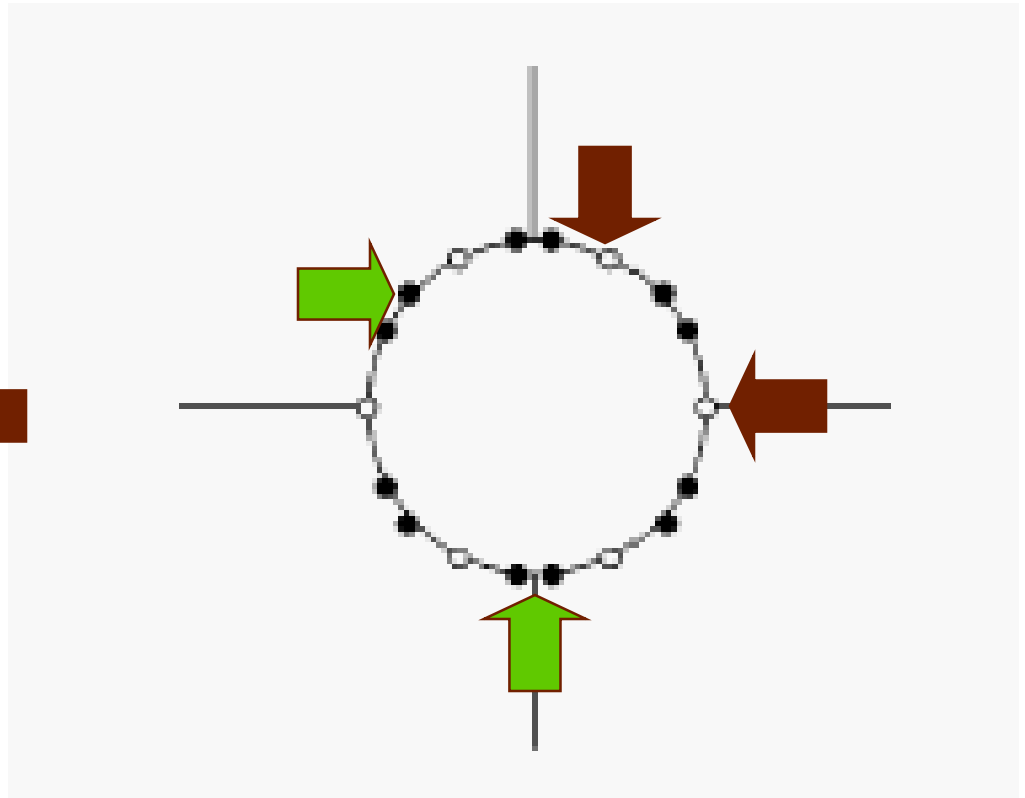
➤ $\langle 11.0 \rangle$ (armchair) tube axis

➤ $\sim 4^\circ$ chirality

Deconvolution of 2W BN FHT Pattern



 10.0 tube



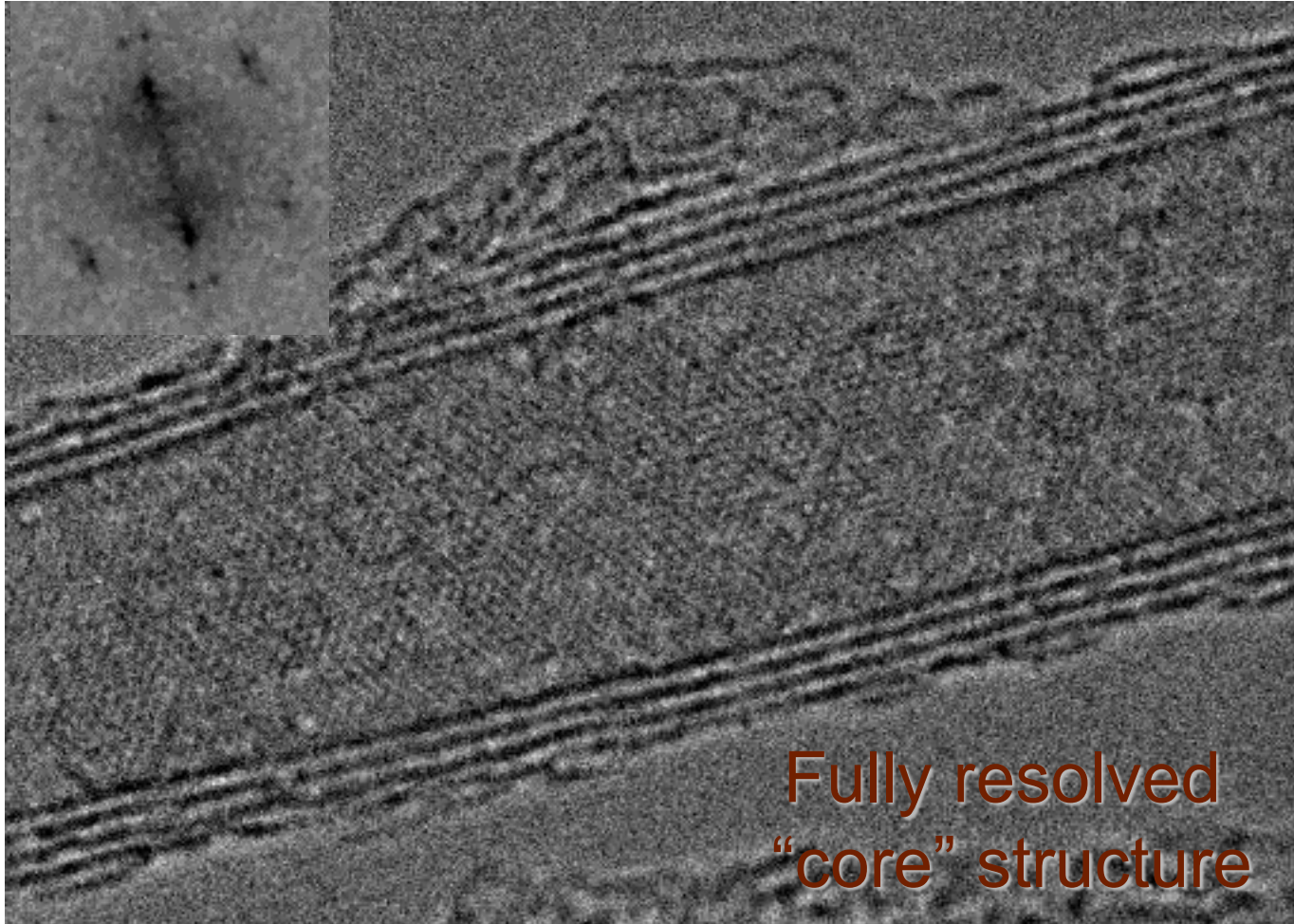
11.0 tube 

Geometrical Arguments

- for axis along $\langle 10.0 \rangle$ (zig-zag)
 - Unit cell “width” = a (= 0.254 nm);
 - Wall spacing = c (= 0.34 nm)
 - Circumference/width = $2\pi c/a = 8.4$ (**high strain**)
 - get defect regions leading to polygonization
 - But if $c = 0.37$,
 - Circumference/width = $2\pi c/a = 9.15$ (**low strain**)
 - less defects

- for axis along $\langle 11.0 \rangle$ (armchair)
 - Unit cell “width” = $\sqrt{3} a$
 - Circumference/w = $2\pi c/a\sqrt{3} = 4.15$ (**low strain**)

BN Four Wall Tube



Results-4 Wall BN Tube

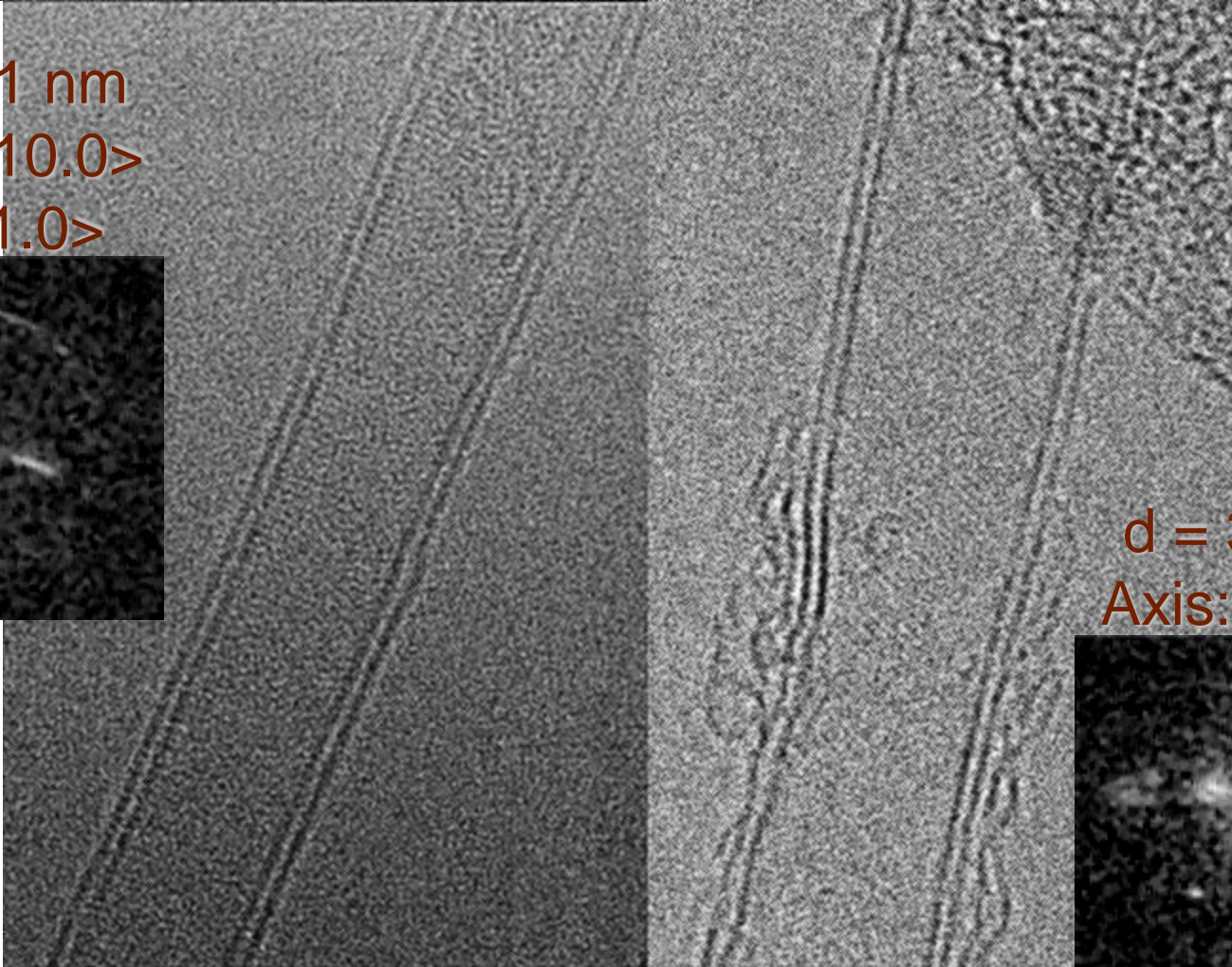
“bilayer” = 0.22 nm
“sidewall” = 0.34 nm

■ all tubes

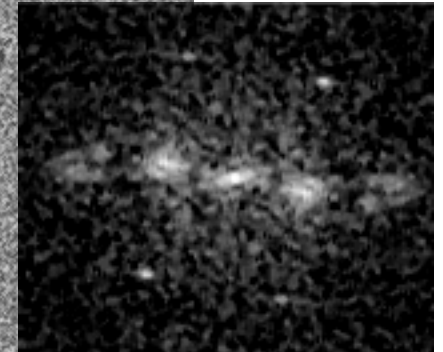
- no orthogonal reflections
 - tube axis $\langle 11.0 \rangle$ (armchair)
- small spot splitting
 - $\sim 4^\circ$ chirality

Core Diameter Effects - 2W

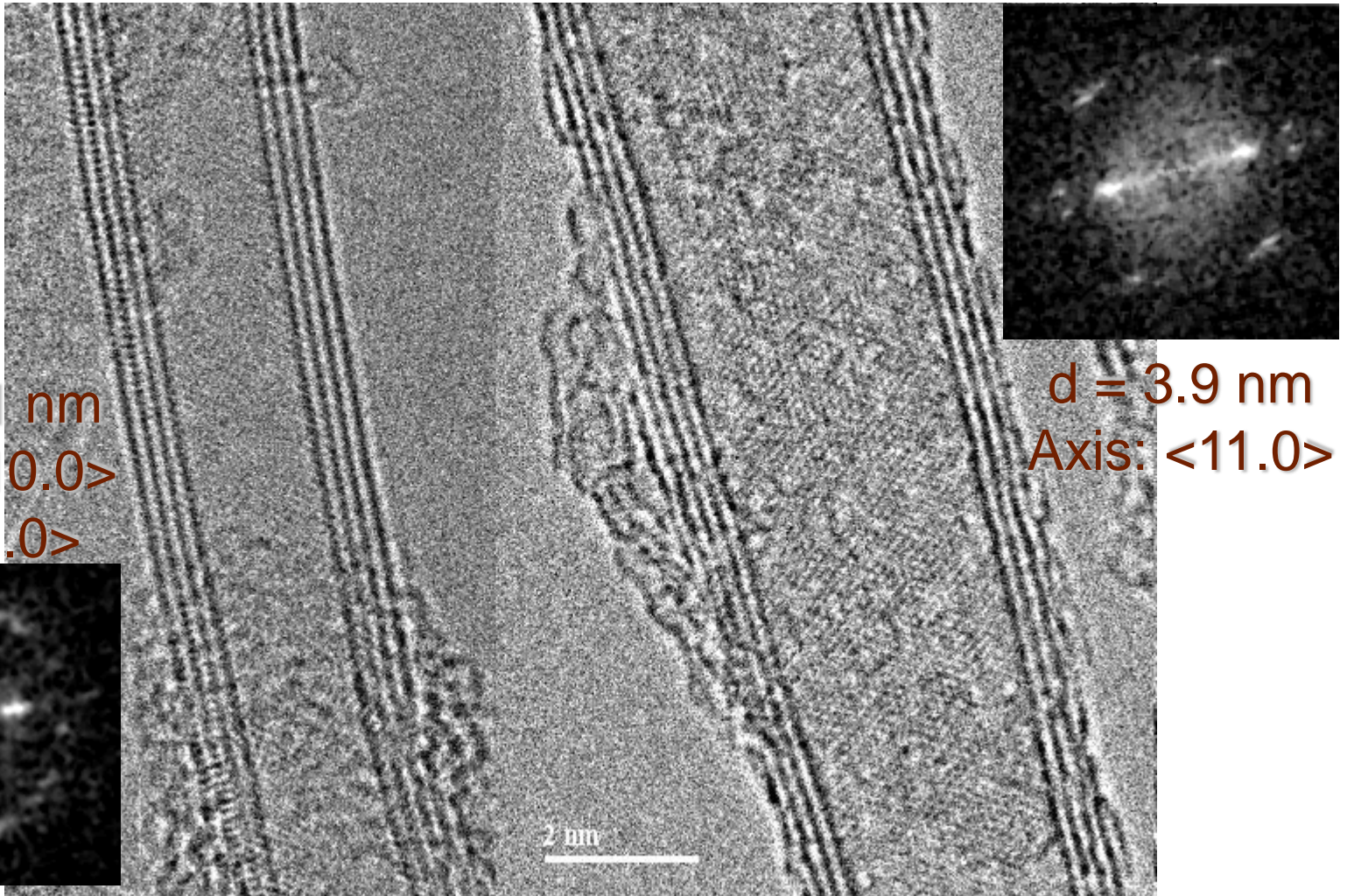
$d = 2.1 \text{ nm}$
Axis: $\langle 10.0 \rangle$
& $\langle 11.0 \rangle$



$d = 3.1 \text{ nm}$
Axis: $\langle 11.0 \rangle$



Core Diameter Effects - 4W



$d = 2.1 \text{ nm}$
Axis: $\langle 10.0 \rangle$
& $\langle 11.0 \rangle$

$d = 3.9 \text{ nm}$
Axis: $\langle 11.0 \rangle$

2 nm

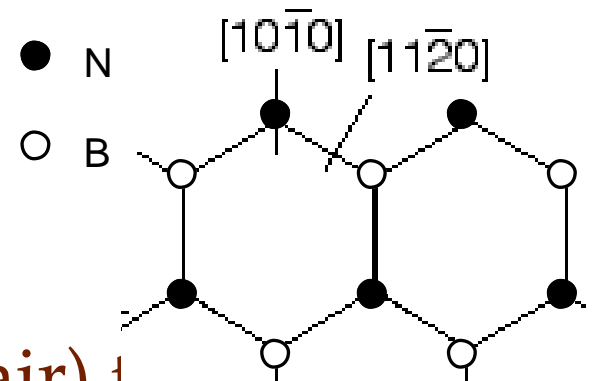
BN NT Growth ($d \sim 2$ nm)

■ First tube

- $\langle 10.0 \rangle$ (zig-zag) due to lower energy of N-terminated planes

■ Subsequent tubes

- Readjust to give $c > 0.34$ nm
- Align along $\langle 11.0 \rangle$ (armchair) to minimize tube closure strain

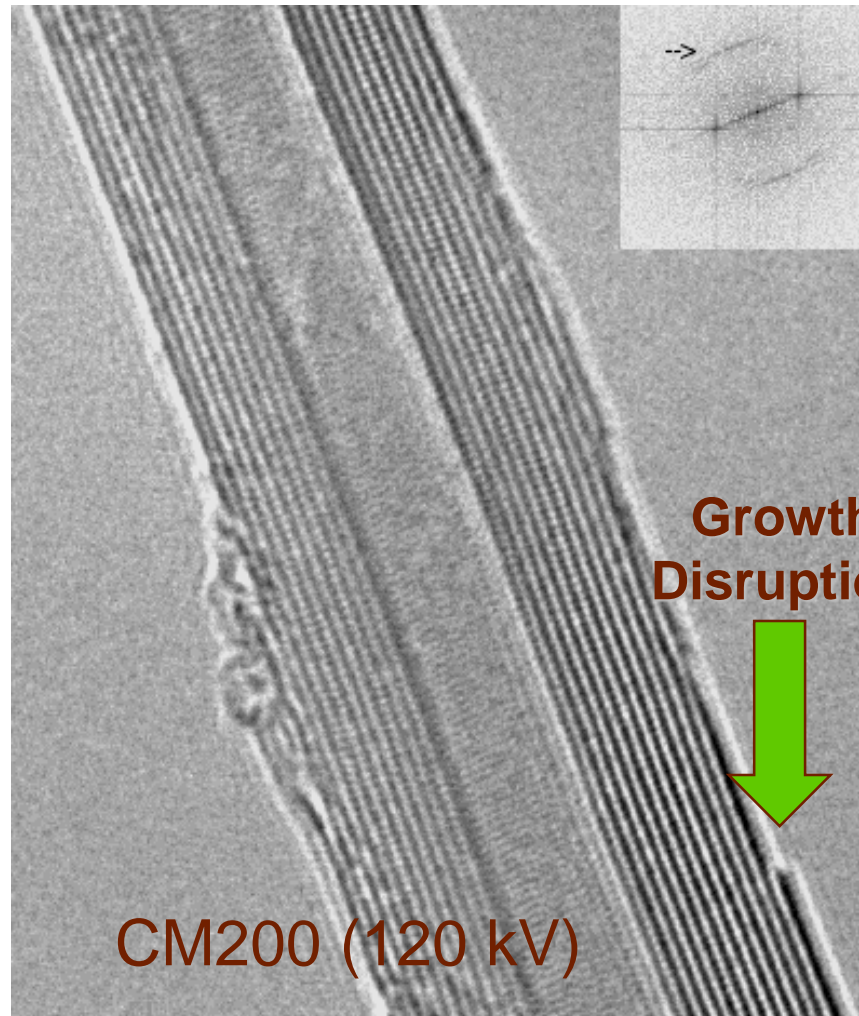


➔ CNT-no energetic preference ←

BN NT Growth ($d \sim 3$ nm)

- Alignment along $\langle 11.0 \rangle$ (armchair) to minimize tube closure strain
- Tubes (2W & 4W) nearly defect-free
 - near predicted mechanical properties possible

Multiwall BN Tubes

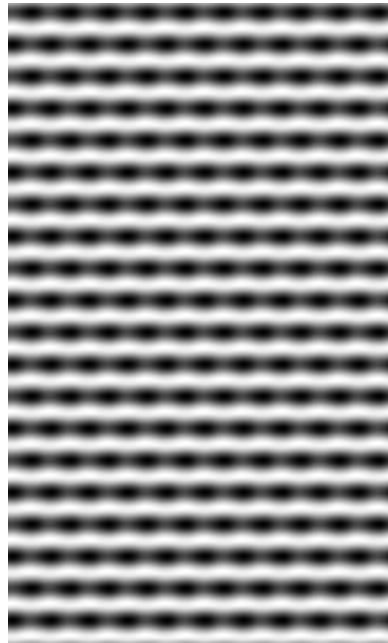


Results-Multiwall BN Tubes

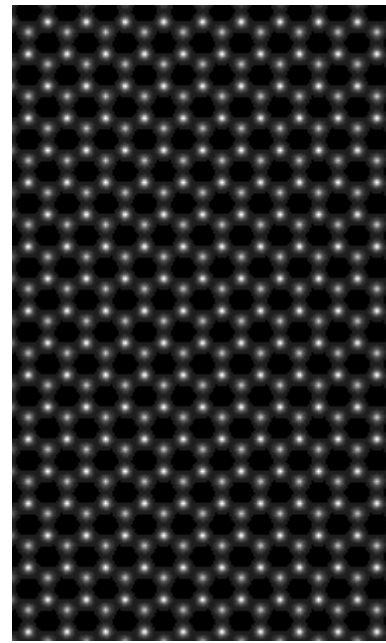
“bilayer” = 0.22 nm
“sidewall” = 0.34 nm

- tube axis $\langle 11.0 \rangle$
- tilt & chirality evident from FHT
- growth termination in outer walls

6W BN Image Simulation

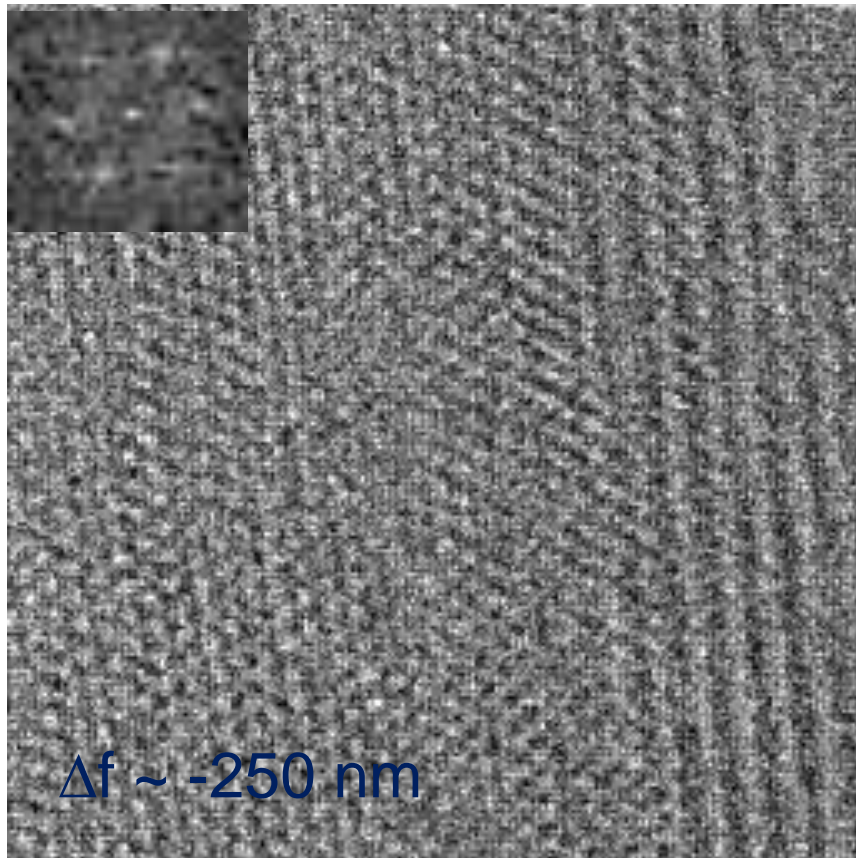


Simulated Image
 $\Delta f = -280 \text{ nm}$

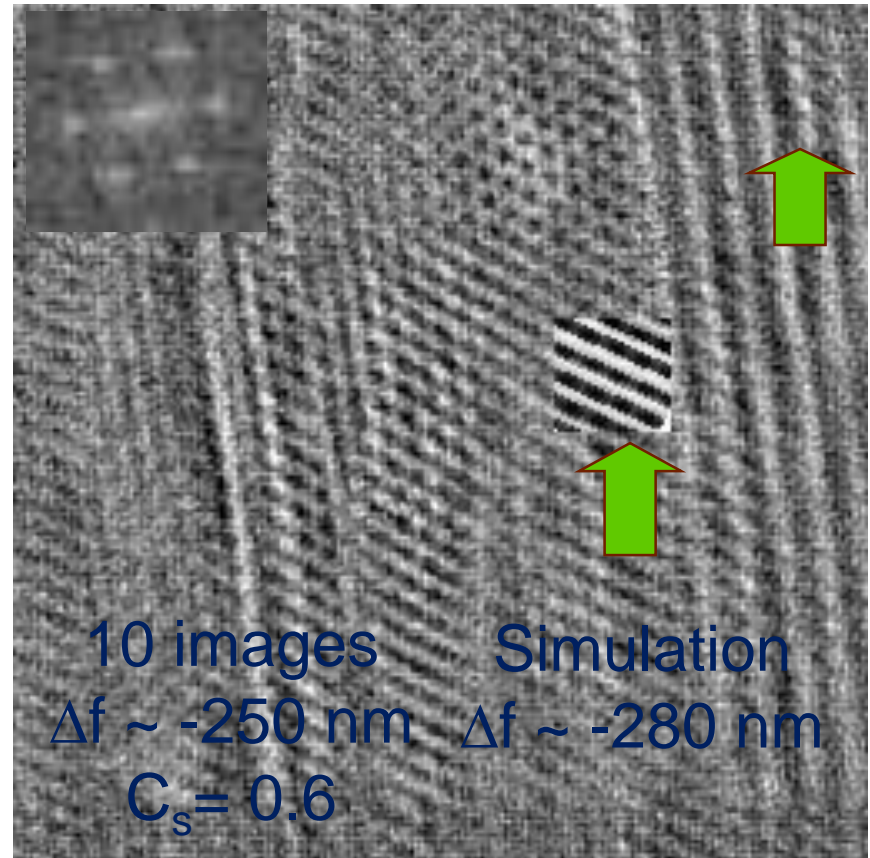


Projected Potential

6W BN Reconstructed Image

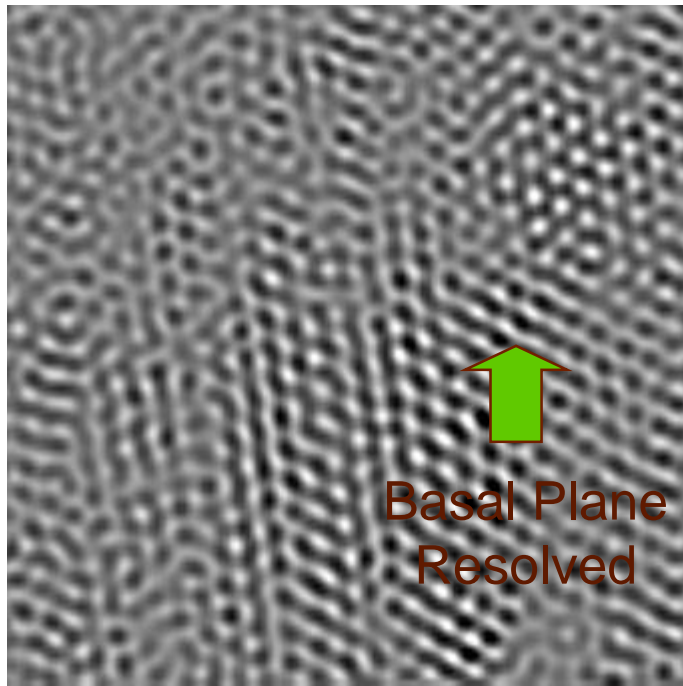


Single Image

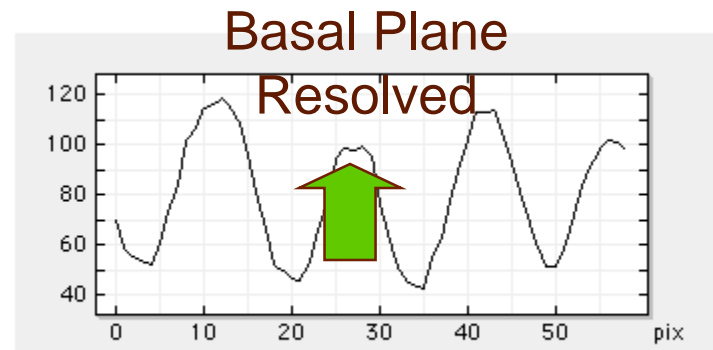


Reconstructed Image

6W BN Image Reconstruction



Reconstructed Image



Line Intensity Scan
(along basal plane)

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