

Can we save lives with thermodynamics?

Nanoengineering and Thermofluids for the Water-Food-Energy Nexus

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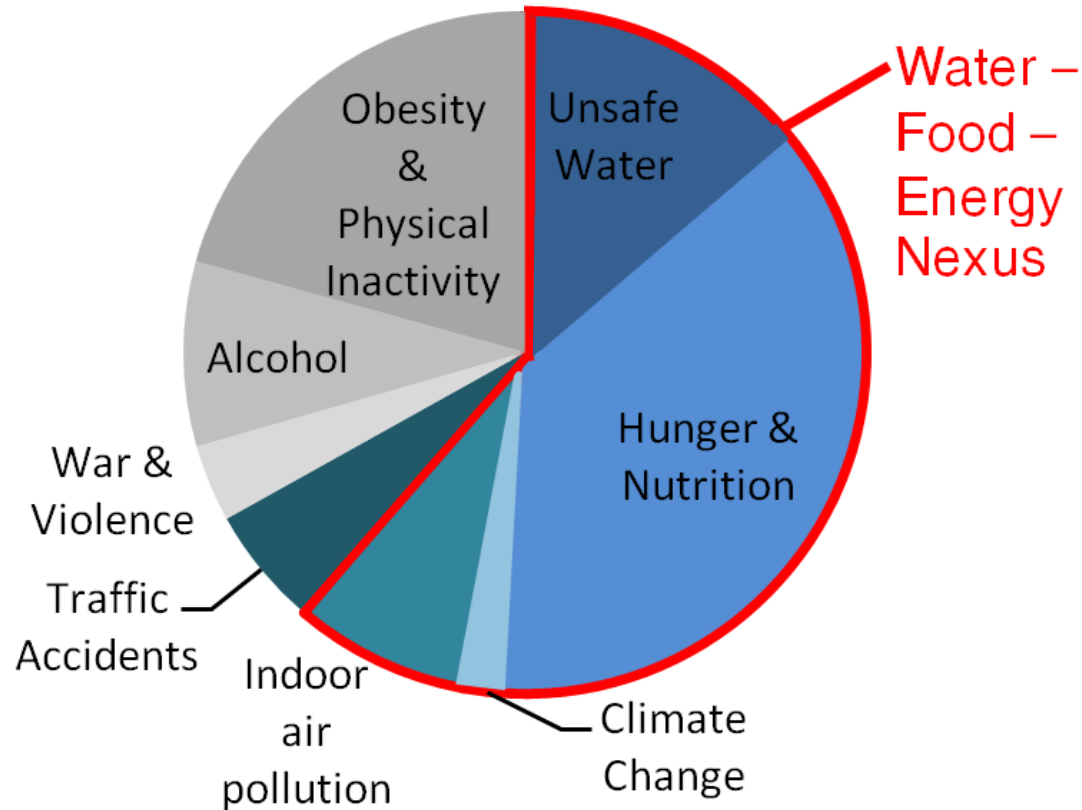


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School of Engineering
and Applied Sciences

PostDoc

February 21, 2017

Global Preventable Causes of Death



Global Preventable Causes of Death

WHO, -factsheets 2014

In 2015 World Economic Forum named “Water Crisis” as the most likely and most impactful global economic risk



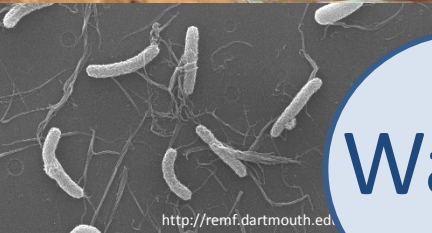
<http://managewaste.org>



<http://www.science20.com>



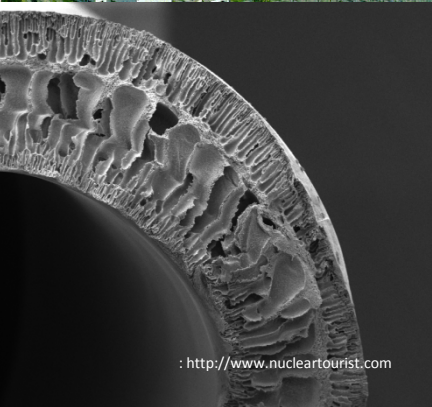
<http://www.agricultureguide.org>



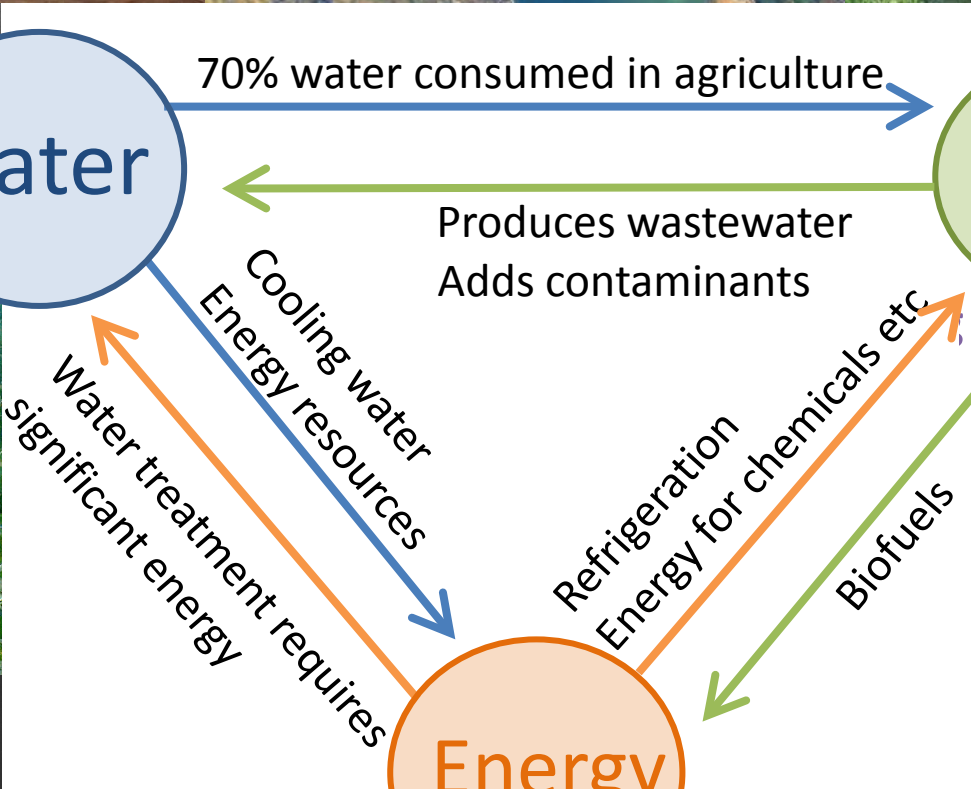
<http://remf.dartmouth.edu>



<http://www.sustainable-desalination.net>



<http://www.nucleartourist.com>



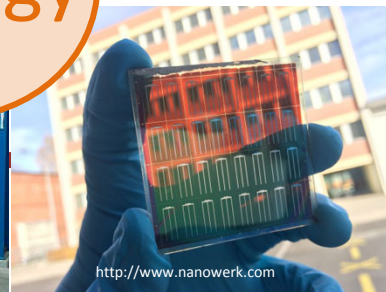
<http://montcalm.co.uk>



<http://news.mit.edu>



<http://www.water-technology.net/>



<http://www.nanowerk.com>

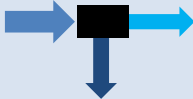


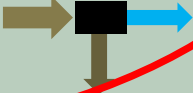
<http://blueclicksondata.com>


Options to Provide Water

Supply


Demand

• Desalination 

• Reuse of sewage or agricultural water 

• Use water more efficiency 

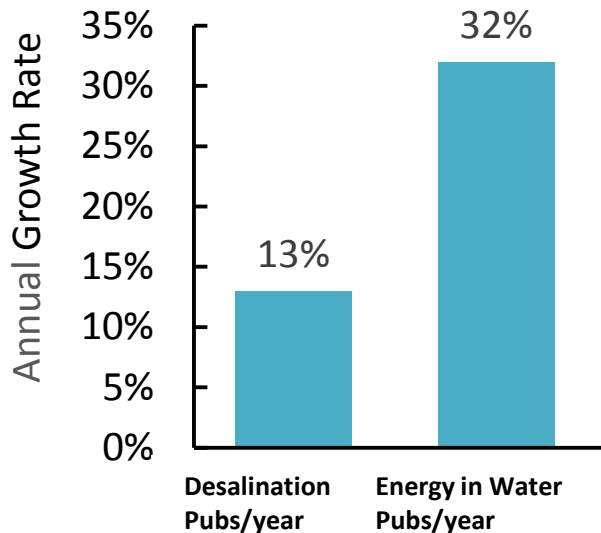
• Reduced population 

• Reduced economy 

• Relocate people 

Growing Water Focus

Water Researchers



Government (funding)



Example:
\$72 million/year NSF:
Innovations at the Nexus of
Food, Energy and Water
Systems (INFEWS) (2016)

Publishers: Two new journals in 2016:



Environmental Science: Water Research & Technology



Sources

[1] "Global desalination market set to grow 320.3% by 2020 - driven by RO," Membrane Technology, vol. 2011, no. 10, pp. 7–, 2011.

[2] U. E. I. Administration, International Energy Outlook 2016. U.S. Department of Energy, 2015.

[3] The Water and Food Nexus: Trends and Development of the Research Landscape, Stockholm International Water Institute and Elsevier, 2012

Thermo-nano scientific techniques for water

**Systems
thermodynamics**

Thermochemistry

**Nanomaterial
fabrication**

Optimization

Transport
phenomena

Interfacial
energy

Nanomaterial
characterization

Novel
configurations

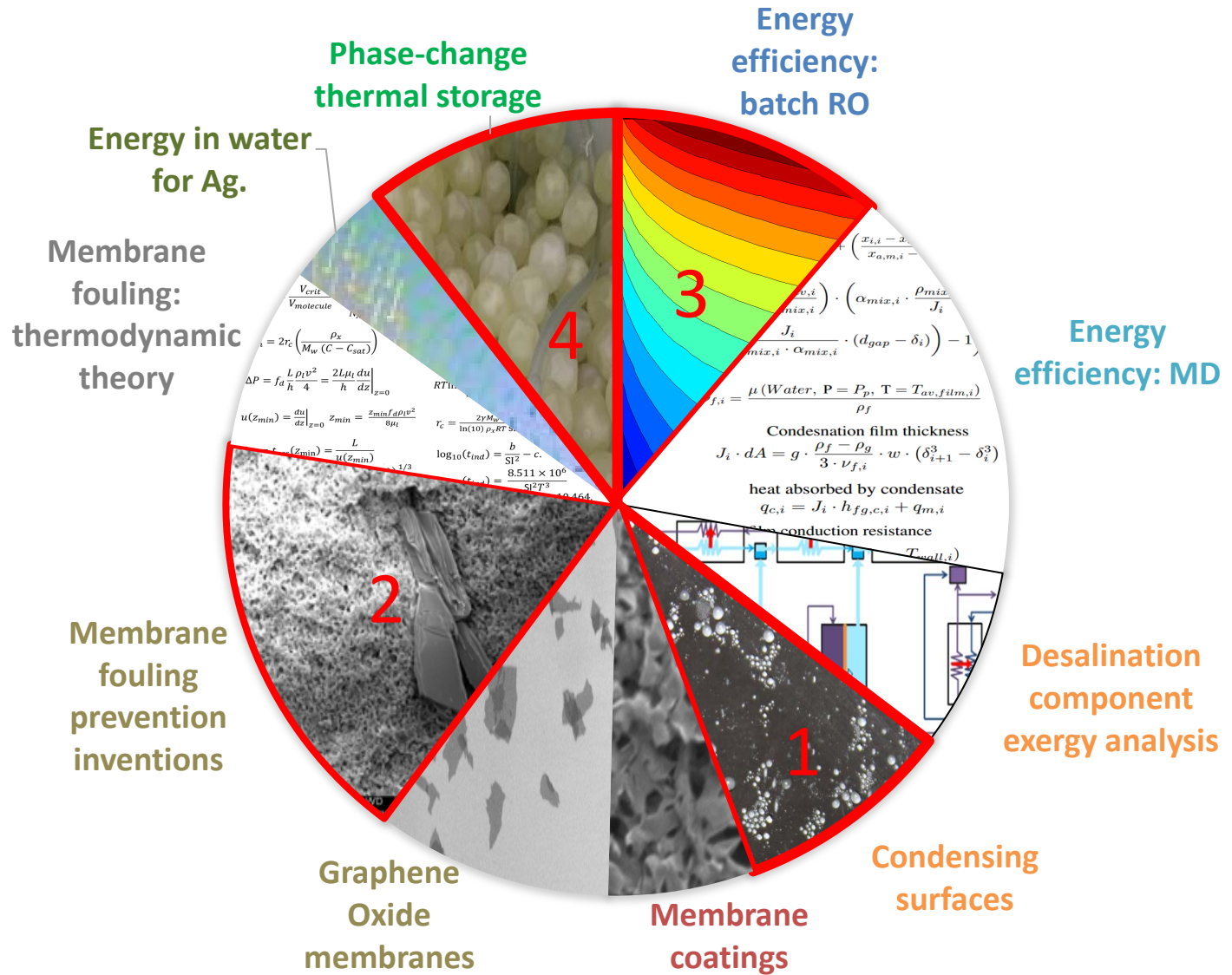
Nucleation
kinetics

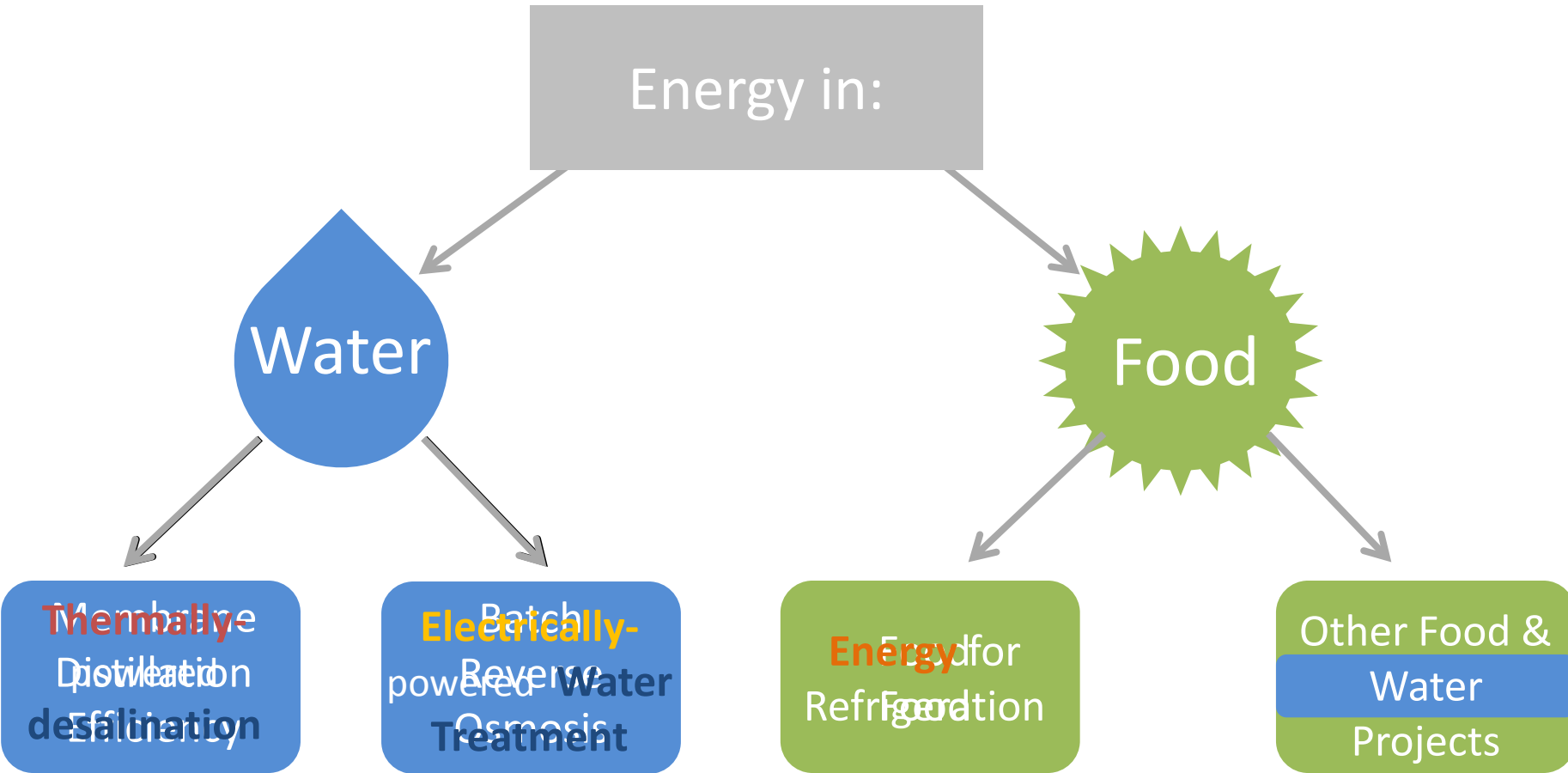
Hydro-phobic/
phillic

Antifouling
systems

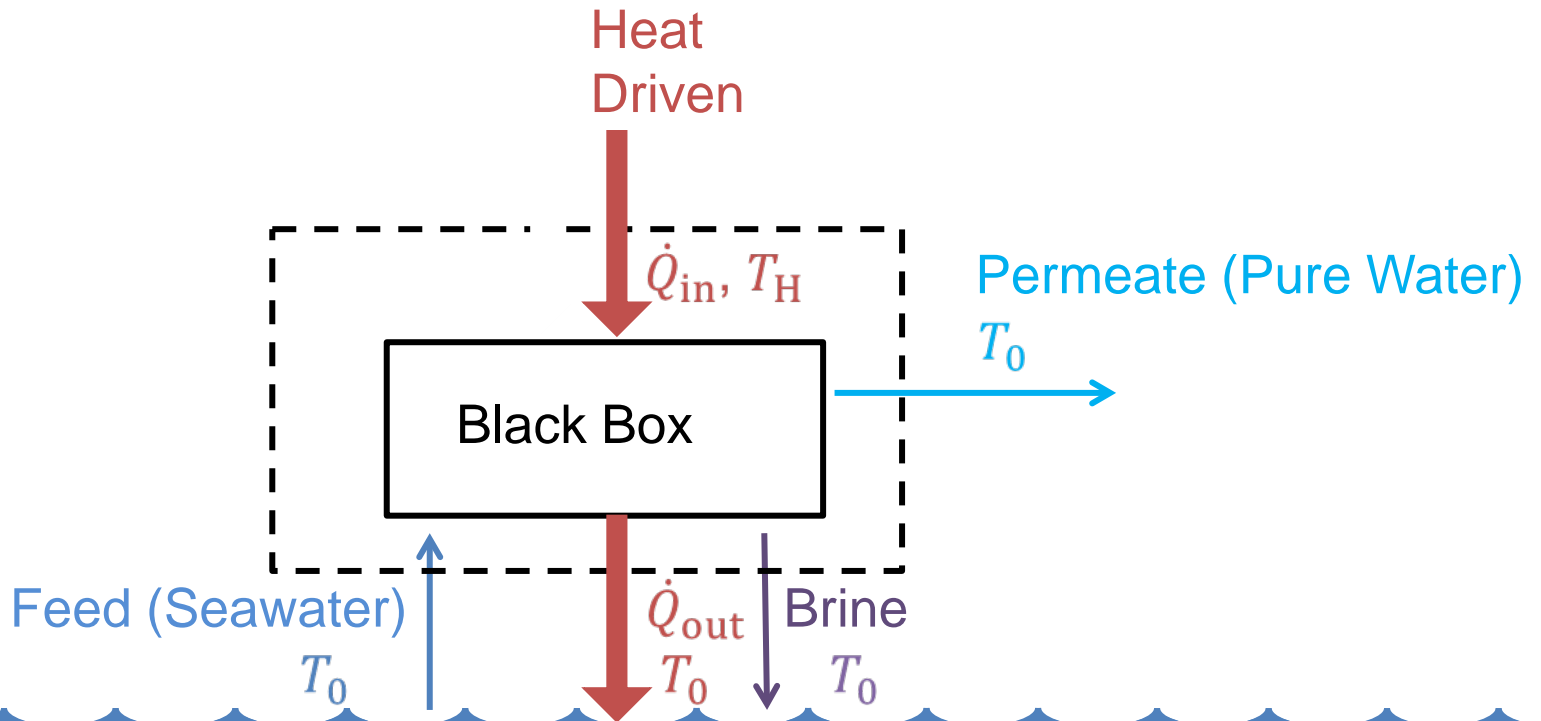
Porosity vs
rejection

My Research





Desalination Systems Level



Definitions

Recovery
Ratio

$$RR = \frac{\dot{m}_{\text{permeate}}}{\dot{m}_{\text{feed}}}$$

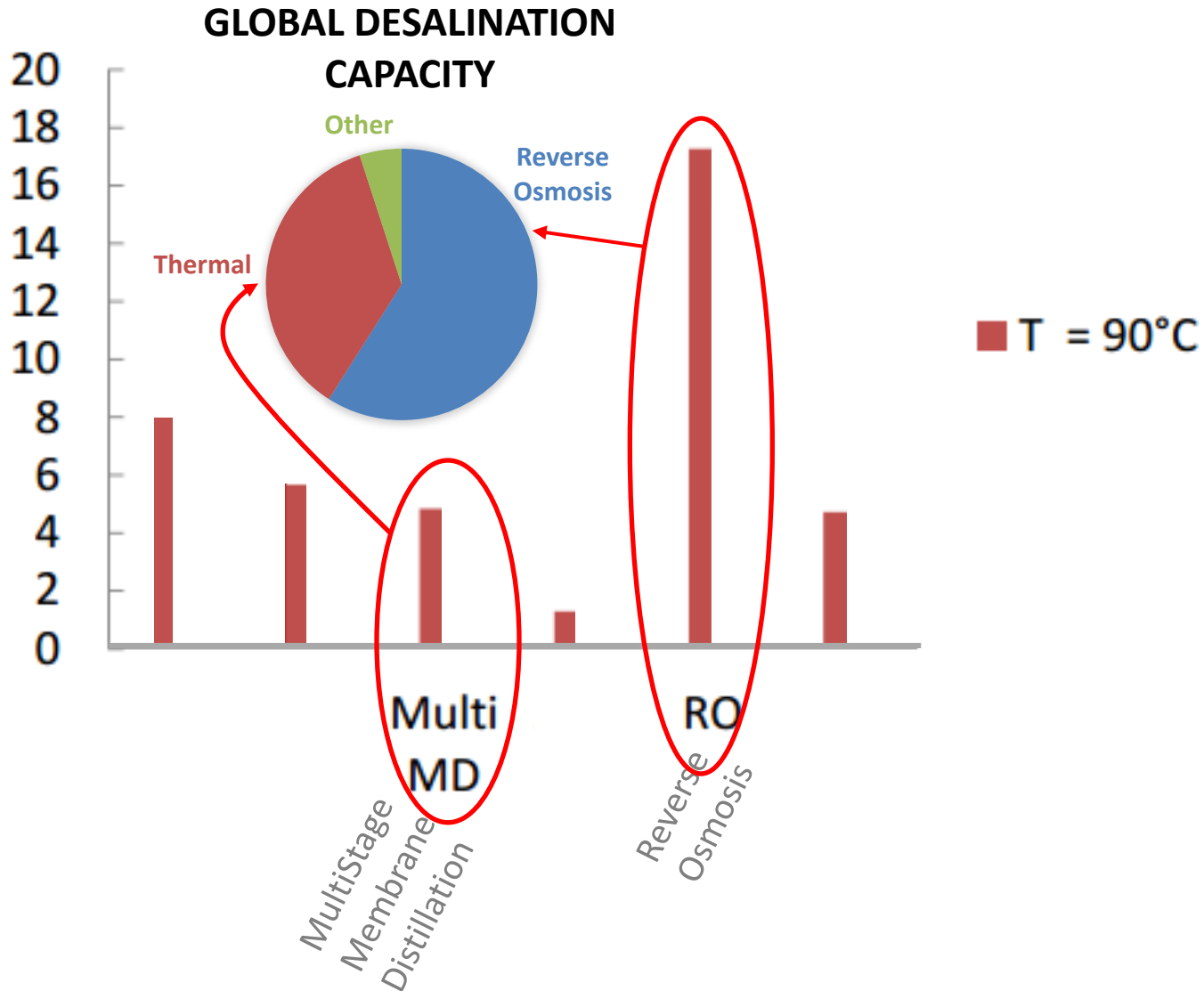
2nd-law
efficiency

$$\eta_{II} = \frac{\dot{W}_{\text{least}}^{\text{min}}}{\dot{W}_{\text{used}}}$$

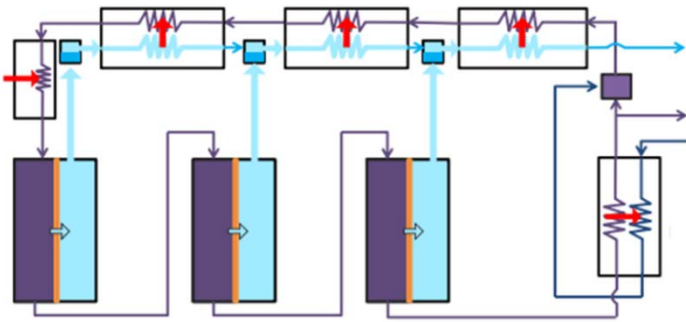


Des

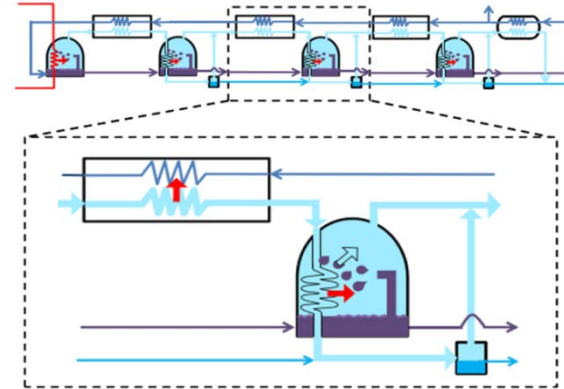
$\gamma \eta_{II}$



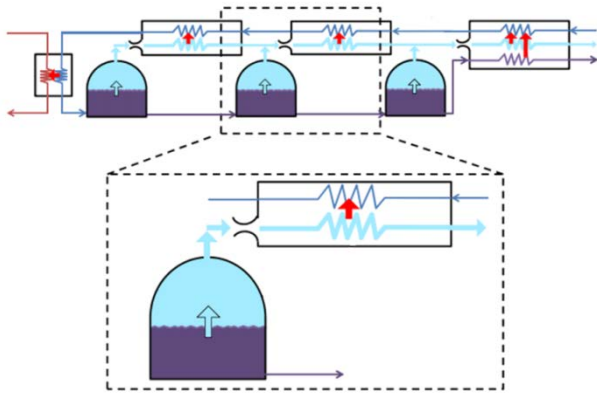
Multistage Vacuum MD



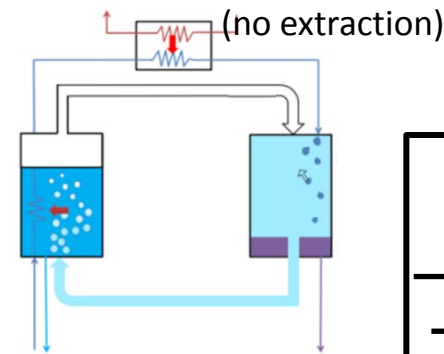
Multiple Effect Distillation (MED)



Multistage Flash (MSF) (once through)



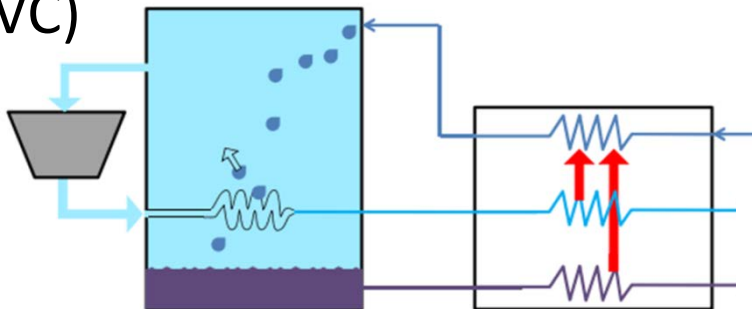
Humidification-Dehumidification (HDH)



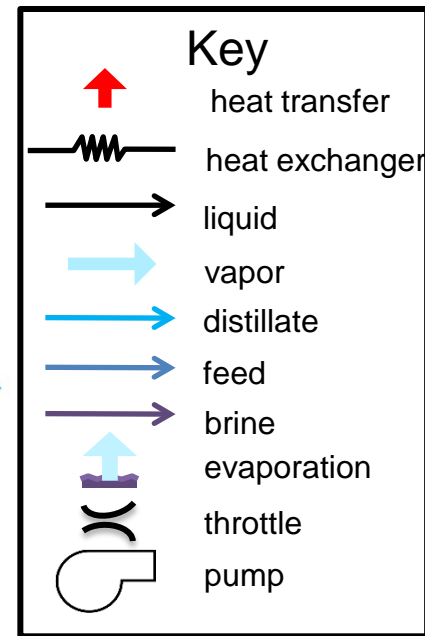
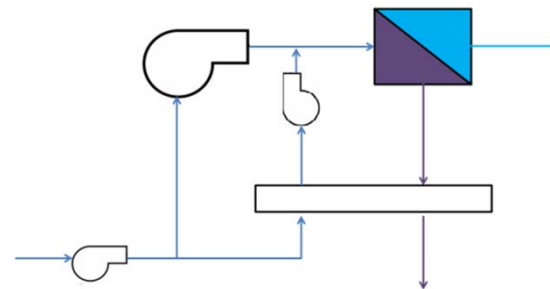
Mechanical Vapor Compression (MVC)

(MVC)

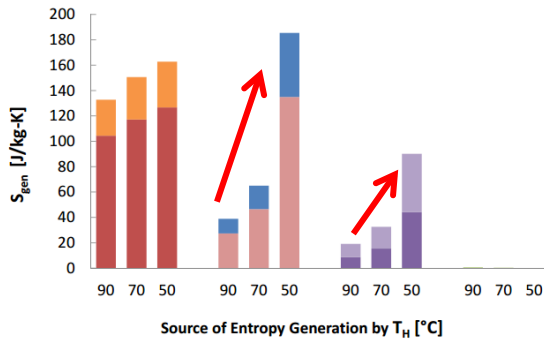
(single effect)



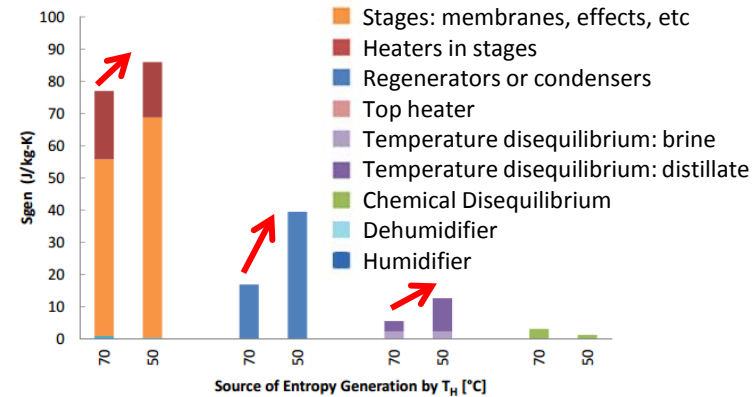
Reverse Osmosis (RO)



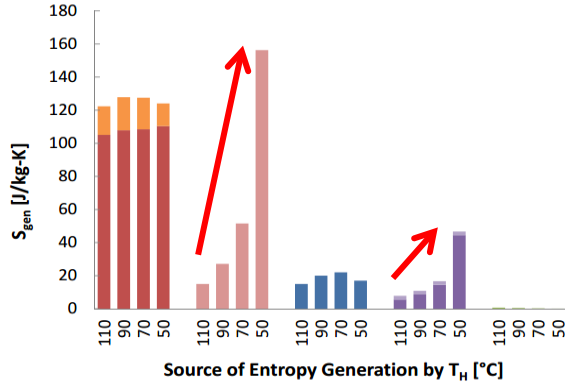
Multistage Vacuum MD



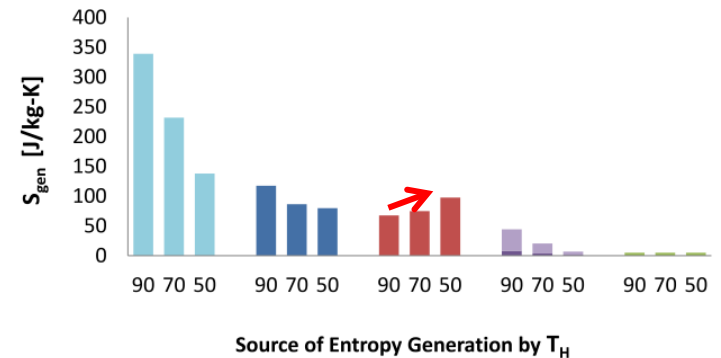
Multiple Effect Distillation (MED)



Multistage Flash (MSF) (once through)

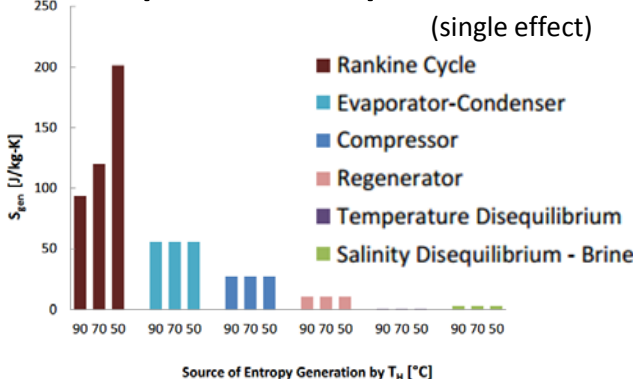


Humidification-Dehumidification (HDH)

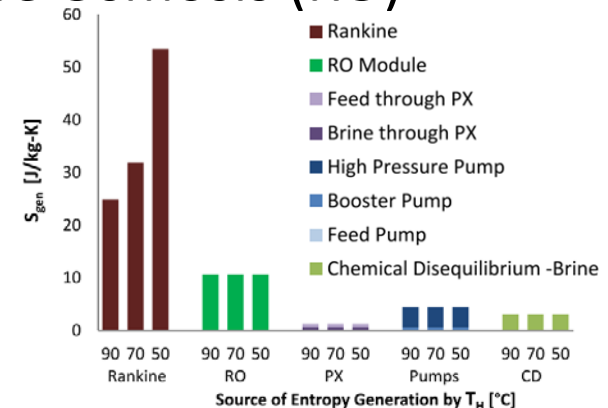


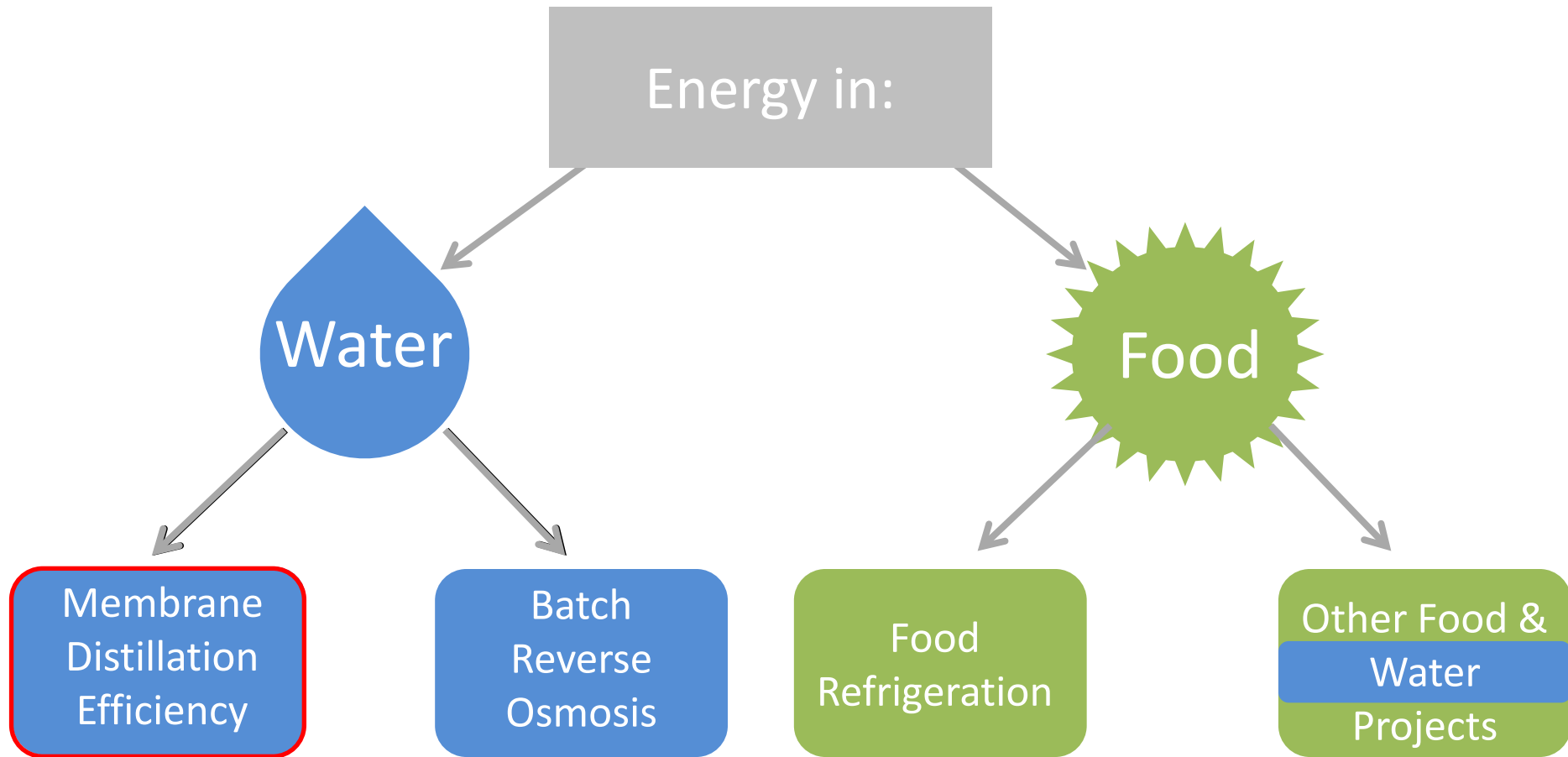
Mechanical Vapor Compression

(MVC)



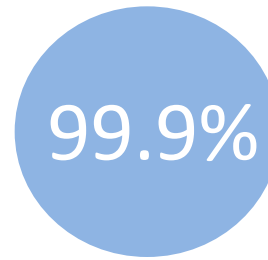
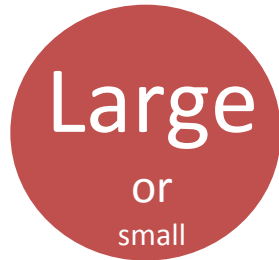
Reverse Osmosis (RO)





Thermal power with **desalination**

Membrane Distillation Advantages

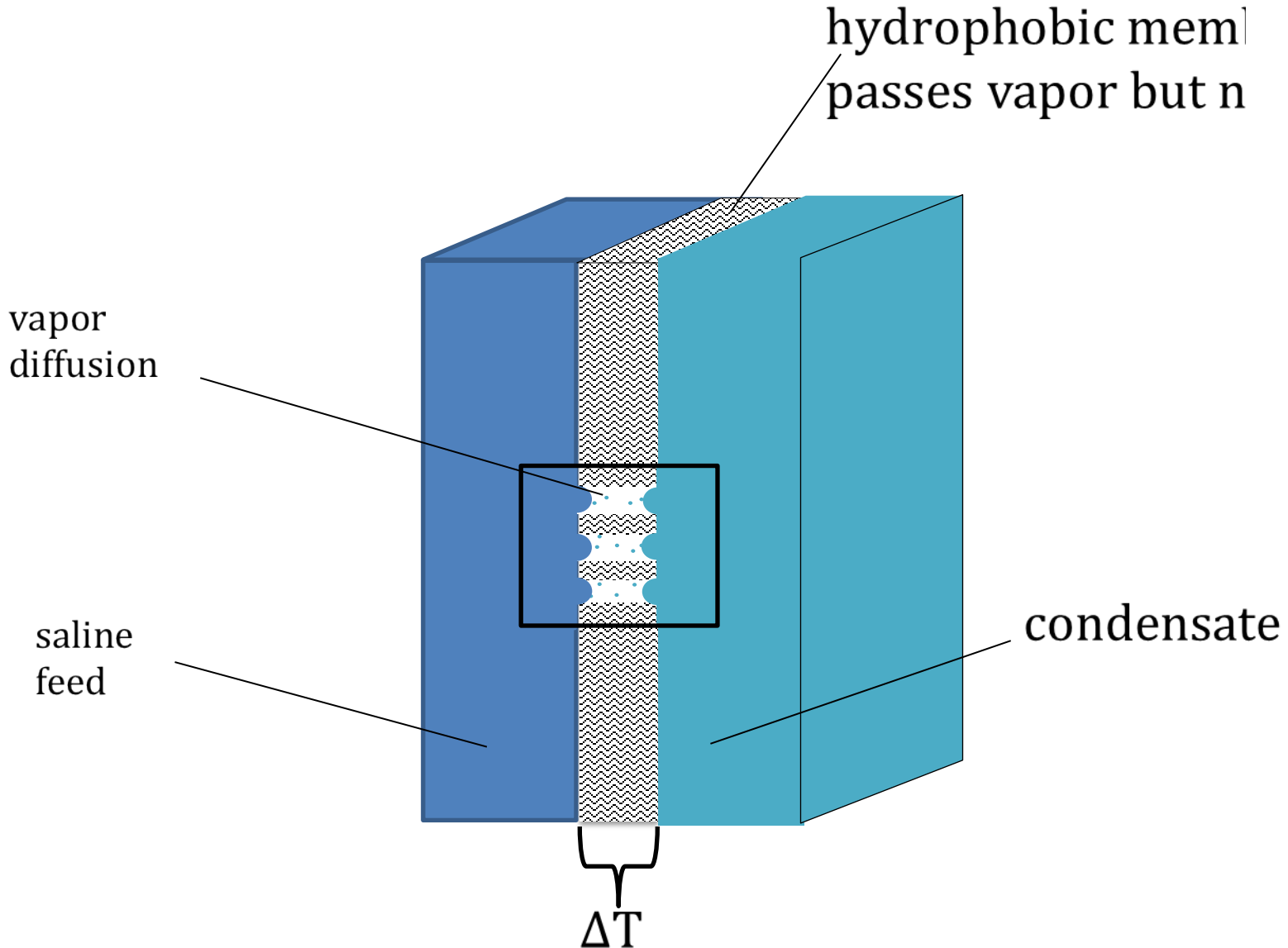


MEMSTILL

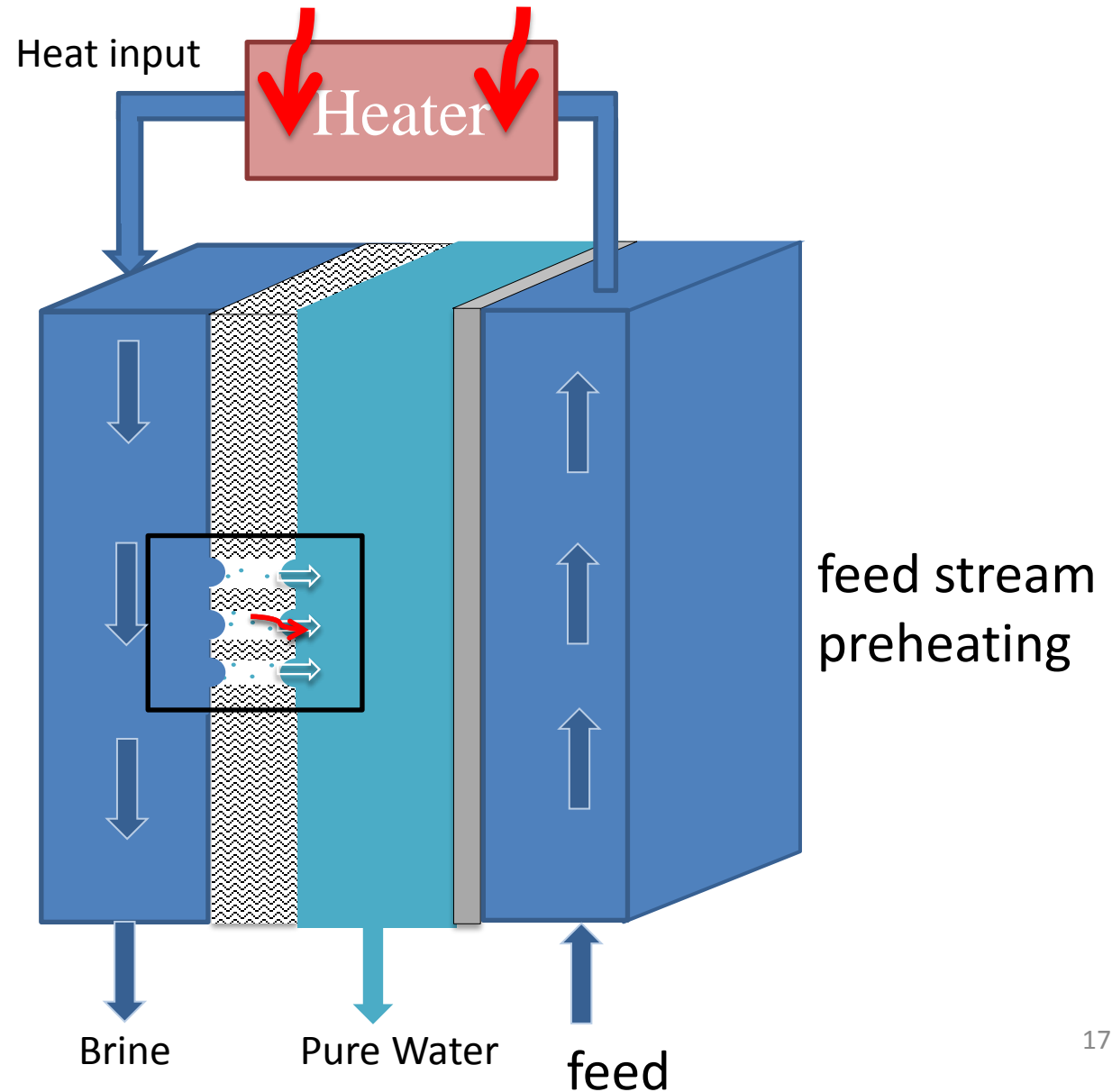
XZERO AB



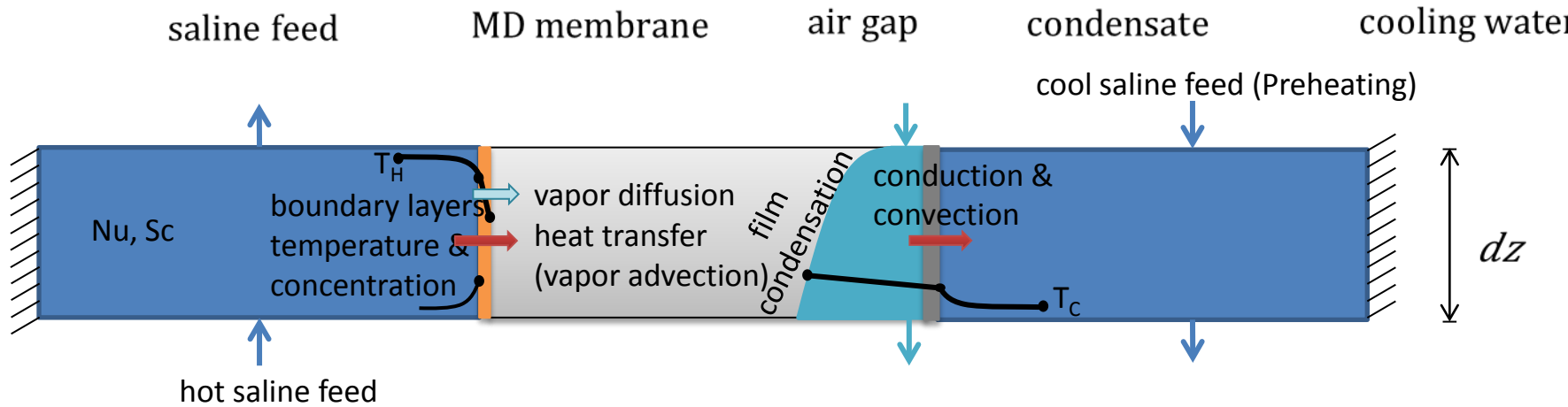
Membrane Distillation Process



Membrane Distillation Process



AGMD Computational Cell



Primary trade off:

Flux $J = B * \Delta P_{vapor\ pressure}$

J	flux	[kg/m ² s]
B	MD membrane permeability	m ² s/kg
\dot{Q}	Heat transfer rate	[W]

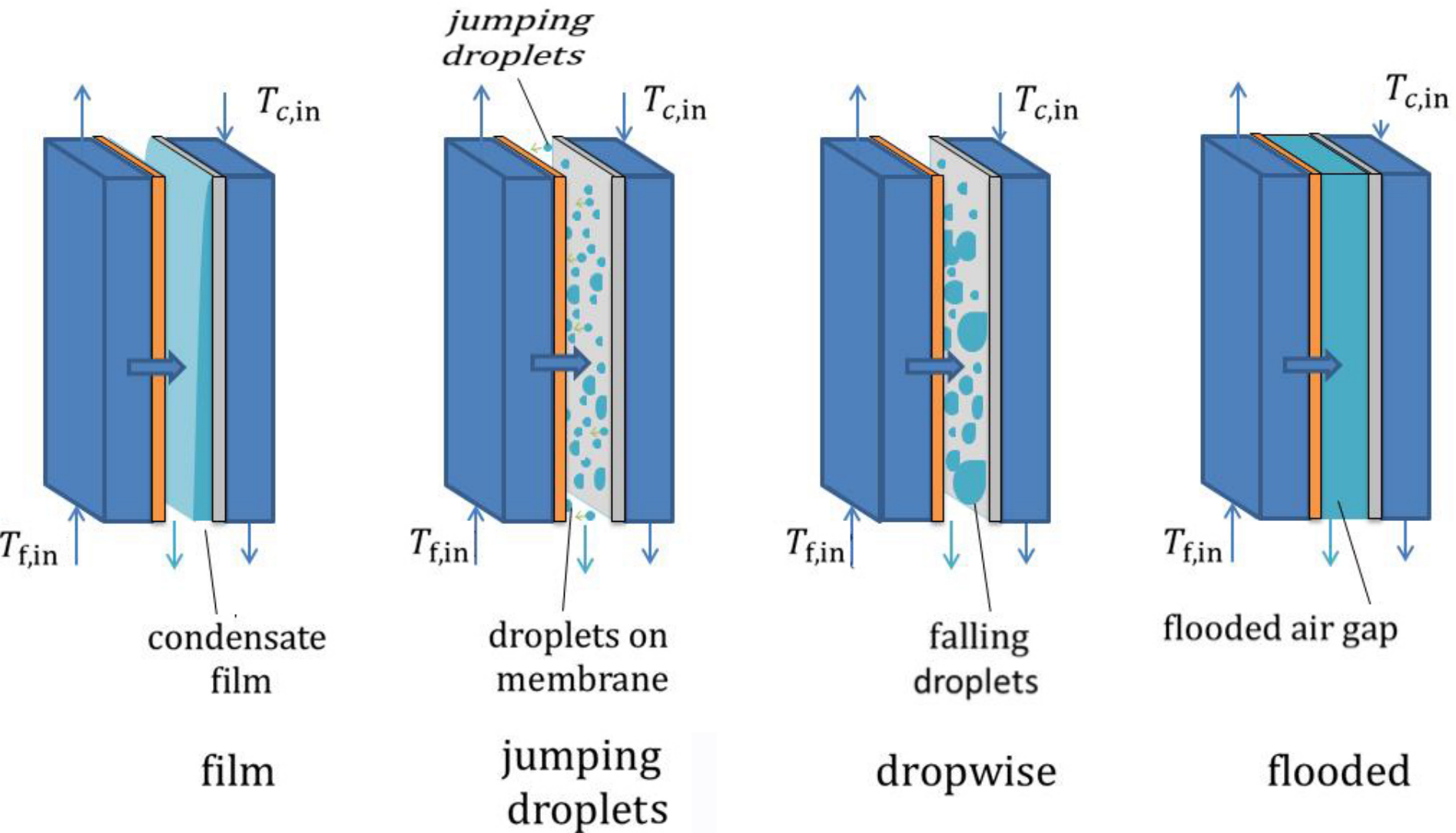
thermal efficiency $\eta_{MD} = \frac{\dot{Q}_{evap}}{\dot{Q}_{evap} + \dot{Q}_{cond}}$

Subscript Key
 $_{evap}$ evaporation
 $_{cond}$ conduction

Jumping droplet condensation



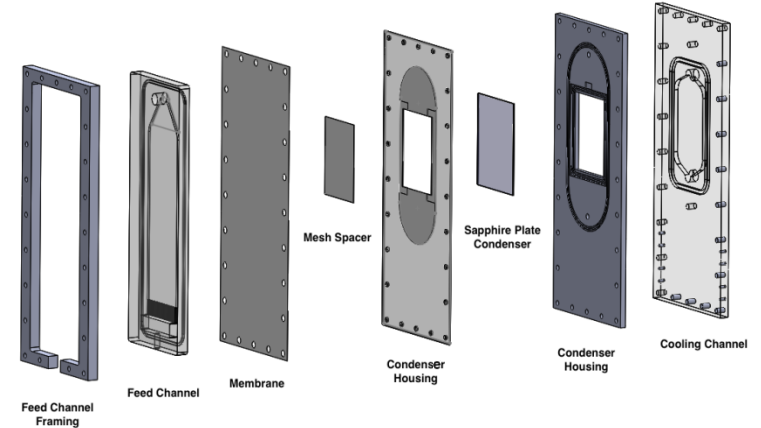
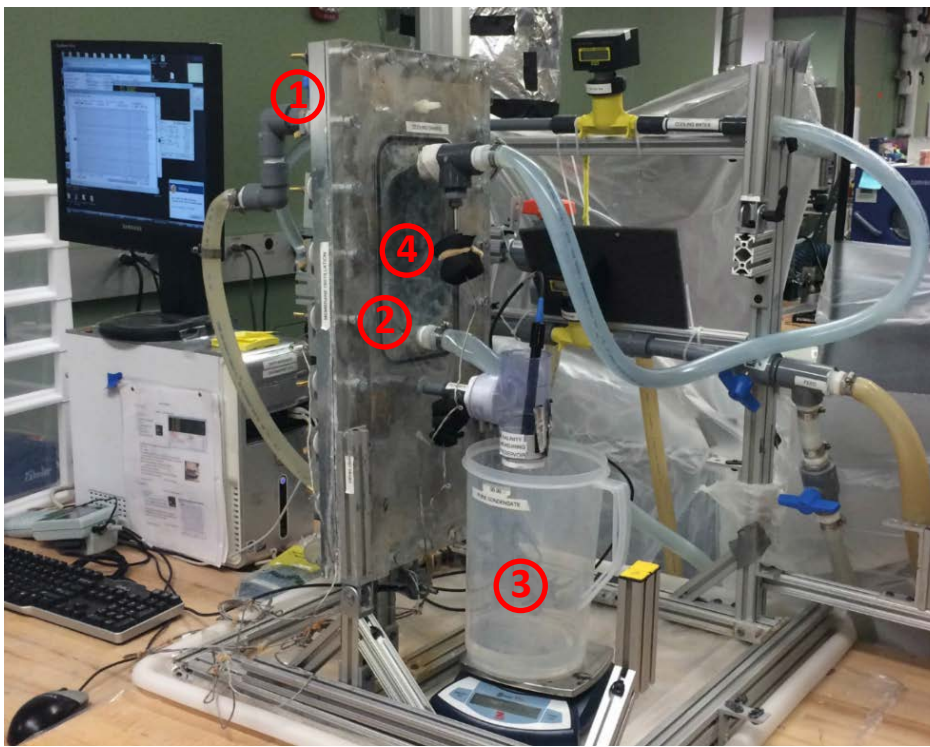
Air Gap Membrane Distillation: *Flow Regimes*



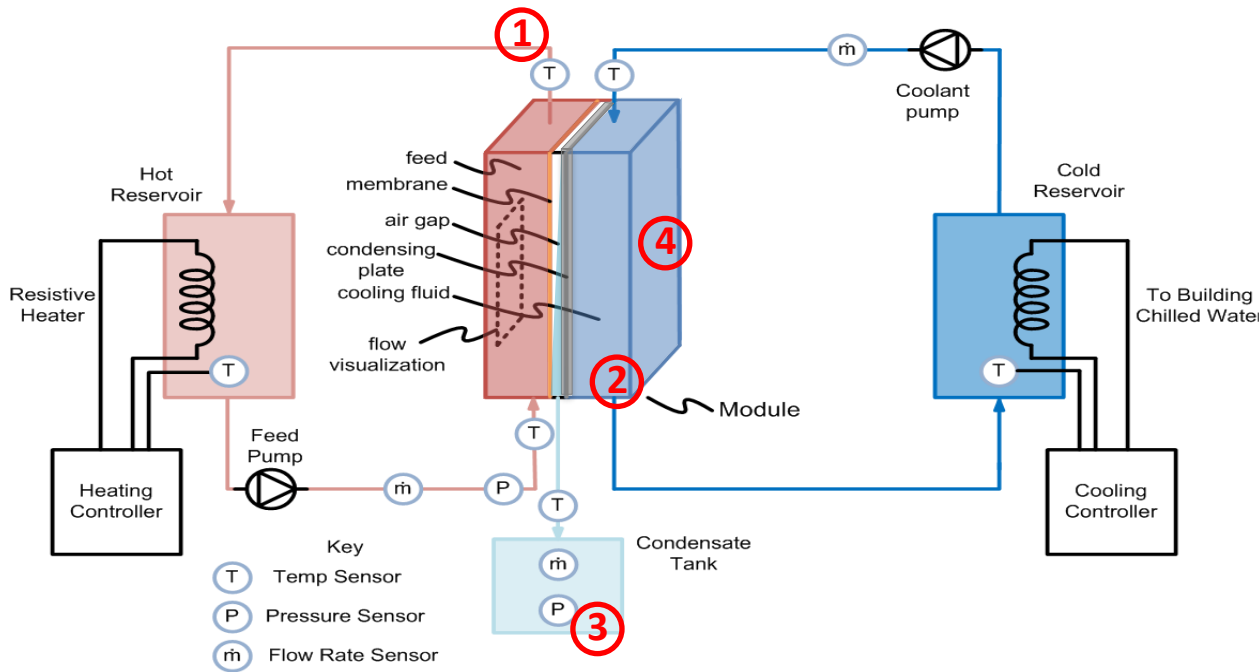
1. David Warsinger, Jaichander Swaminathan, Laith Maswadeh, and John Lienhard V. Superhydrophobic condenser surfaces for air gap membrane distillation. In *planned submission to Desalination*, October 2014.

2. David Warsinger, Jaichander Swaminathan, and John. Lienhard V. Superhydrophobic condensing surfaces for air gap membrane distillation, October 2014. reference number 16942.

Air-Gap Membrane Distillation Experimental Setup

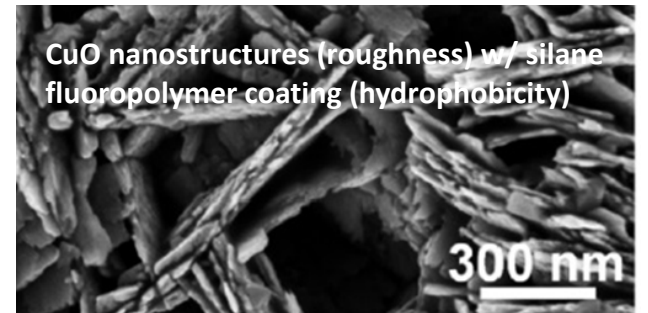
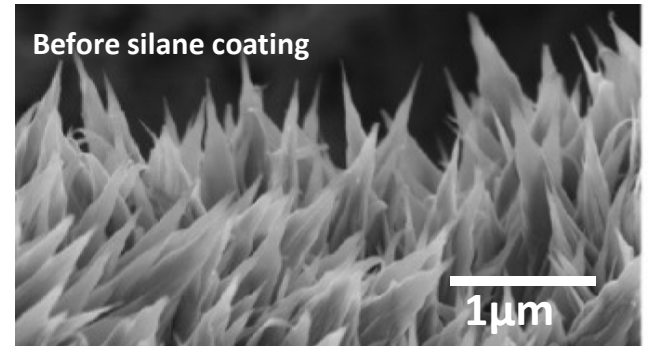
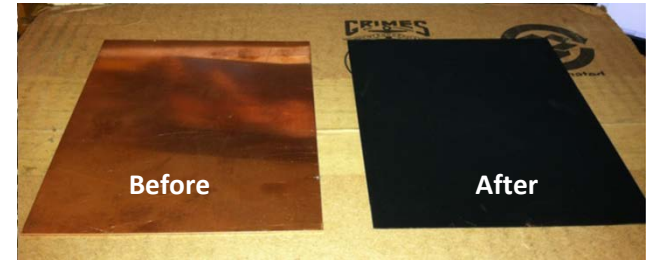
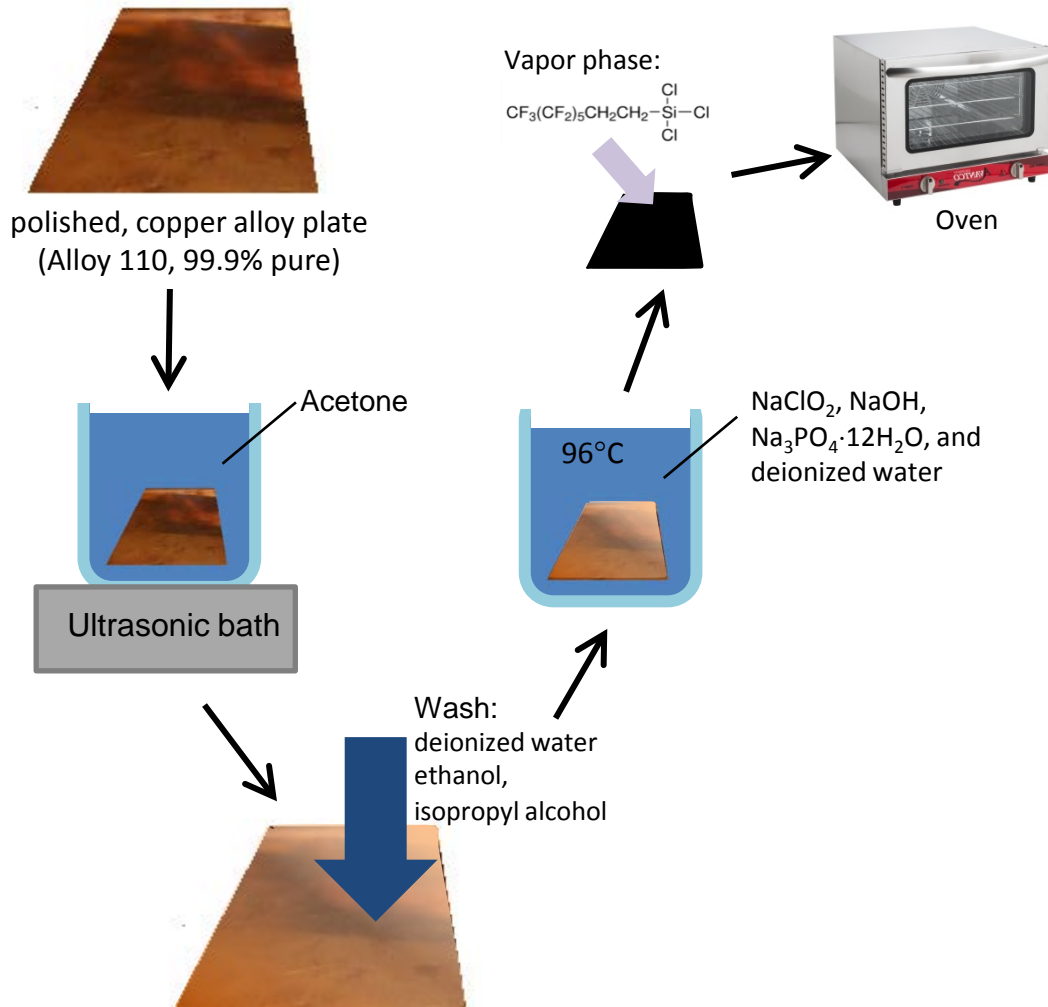


CNC Plates for Membrane Module



Sapphire condensing surface (visualization)

CuO Superhydrophobic Surface Fabrication



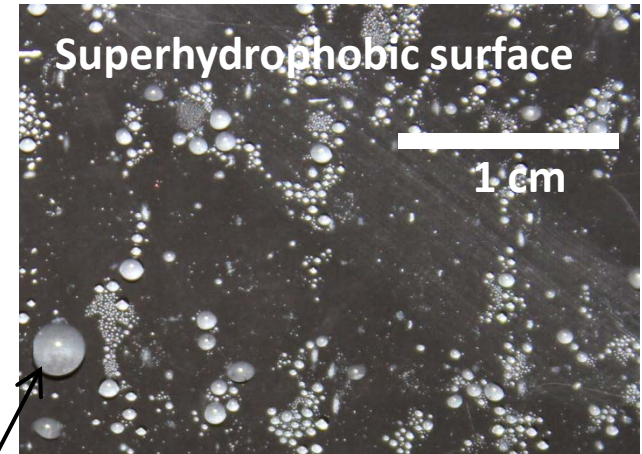
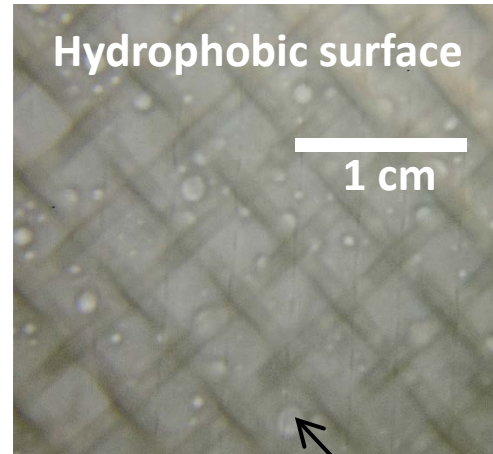
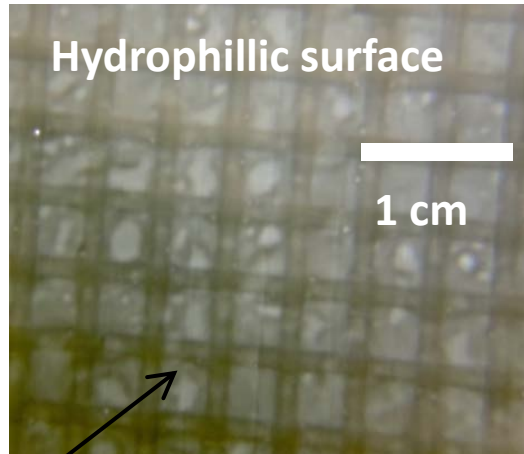
1. D. M. Warsinger et al., Journal of Membrane Science, vol. 492, pp. 578–587, 2015.
2. N. Miljkovic et al. Nanoletters, vol. 13, pp. 179–187, 2012.

CuO Superhydrophobic surface desired properties

- High roughness (hydrophobicity)
- Low surface energy coating (hydrophobicity)
- Thin self-limiting layer (thermal conductivity)
- Materials with high thermal conductivity (CuO)
- Robustness for long duration operation
- Scalable to large sizes cheaply (via bath process)



Hydrophobic condensing in MD



Visualized through sapphire condensing surface

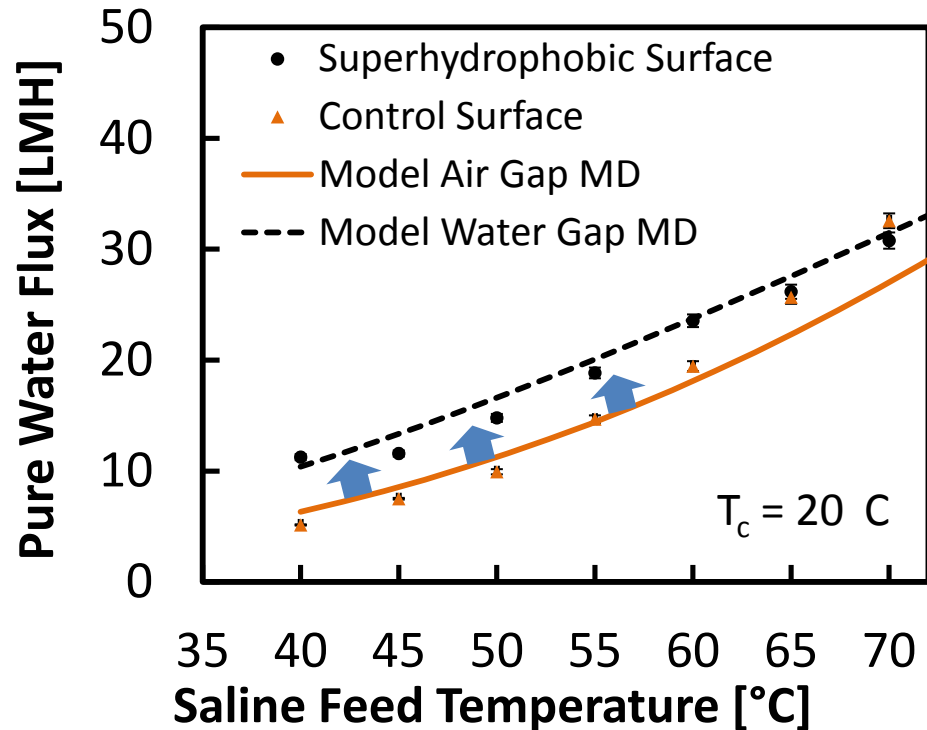
After operation, membrane removed

Summary of the influence of gap and configuration changes on permeate flux

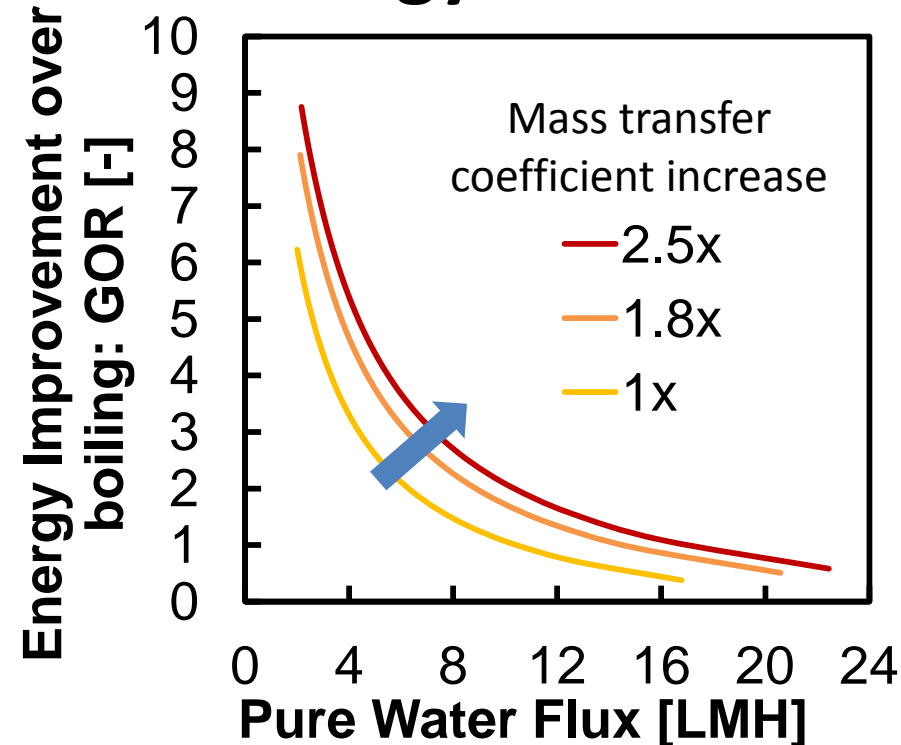
parameter	Spacer Orientation	Surface Hydrophobicity	Spacer Hydrophobicity	Mesh Thermal Conductivity	Tilt Angle
range/details	horizontal & diagonal	Contact angle of <math><20^\circ</math> to 164°	Contact angle of $\sim 80^\circ$ to $\sim 150^\circ$	~ 0.3 to 400 W/m ² K	Module tilt of 60° to 85°
Flux Increase	<math><5\%</math>	0-110%	-22-2%	21-119%	0-54%

Jumping Droplet Condensation in Membrane Distillation CuO Coated and silanized surfaces

Improved Condensate Flux



Improved Flux vs Energy Tradeoff

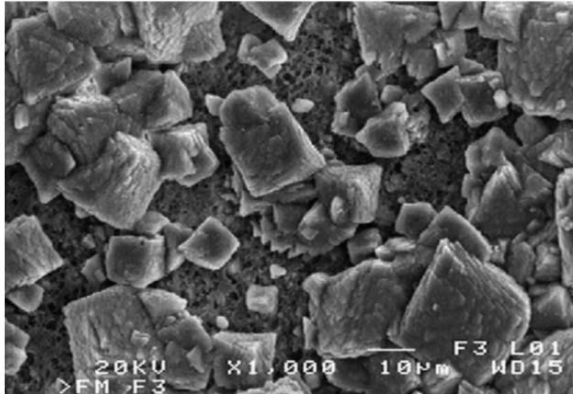


Implications of hydrophobic condensing

- It improves **flux** substantially, and overall **efficiency** (GOR). Are similar gains possible in other thermal desalination technologies?
- Can other condensing and micro-fluidic nanotechnologies improve this and others, including directional **wicking**?
- How will technologies be **designed differently** at the nano and system-level with these techniques?

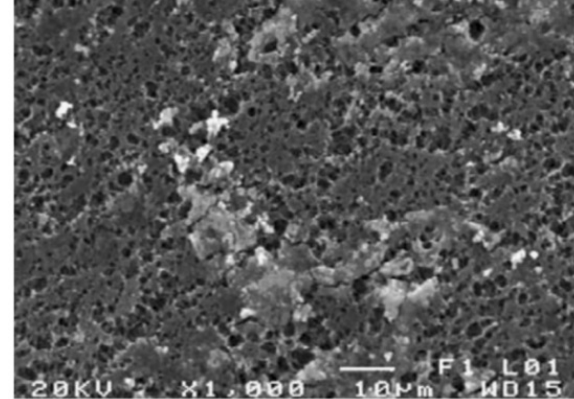
Fouling Types in MD

Inorganic scale



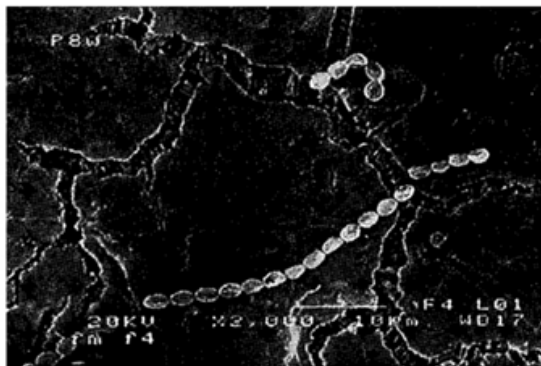
CaSO₄

Particulate fouling



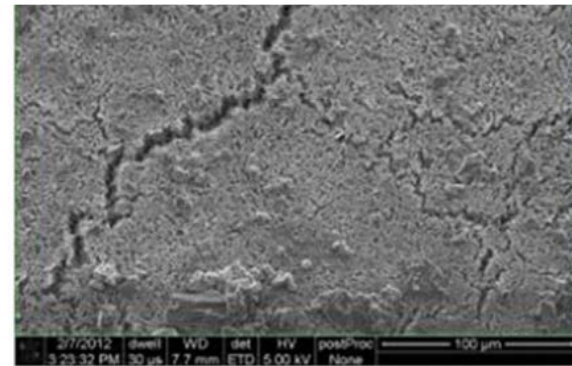
Iron Oxide

Biofouling



Streptococcus faecalis

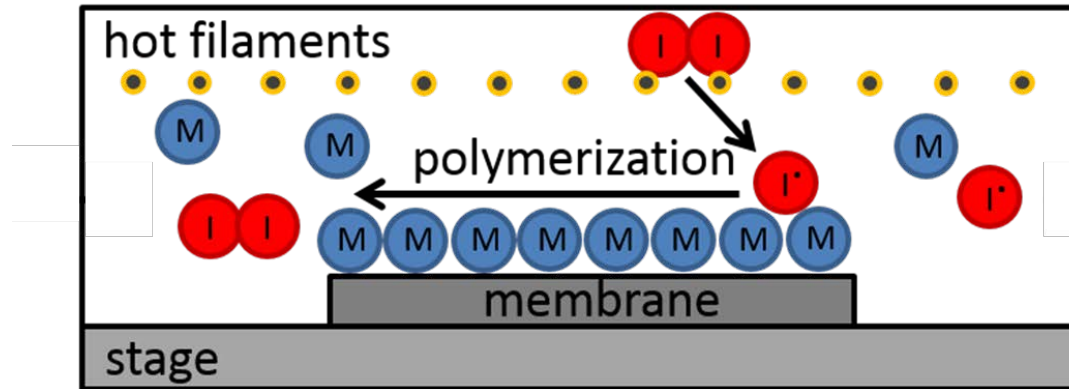
Membrane degradation



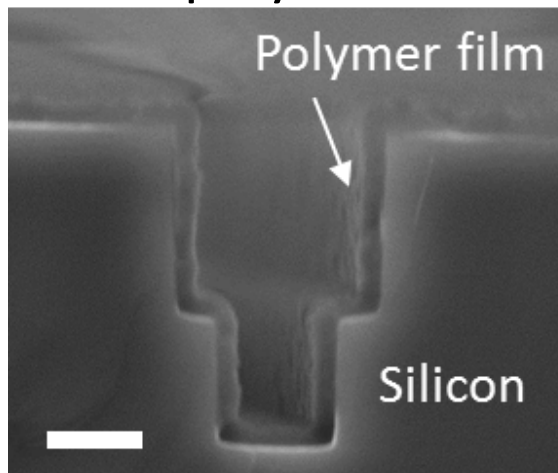
cracking from intermittent operation

Polymer thin films deposited using initiated chemical vapor deposition (iCVD)

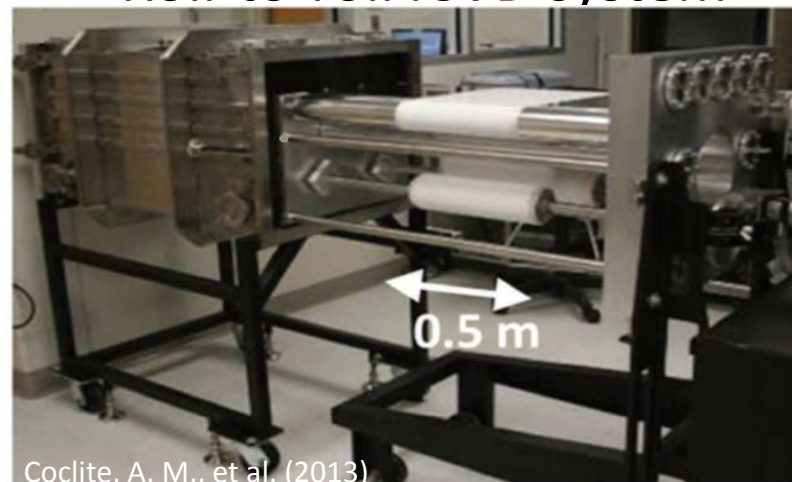
iCVD chamber



iCVD polymer film

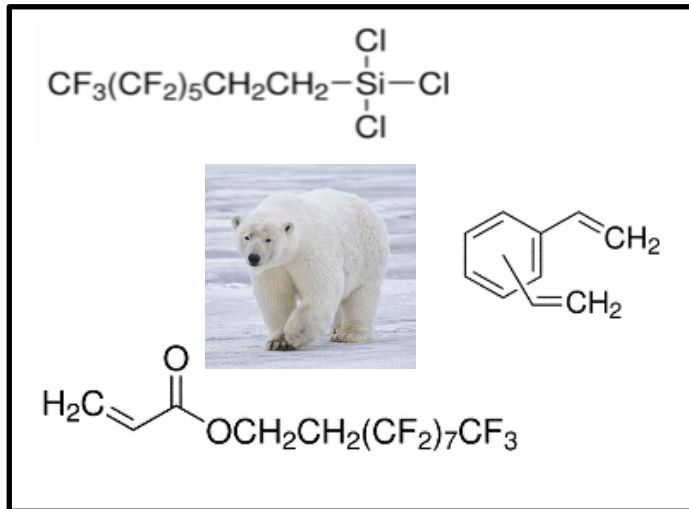


Roll-to-roll iCVD system



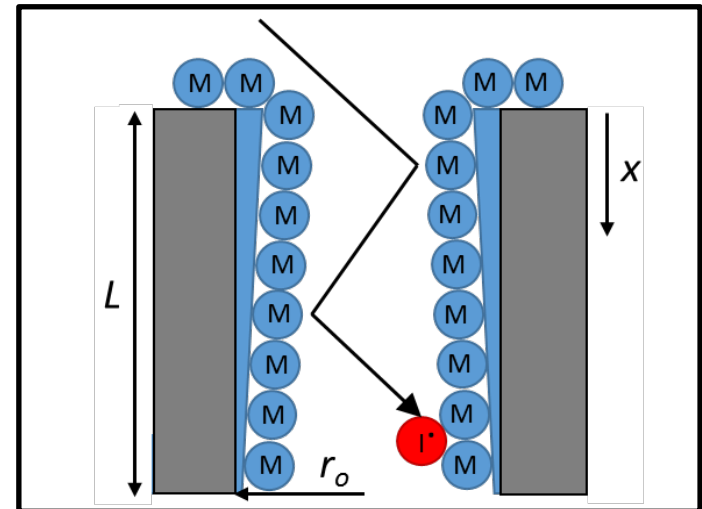
iCVD for hydrophobic membranes

iCVD parameters to optimize



1. Chemistry

- Safe?
- Hydrophobicity?
- Stability & performance



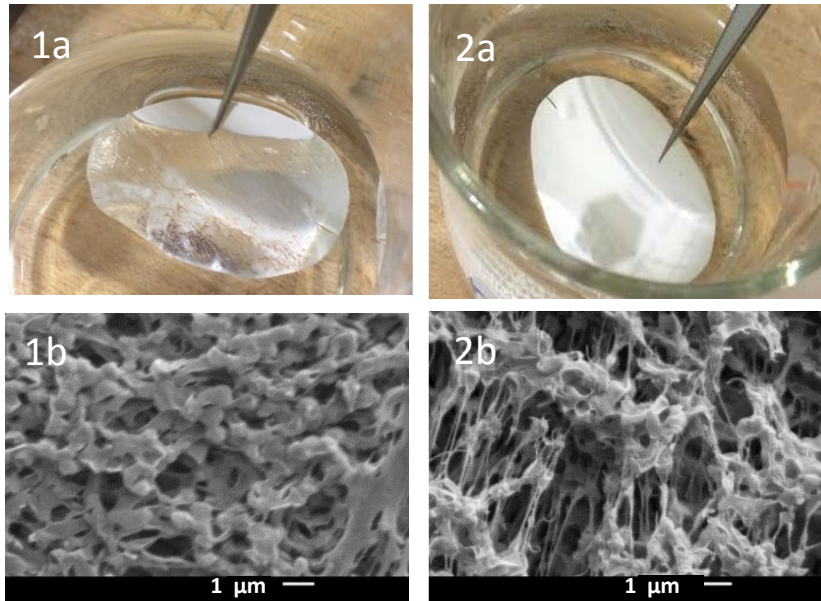
2. Thickness and conformality

- Avoids pore blocking
- Avoids gaps in surface coverage

Fouling Resistant Nanoengineered Membranes

Superhydrophobicity & Air Layers

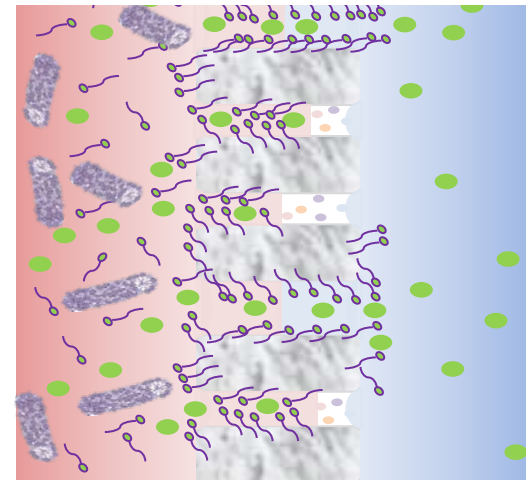
1. Superhydrophobic (157°) 2. Hydrophobic (125°)



Top: submerged superhydrophobic MD membrane, visibly shiny due to the thin air layer on its surface.

Bottom: SEM images of MD membrane surface. PVDF membrane coated with PFDA via iCVD for superhydrophobicity

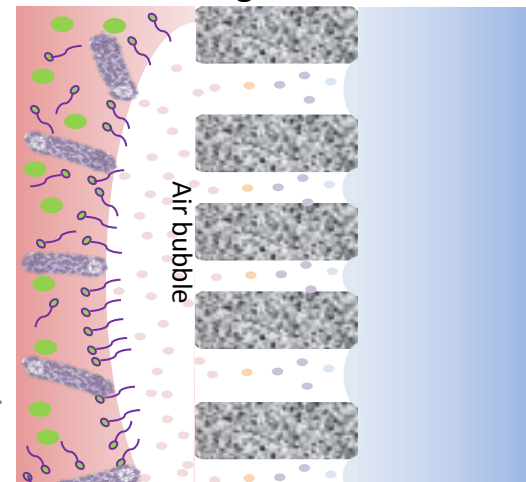
Wetting Occurrence



- Salts
- ~ Surfactants
- Micelles
- Hydrophobic Membrane



Wetting Prevention

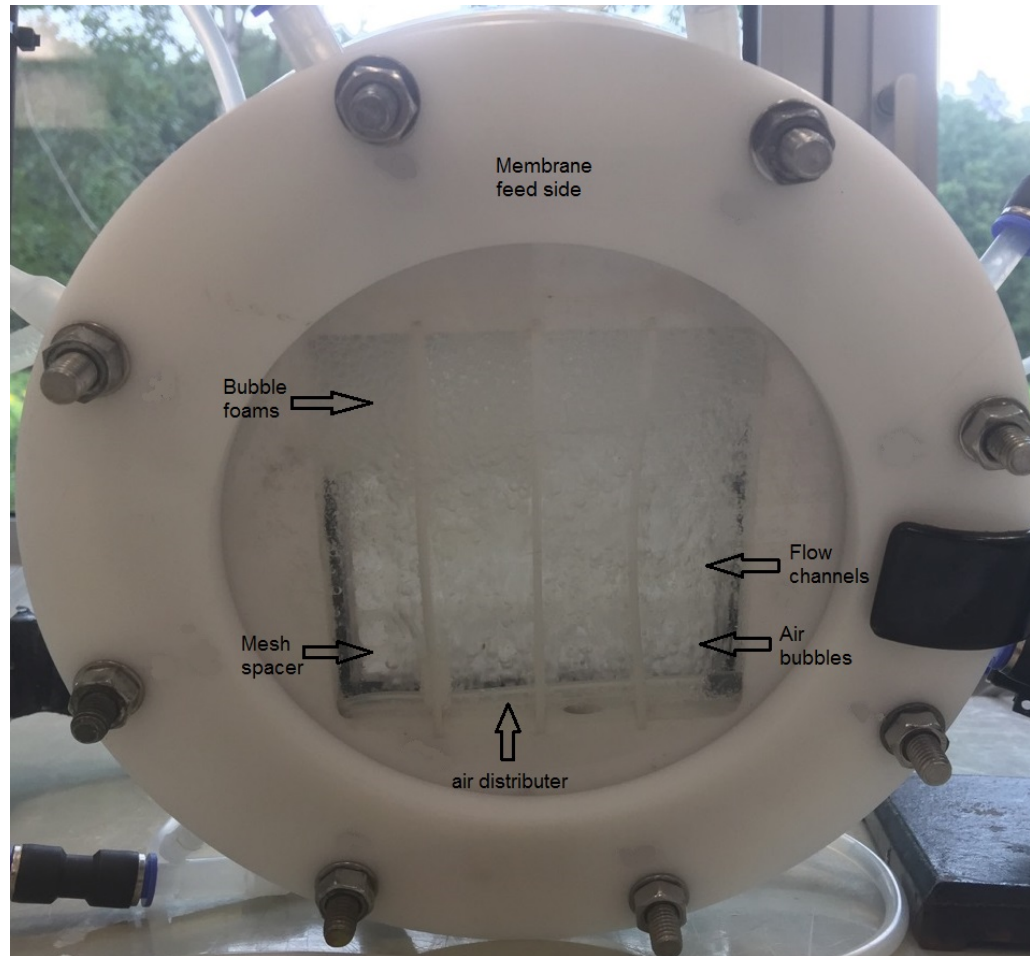


- Superhydrophobic Membrane

[6] Warsinger et al. *Journal of Membrane Science* in June 2015 **505**, 241–252 (2016).

[19] Warsinger et al. In *Proceedings of ACE15, Anaheim, CA, USA*, (2015).

[29] Warsinger et al. " *Provisional Patent Application Submitted, mit-17920pro*, 2015

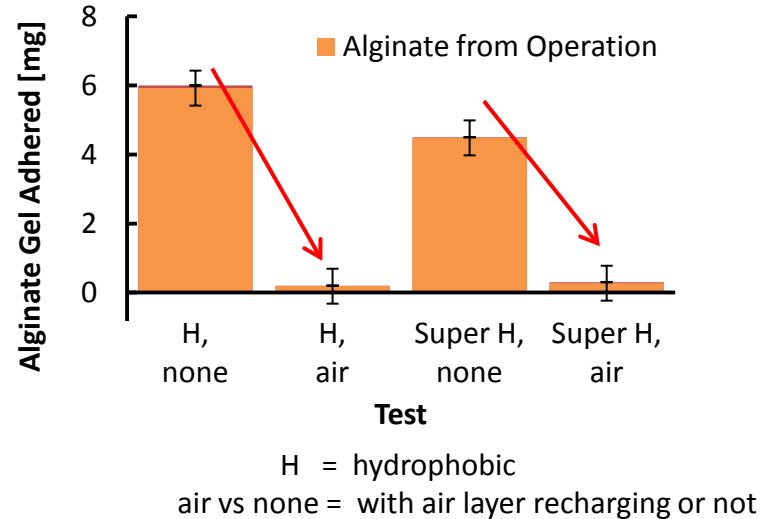
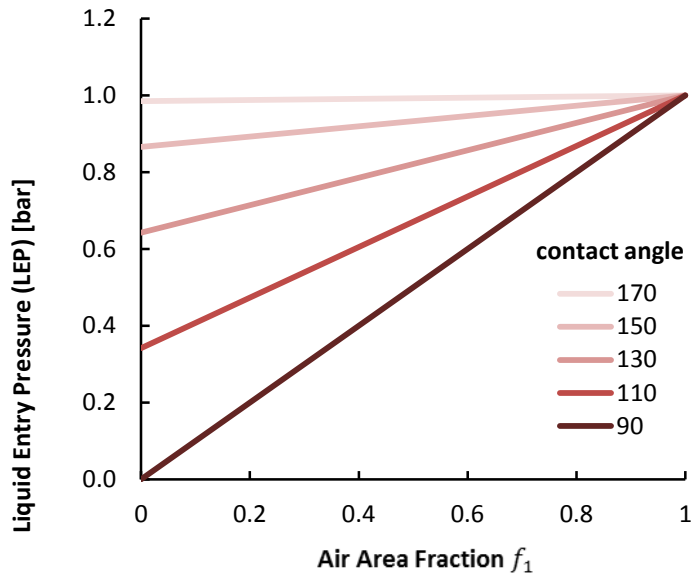


Properties of polymeric membranes

Membrane type	Manufacturer	Trade name	Polymer	Thickness (μm)	Nominal pore size (μm)	IPA bubble point (kPa)	Air flowrate (l/min/cm ² @ 0.7 bar)	Contact angle
Flat sheet	Enka	Accurel 2E-PP	PP	177	0.2	114.5	1.3	113°
Flat sheet	Donaldson	Tetratex 6532	PTFE/PES	130	0.1	200	3	153°

Fouling Resistant Nanoengineered Membranes

Superhydrophobicity & Air Layers

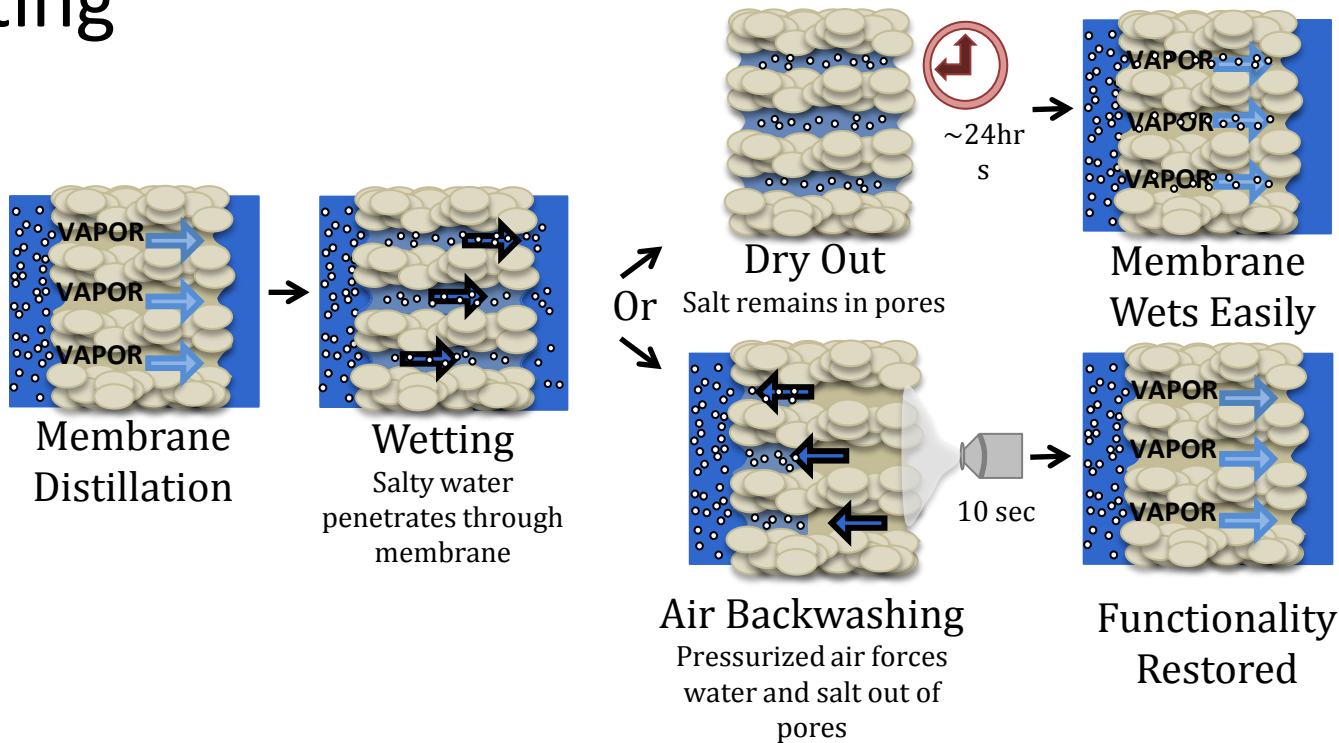


Experiment	Membrane	Feed side		Permeate side		Maximum SDS Conc. before wetting
		Air recharging	Spacer	Air recharging	Spacer	
E1 (Default 1)	PP	-	-	-	-	0.2
E2	PP	-	+	+	+	0.3
E3	PP	+	-	-	+	0.3
E4 (Default 2)	PTFE	-	-	-	-	0.4
E5	PP	+	+	-	+	0.4
E6	PTFE	+	+	-	+	0.8< (no wetting)

Fouling Resistant Nanoengineered Membranes

Superhydrophobicity & Air Layers

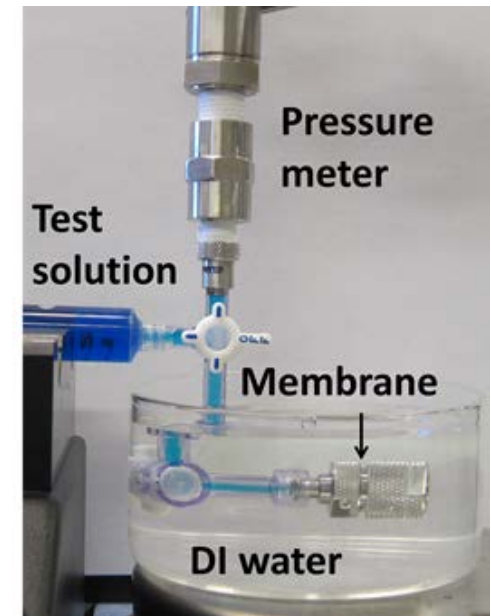
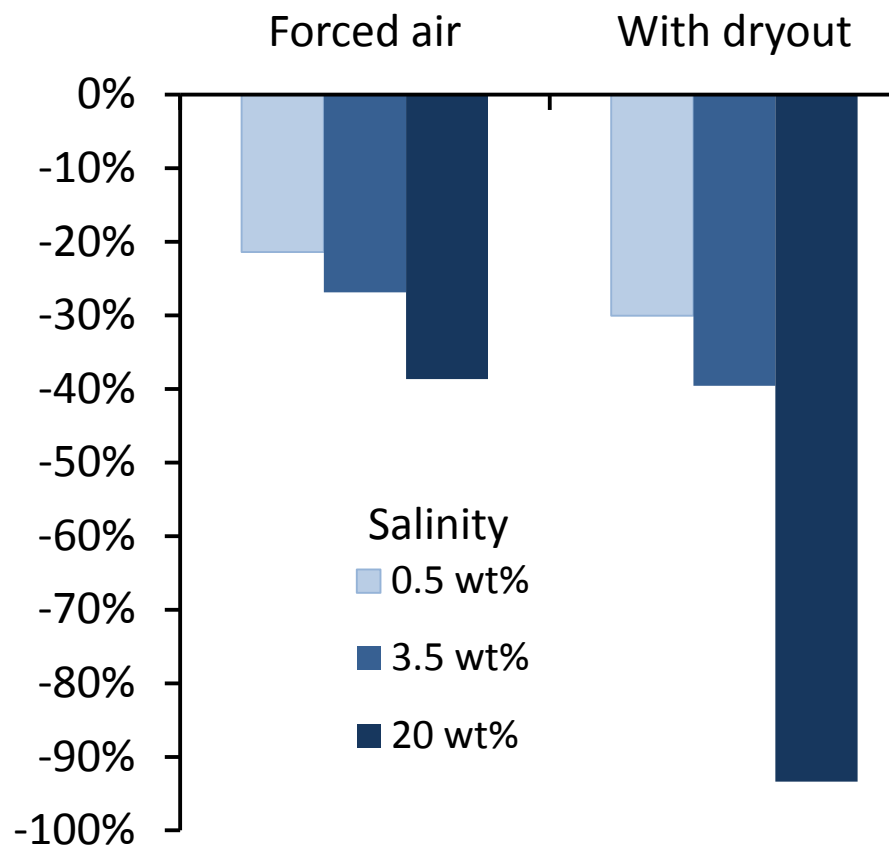
Concept: providing air at high pressure from the backside (from pure permeate) to reverse wetting

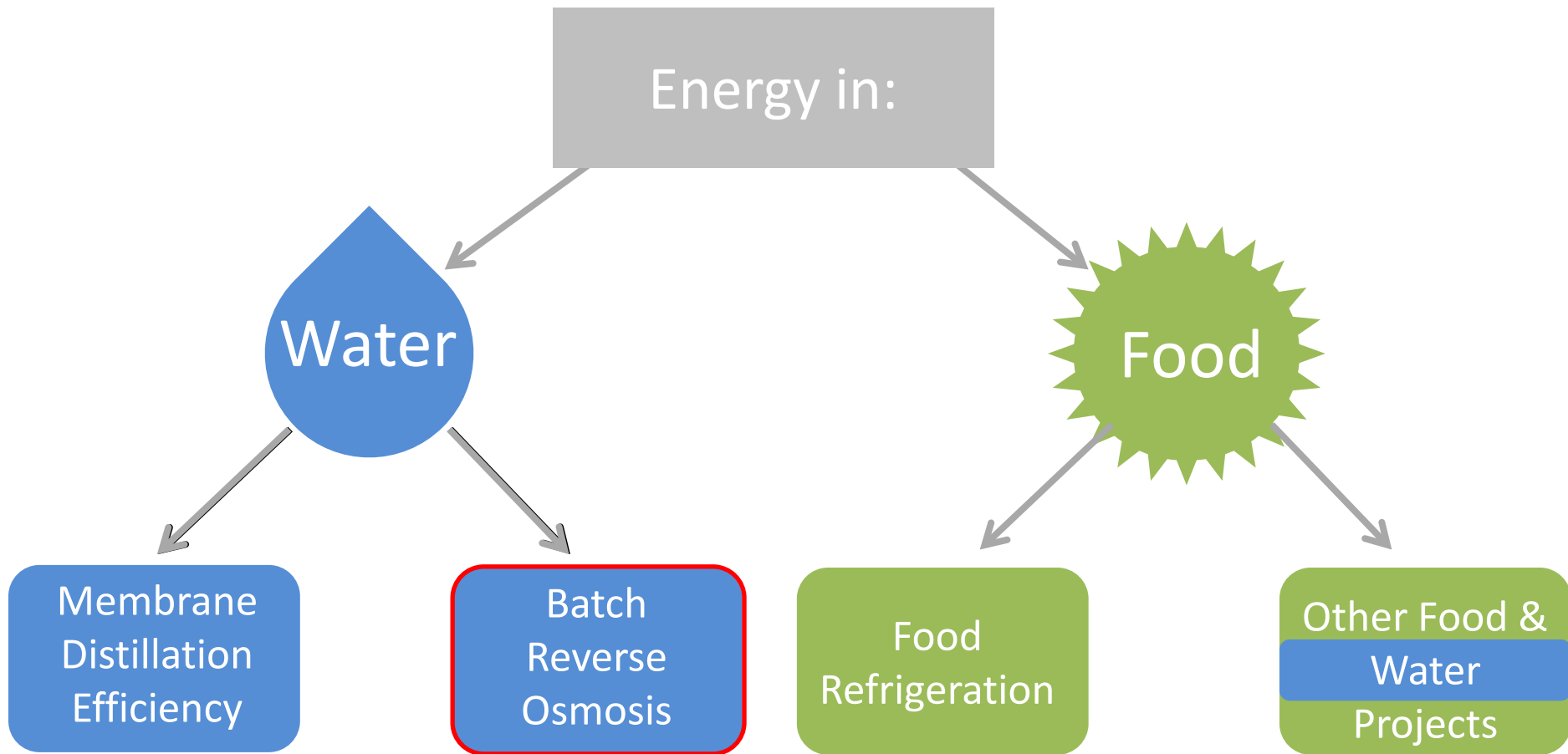


Fouling Resistant Nanoengineered Membranes

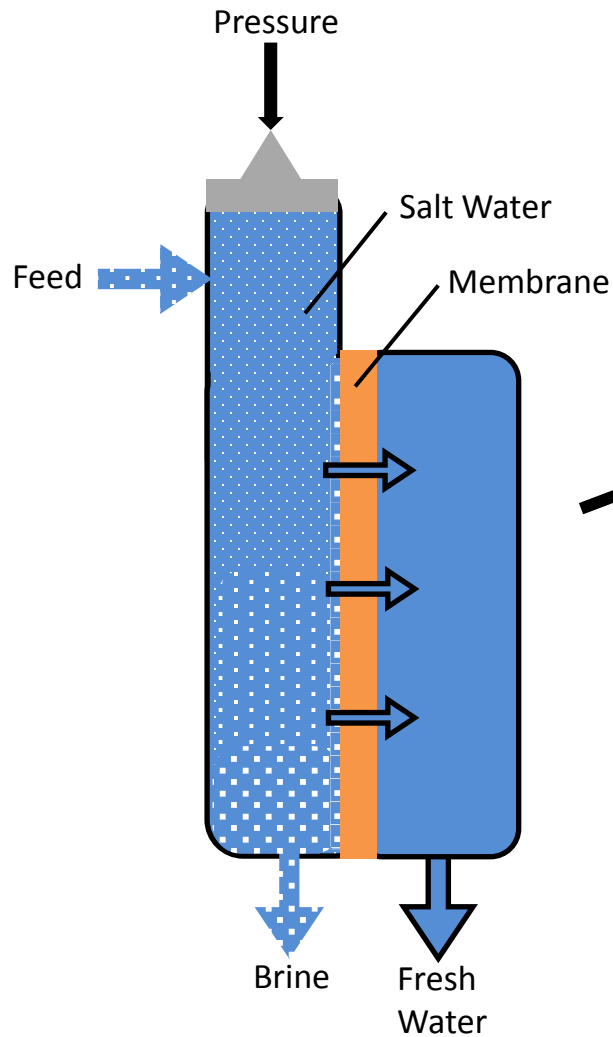
Superhydrophobicity & Air Layers

Percent Change in Liquid Entry Pressure (LEP)
after breakthrough

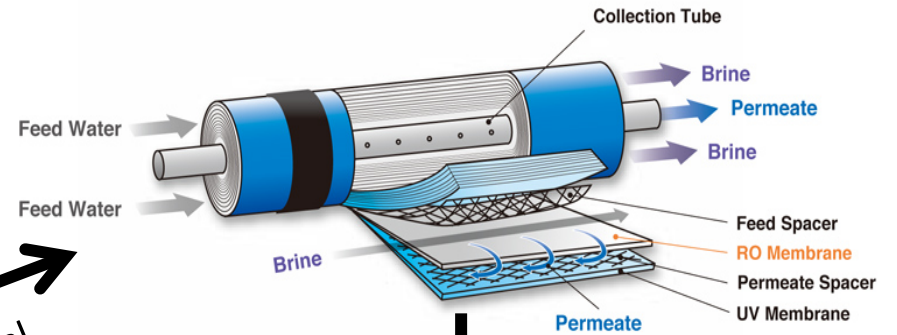




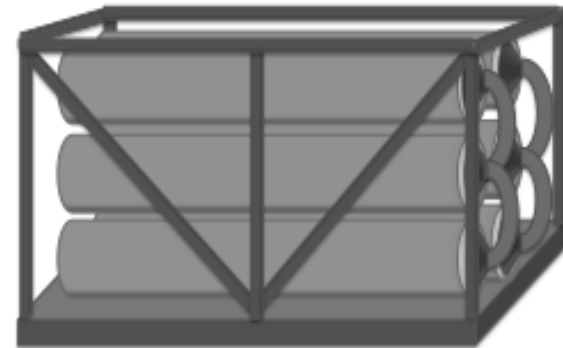
Reverse Osmosis (RO)



Kept in Spiral Wound Elements



Many elements to an RO membrane module

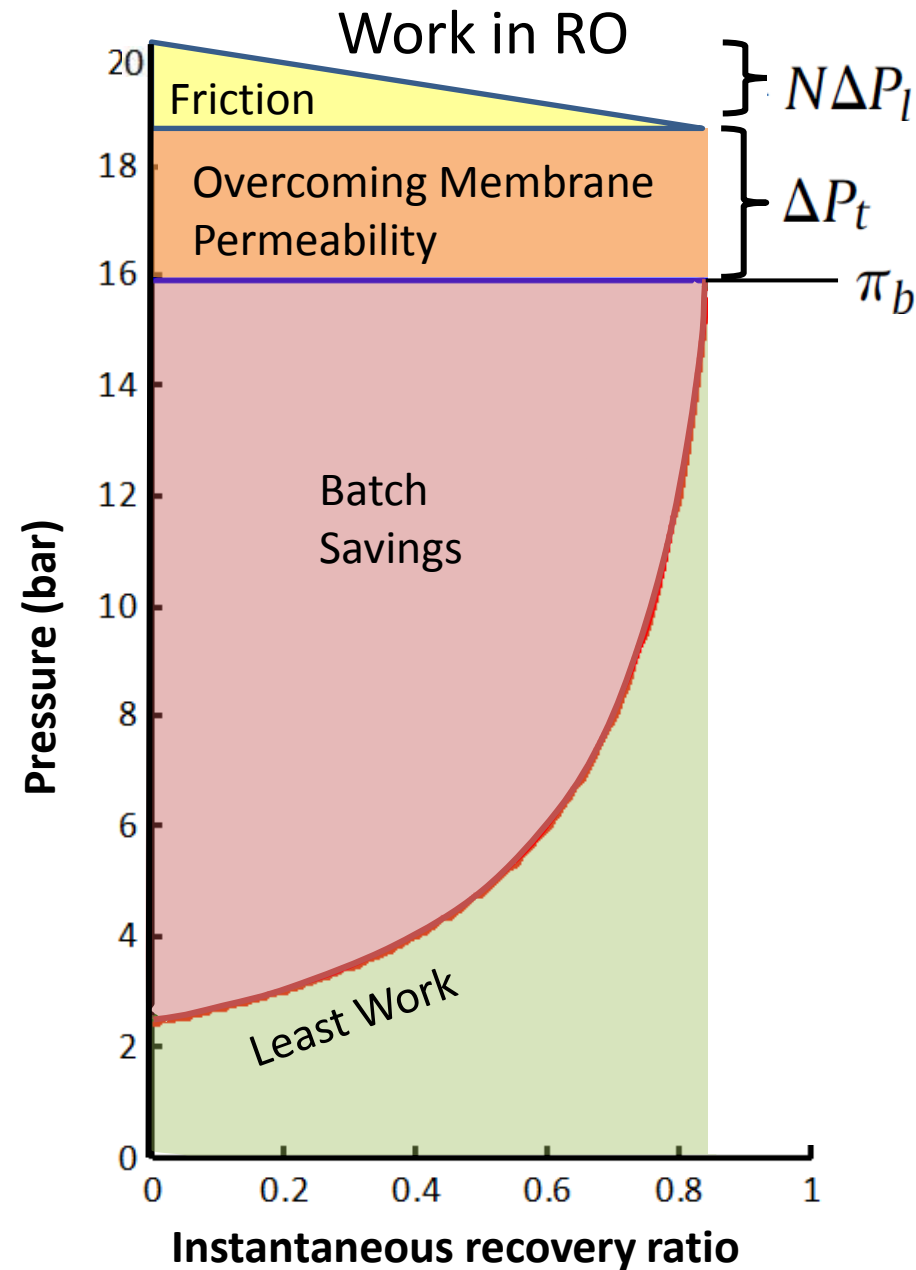


$$W_{lost} = \int \Delta P_{\text{applied-osmotic}} dV$$

RO Energy Modeling

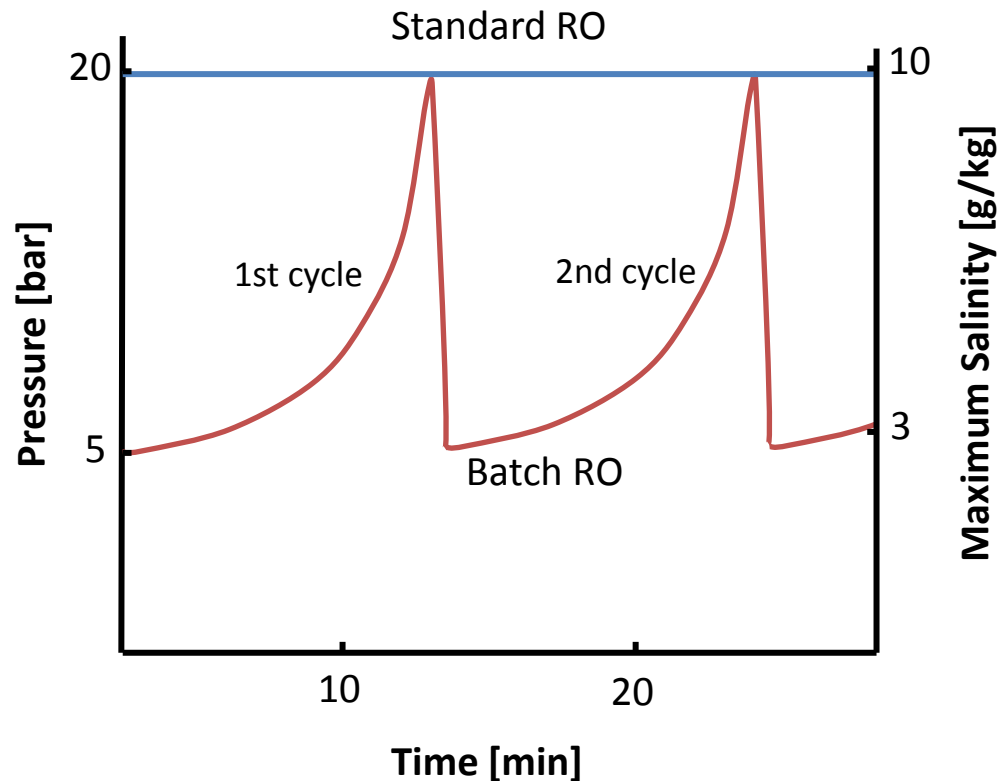
$$W_{RO} = \frac{\pi_b + \Delta P_t + N\Delta P_l}{\eta_p RR}$$

Osmotic pressure (π_b)
 Terminal Overpressure (ΔP_t)
 Viscous losses each pass ($N\Delta P_l$)
 Pump efficiency (η_p)
 Recovery Ratio (RR)

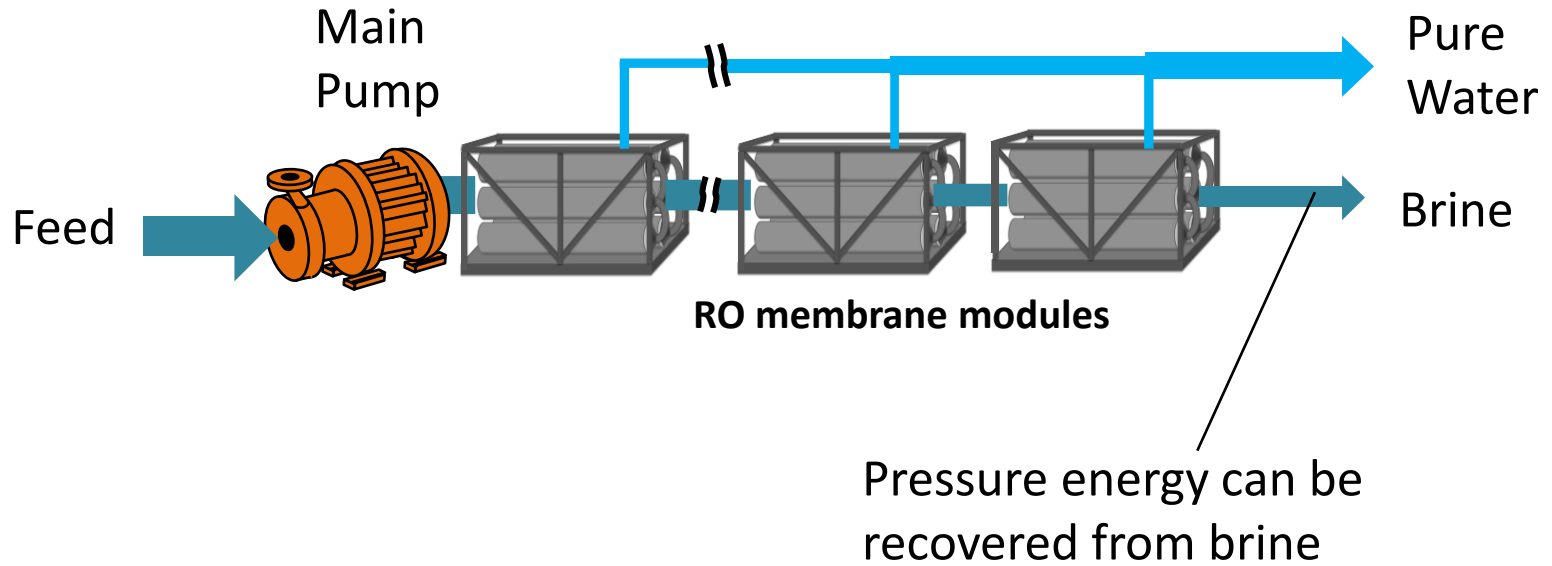


What is Batch?

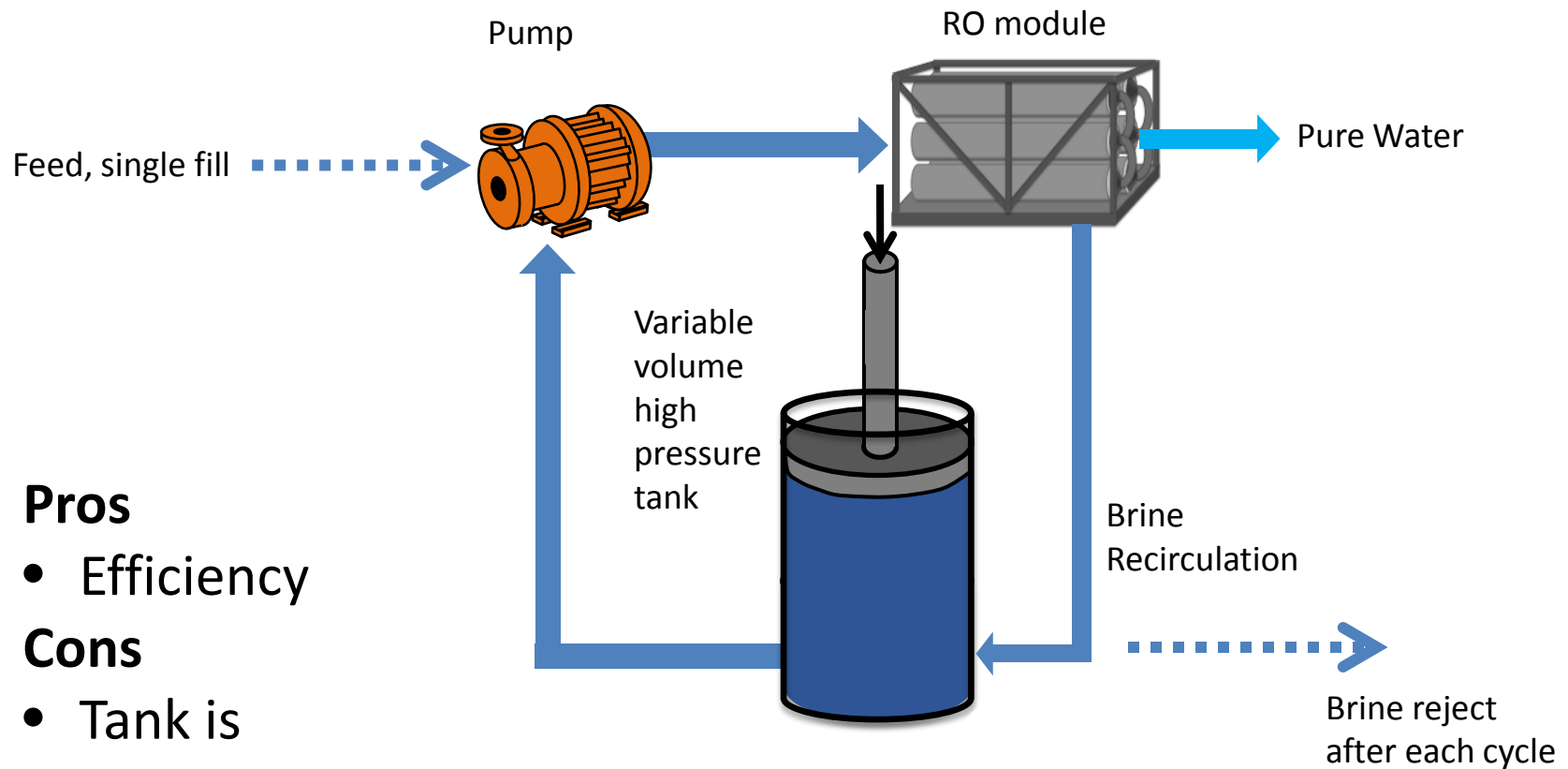
- A set volume of liquid is concentrated
- Pressure varies over time



Standard RO



Batch RO: High Pressure Tank Concept



Pros

- Efficiency

Cons

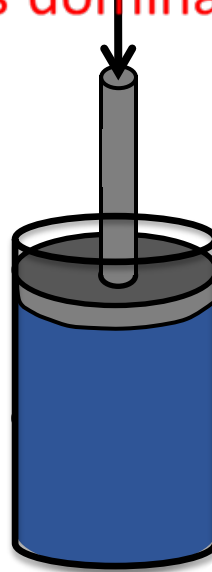
- Tank is Infeasible?

How to make a high pressure tank Batch Process?

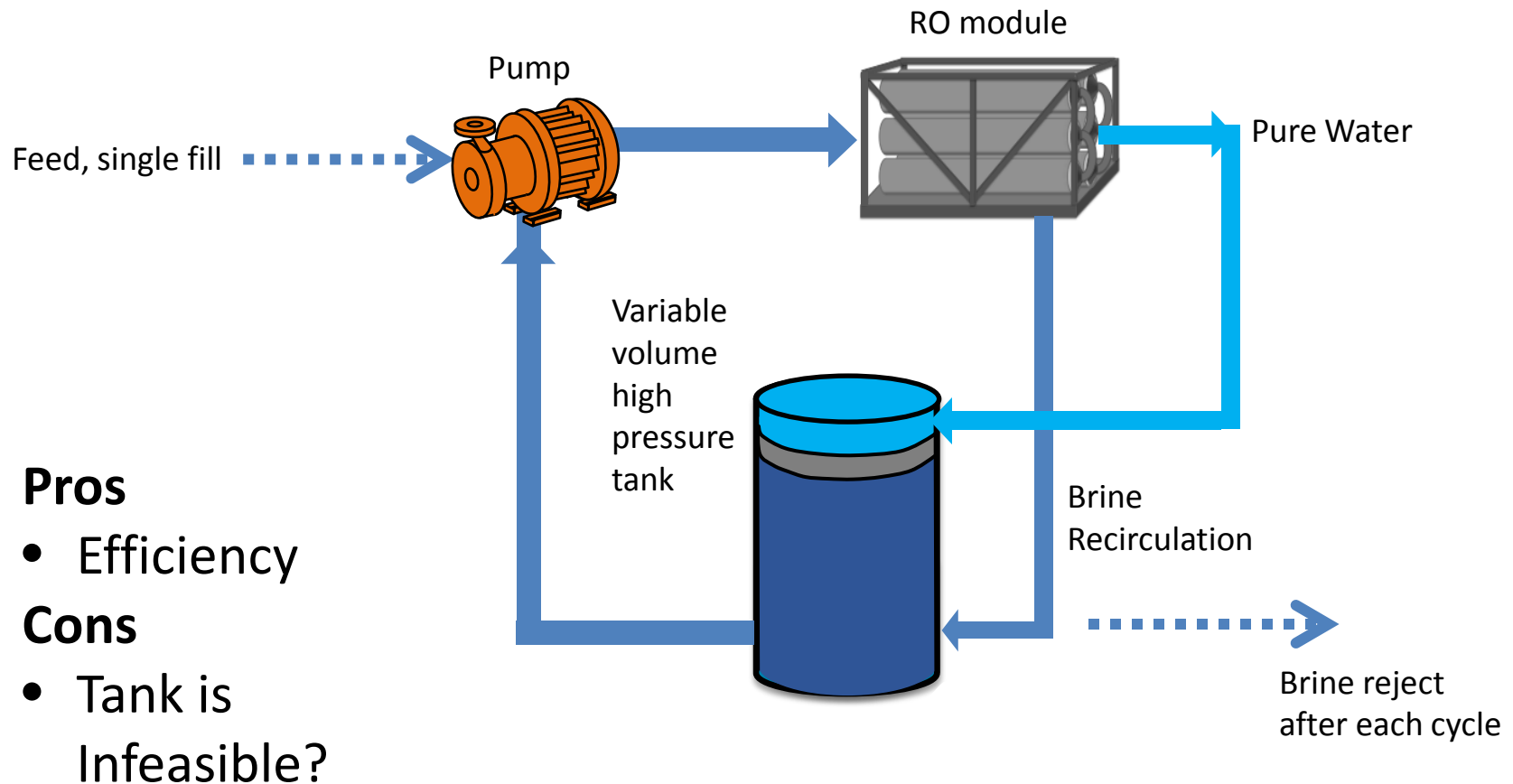
Need: simultaneously set ideal pressure while volume changes over time, done reversibly!

Idea?

- Motor? **Small inefficiencies dominate**
- Springs? **No $\frac{dP}{dt}$ control**



Batch RO: High Pressure Tank Concept



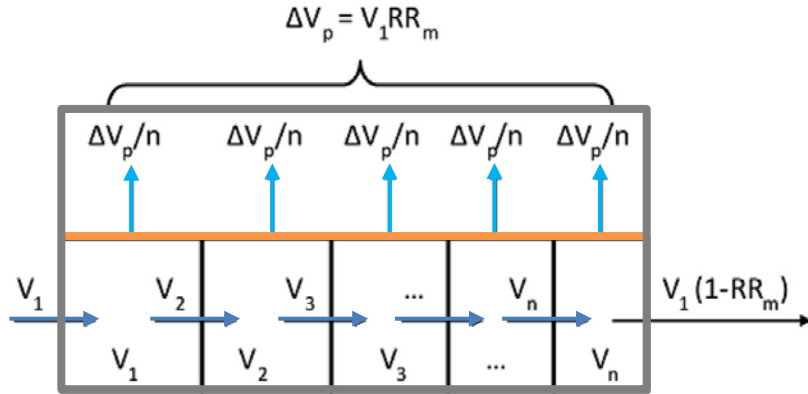
Pros

- Efficiency

Cons

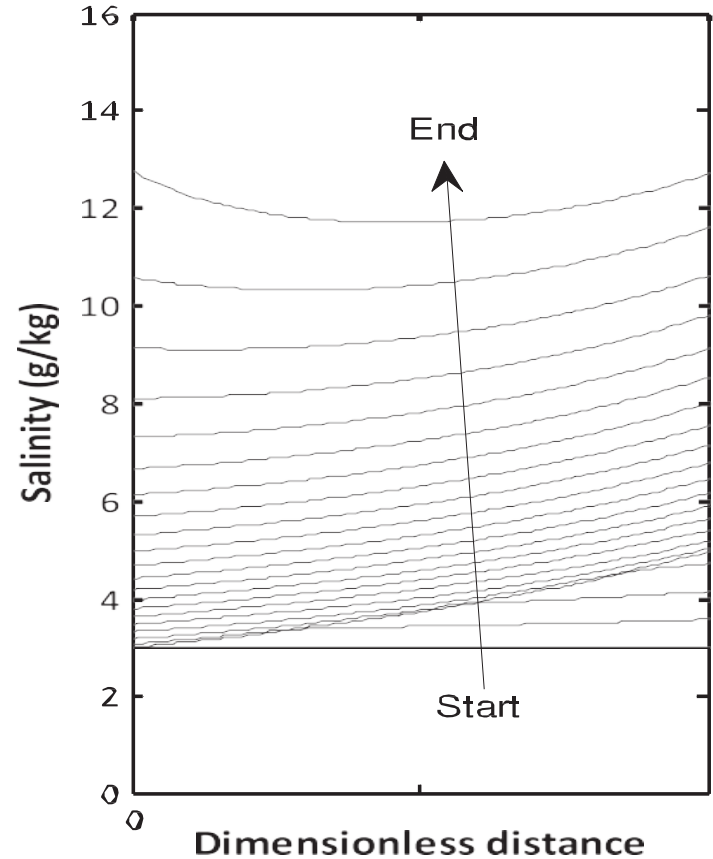
- Tank is Infeasible?

Analysis details



Volume discretization of membrane module for batch models.

The module is divided into unequal volumes, and in each step, equal amounts of permeate are removed from each section and the remaining liquid moves to the next section.



Salinity profiles in the membrane module as recovery increases during each cycle for the batch process with 3 ppt at 75% recovery.

Dimensionless distance (The abscissa) is defined as the fraction of the module recovery achieved as the fluid traverses the module (equivalently, i/n). Lines are equally spaced by permeate production; arrows indicate the direction of cycle progression.

$$W_{\text{batch,HP}} =$$

high pressure permeate pump work

$$\frac{\Delta V_p \sum_{j=1}^{V_p/\Delta V_p} (\pi_{n,j} + \Delta P_t)}{V_p \eta_p}$$

circulation pump work

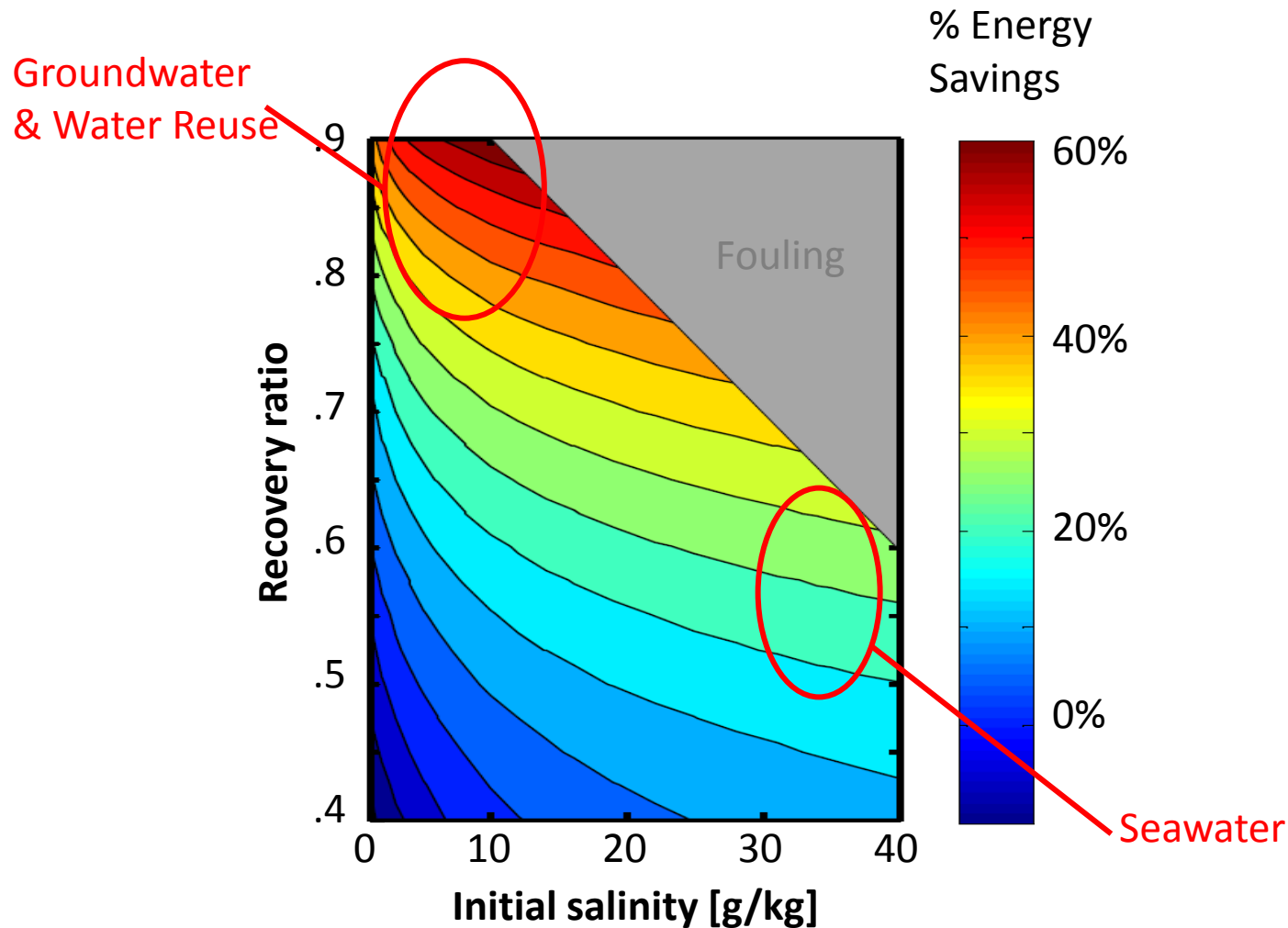
$$+ \frac{\Delta P_l}{\eta_c RR_m}$$

brine ejection

$$+ \frac{1 - RR}{RR} \frac{\Delta P_l}{\eta_c}$$

Which is discretized across the membrane module for spatial effects, and also calculated over time

Batch Improvement



Percent reduction in energy requirements of batch RO systems compared to continuous, single-stage RO with pressure recovery.

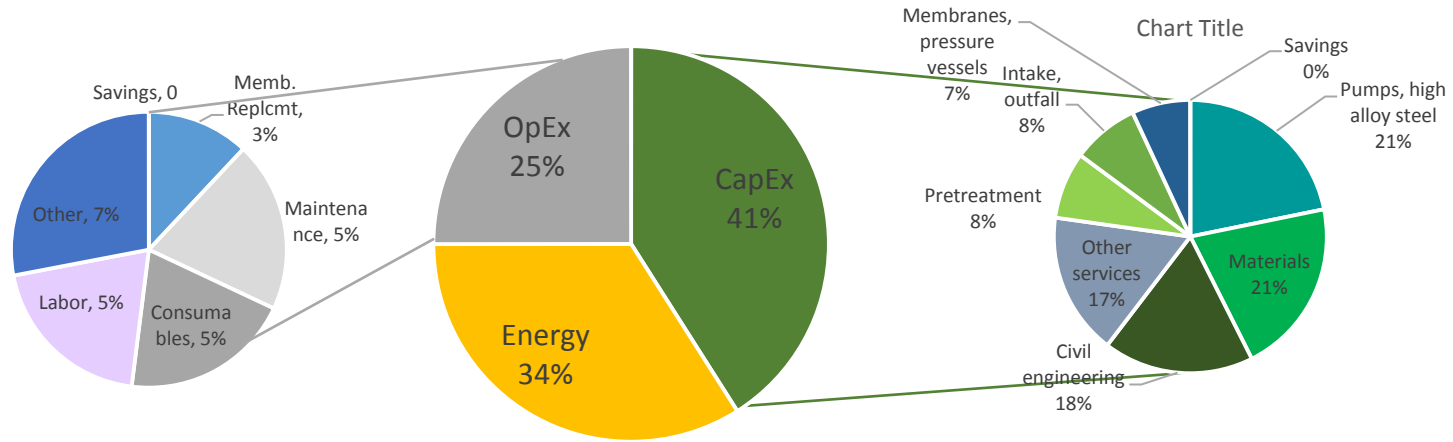
Applications

- **Large-scale desalination**
- **Agricultural water** use: more efficient, cheaper, water savings
- **Household disinfection** for India etc. 70% water savings
- **Mining Water** treatment

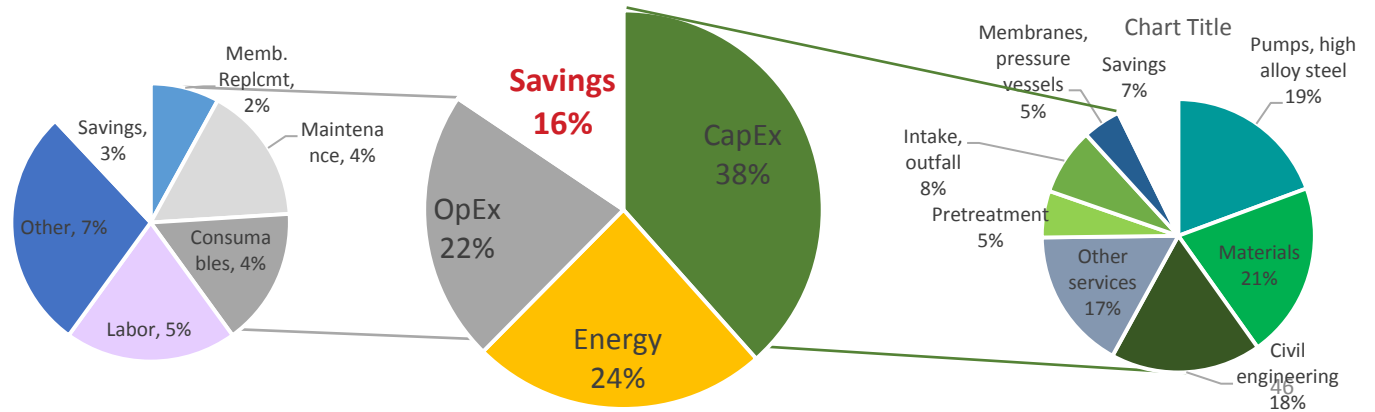


Batch Cost Savings

Current RO costs



Batch RO costs (estimate)



Batch RO in the News

WATER DESALINATION REPORT

The international weekly for desalination and advanced water treatment since 1965

Volume 52, Number 41

31 October 2016



Fort Irwin Water Plant nears completion

hardness to less than 1 mg/L as CaCO₃, before it undergoes crystallization in a 40 gpm (2.52 L/s) Encon forced circulation evaporator with mechanical vapor compression (MVC).

Initially, the RO permeate and evaporator distillate are returned to the head of the plant; however, upon California Department of Public Health approval, both flows will be blended with the EDR product water.

The non-recoverable portion of the RO concentrate, spent regenerant, crystallizer blowdown, lime sludge and CIP wastes are discharged to the eight active, and one standby, solar evaporation ponds. The ponds have an average water depth of 16 inches (41cm) and a combined surface area of 6.74 acres (2.7ha). It is anticipated that a pond will be removed from service once every eight years for cleaning, with the solids hauled to a landfill for disposal.

process, this was not an absolute energy minimum for RO desalination, adding, "It may be that better designs can move us even closer to the true thermodynamic limit."

WDR has reviewed two recently accepted Journal papers in which researchers have evaluated several RO configurations as they consider various strategies of approaching greater energy efficiency.

The first paper is entitled "Energy efficiency of batch and semi-batch reverse osmosis desalination" by MIT's David Warsinger, Emily Tow, Kishor Nayyar, Laith Maswadeh and John Lienhard V. The paper was published in Elsevier's *Water Research* journal online on 25 September. The second paper is entitled "Can batch or semi-batch processes save energy in reverse-osmosis desalination?" by Yale University's Jay Werber, Akshay Deshmukh and Menachem Elimelech. It is scheduled for January 2017 publication in *Desalination*.

The semi-batch process referred to in both papers is Desalitech's Closed Circuit Desalination (CCD) process, which recirculates pressurized concentrate until a desired recovery level is achieved. The concentrate is then displaced from the system with new feedwater without interrupting the feed or permeate flows.

Both papers also analyzed pressure exchanger batch ROs, agreeing that batch processes may be "the least energy possible RO processes," while acknowledging that scalable, energy-efficient batch systems have not yet been developed. Although the Yale authors consider a variable volume tank arrangement to be "relatively impractical," they believe it to be "ideal from an energetics perspective".



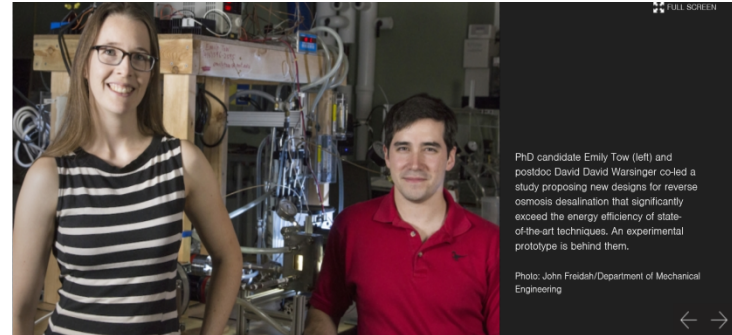
TECH IDOL

BIOGRAPHY

Dr. David Warsinger completed his B.S. and M.Eng at Cornell, and his PhD in Mechanical Engineering at MIT. He completed his graduate studies in a combined 3 years. David's research focuses on the water-energy nexus, with approaches from thermofluids and nanoengineering. Currently, David is a PostDoc at MIT and beginning a joint PostDoc at Harvard. Prior to starting his PhD, David worked at the engineering consulting firm Arup, where he performed energy and sustainability analysis and designed heating and cooling systems. David is a coauthor of 22 published and 6 submitted journal or conference papers, and a co-inventor on 13 filed or awarded patents. He is also involved with entrepreneurial endeavors, including demonstrating batch reverse osmosis with MIT startup Sandymount, and cofounding Coolify, a startup providing cold storage for farmers in developing economies. Notable awards David has earned include the national dissertation award from UCOWR, the highest GPA award for his masters, and the MIT Institute Award for Best Research Mentor for Undergraduate Students.

BACK TO SPEAKERS

DAVID WARSINGER
Researcher, Lienhard Research
Group, MIT



PHD candidate Emily Tow (left) and postdoc David David Warsinger co-lead a study proposing new designs for reverse osmosis desalination that significantly exceed the energy efficiency of state-of-the-art techniques. An experimental prototype is behind them.

Photo: John Freidsh (Department of Mechanical Engineering)

Batch desalination configuration bests standard reverse osmosis approach

Researchers develop a new way to create more clean water with less energy, thanks to clever timing.

School of Engineering
November 18, 2016

Press Inquiries

RELATED

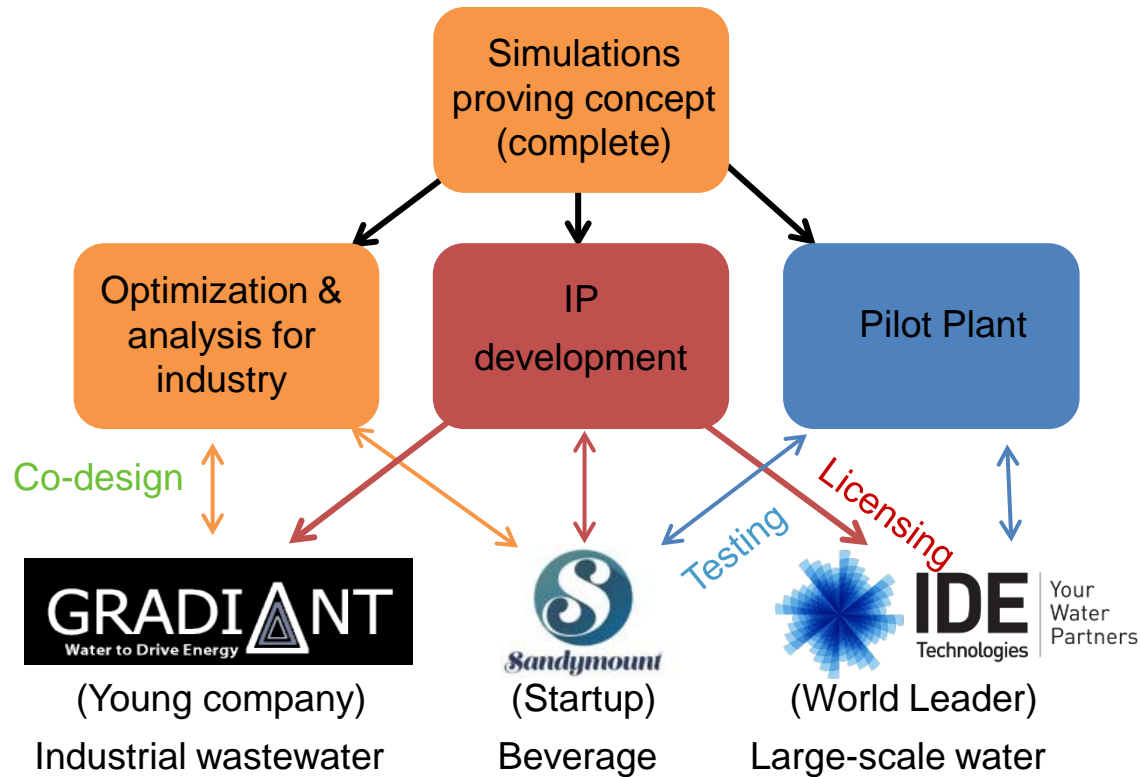
With water scarcity affecting nearly 2 billion people — many of whom live near the oceans — "water, water everywhere and not a drop to drink" has become a common cry for more than just wayward sailors. Desalination through reverse osmosis (RO) has long offered one solution to help meet global water needs in the face of population growth, development, and climate change. However, removing salt from water is energy-intensive.

A team of MIT researchers has responded by creating new designs for reverse osmosis

- Paper: "Energy efficiency of batch and semi-batch (CCRO) reverse osmosis desalination"
- Rohsenow Kendall Heat Transfer Lab

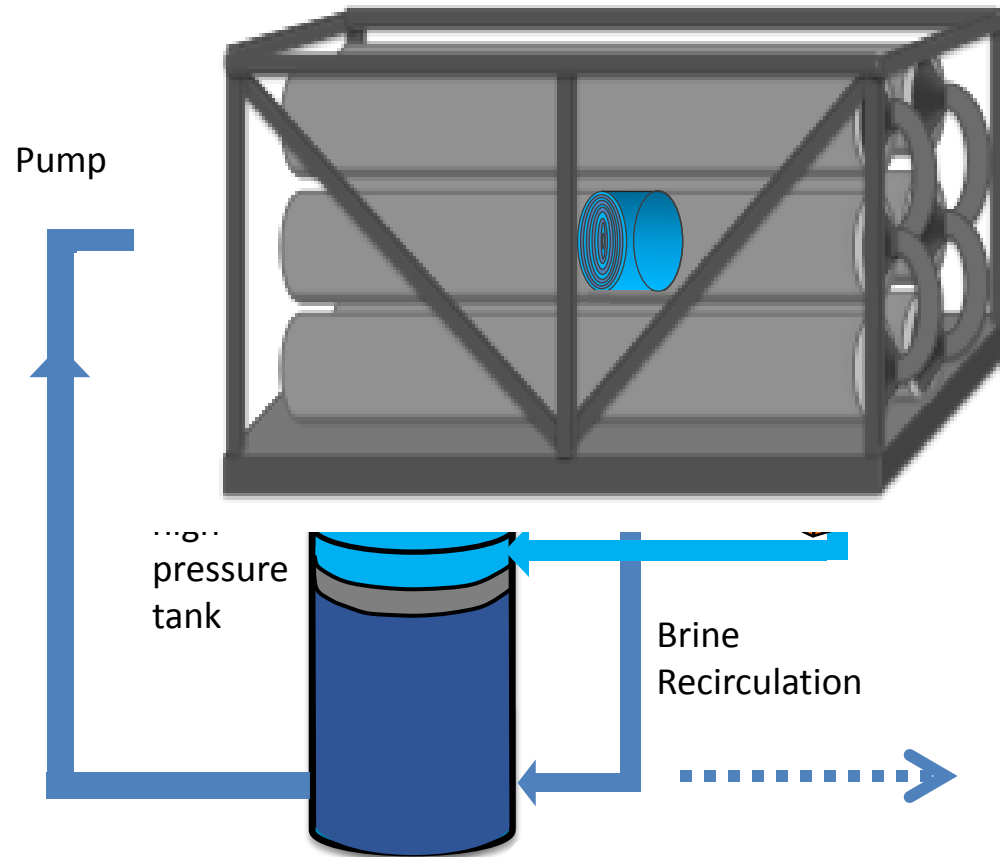


Commercialization Strategy



Commercialization and additional funding implementation plan of batch desalination research

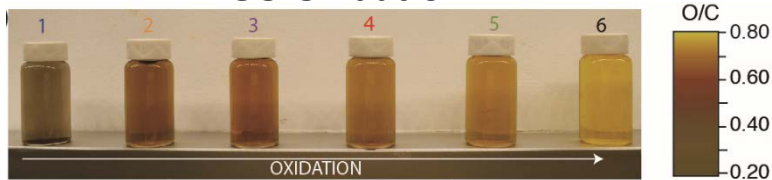
Can we get big benefits too from improving not just the process, but its nanomaterials?



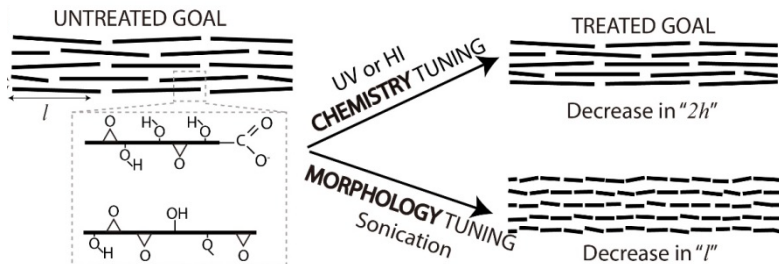
Ultrapermeable RO Membranes: Graphene Oxide (GO)

- Reduces membrane area (\$\downarrow\$)
- Energy savings: less overpressure
- Potentially fouling resistant
- Emerging contaminants (PFOA)

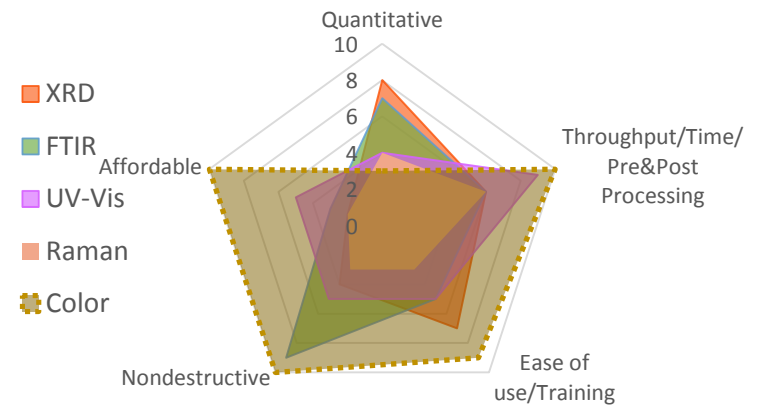
GO Oxidation



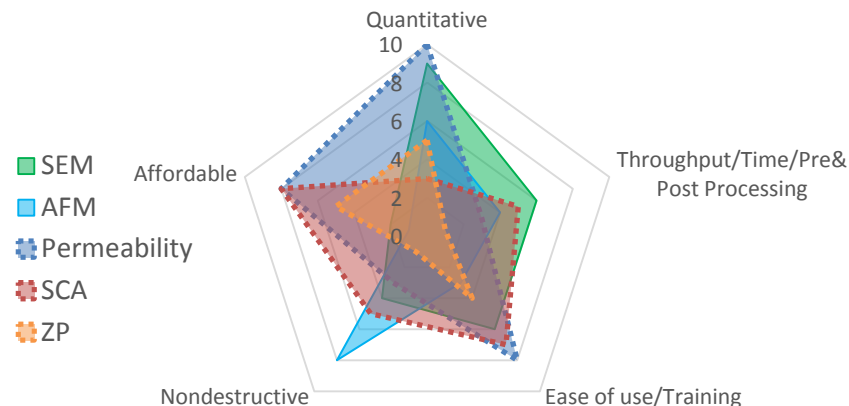
GO Membrane Fabrication



CHEMISTRY

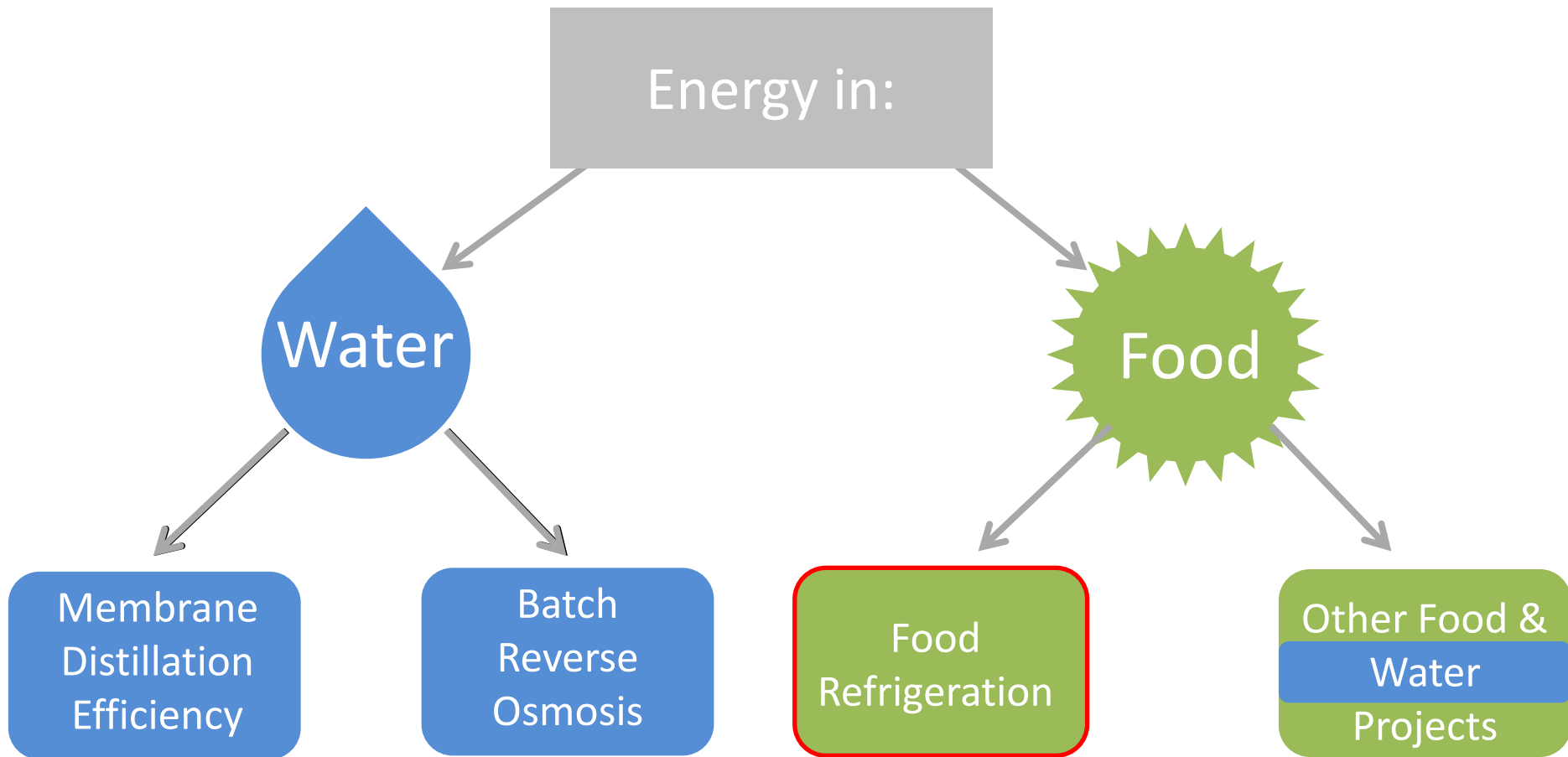


MORPHOLOGY



D. M. Warsinger et al. (in progress)

C. Amandei D. M. Warsinger et al. (in progress)



Energy and thermofluids strategies for intermittent power

Visualizing Water Stress

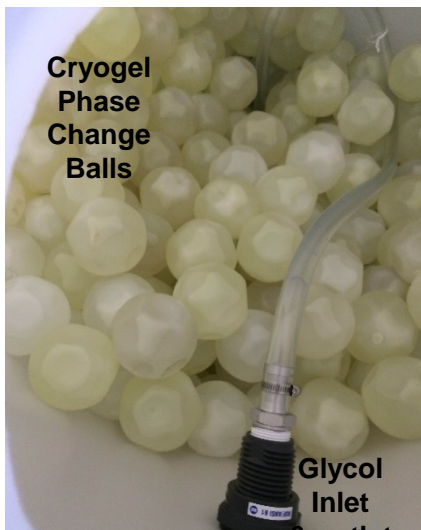
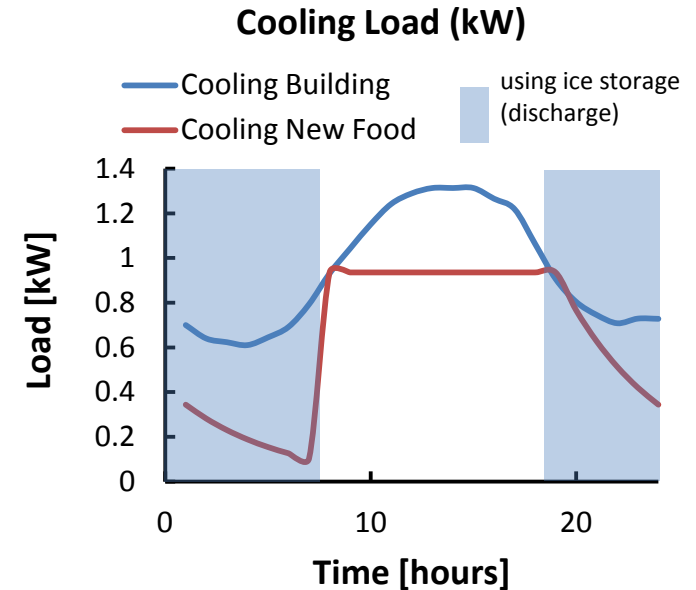
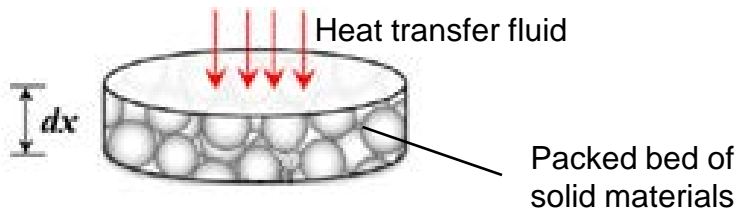


Coolify®

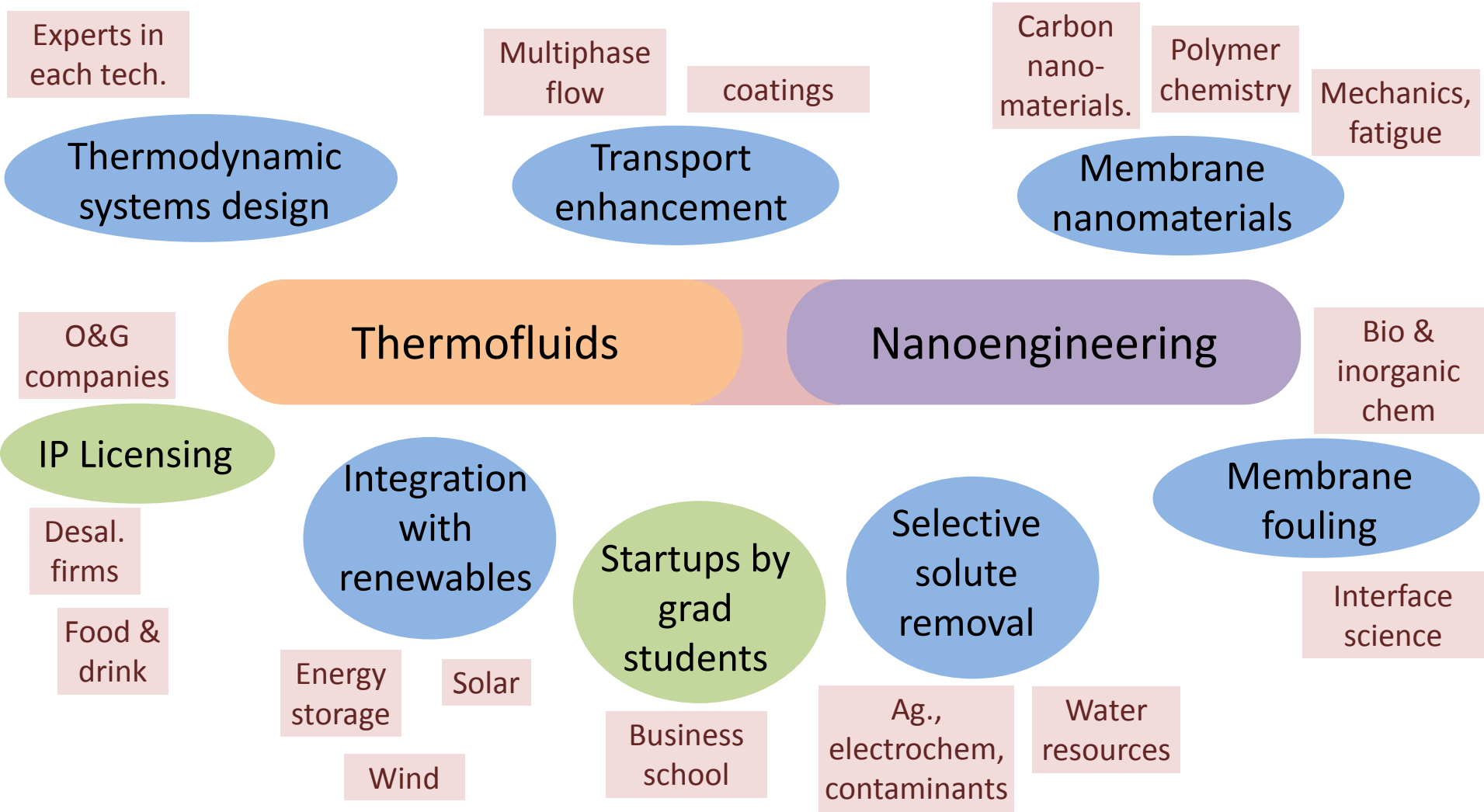


Phase-change thermal storage

- Freezing packed-bed heat transfer
- Thermodynamic system design
- Phase change materials



Vision & Collaboration



Energy-Water Nexus Funding Ecosystem

Federal

- >\$627,000 raised in grant applications and pitch competitions in last 2.5 years
- ~\$1 million in high school submissions



University



Institutions



Foreign Gov



Industry



Funding sources used so far

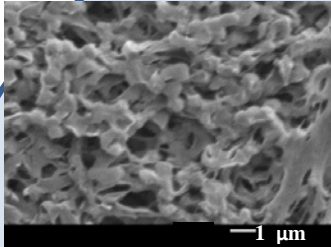
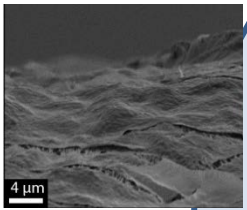
Future funding sources



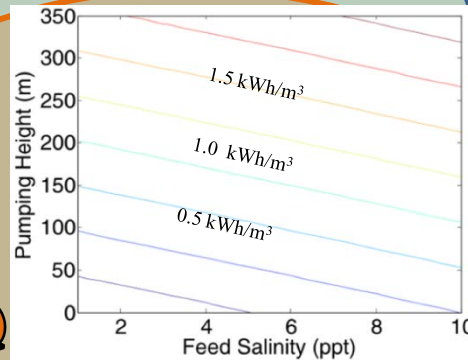
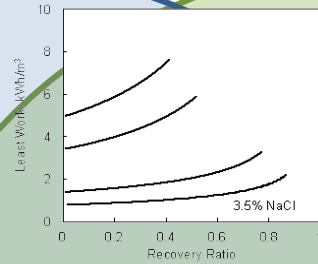
Water-Energy-Food Nexus

Water

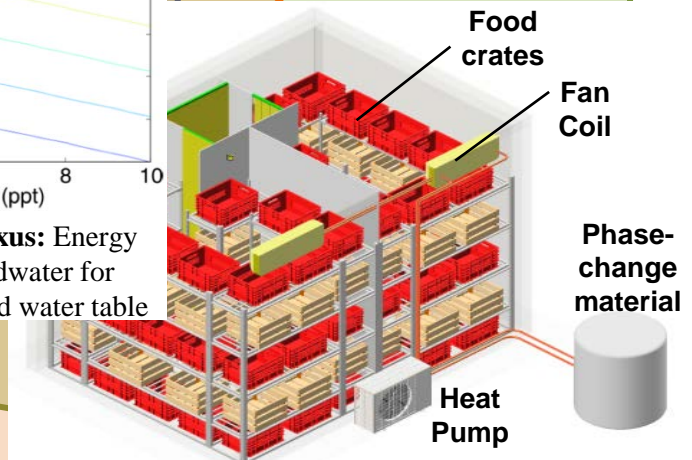
Food



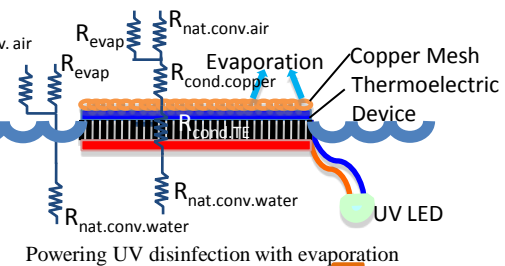
SEM of super-hydrophobic MD membrane created with iCVD of PPFDA on PVDF [24]



Water-Food-Energy Nexus: Energy use of desalinating groundwater for agriculture, by salinity and water table depth²⁶



Coolify refrigeration unit with Phase-Change thermal storage



Powering UV disinfection with evaporation

Energy

Acknowledgements

MASDAR INSTITUTE
OF SCIENCE AND TECHNOLOGY



MIT Technology
Licensing
Office



Abdul Latif Jameel
World Water and Food Security Lab



DESHPANDE CENTER
FOR TECHNOLOGICAL INNOVATION

TATA CENTER
TECHNOLOGY
+ DESIGN



powered by **40**
FORTY CHANCES



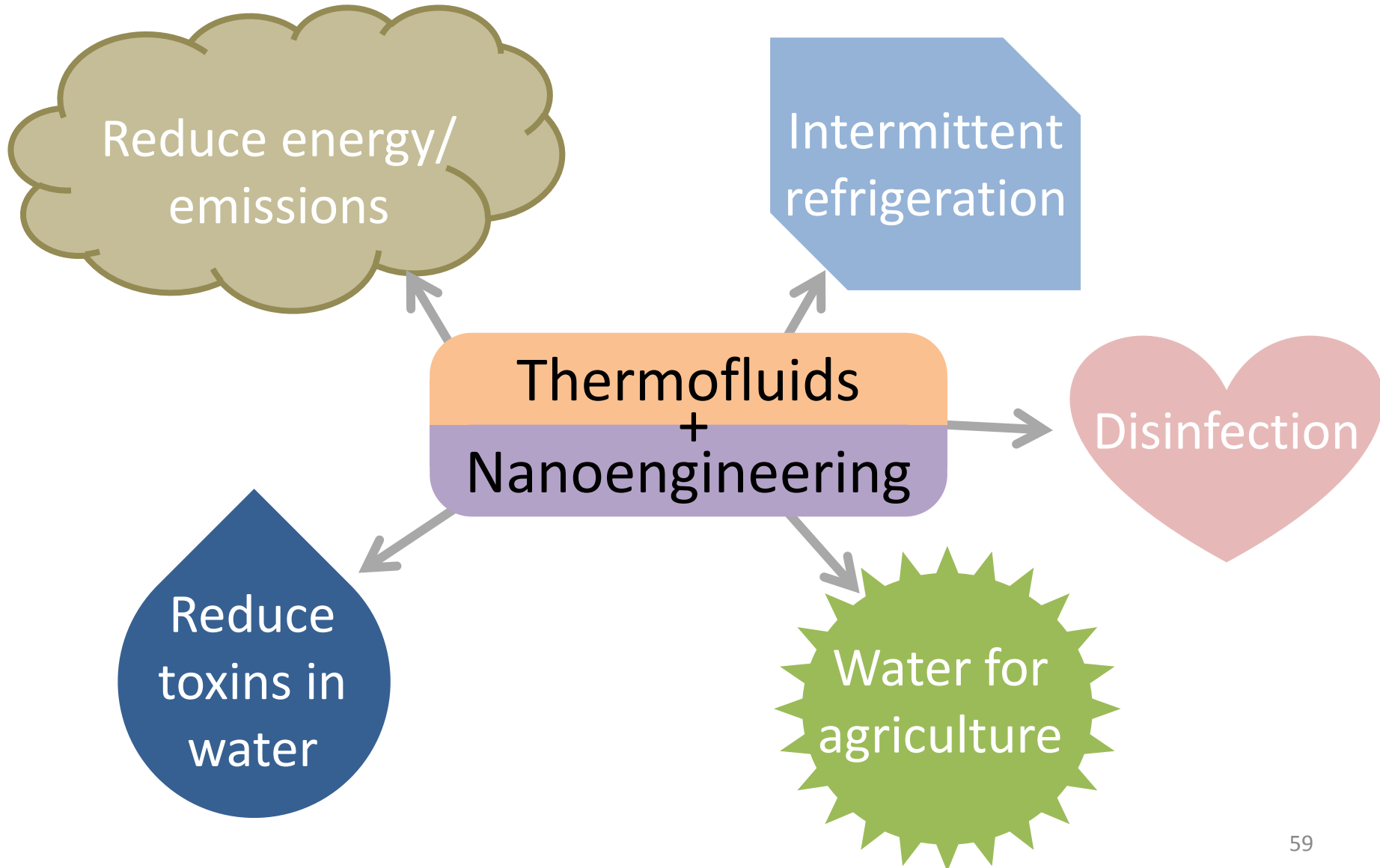
Lab



Undergrad + Grad Team



Can we save lives with thermodynamics?



Questions?



Feed Modeling

$$Nu = \frac{(f/8) \cdot (Re - 1000) \cdot Pr}{1 + 12.7 \cdot (f/8)^{1/2} \cdot (Pr^{2/3} - 1)}$$

Main Flux eqn

$$J_i = B \cdot (P_{f,m,i} - P_p \cdot x_{a,m,i})$$

$$Sc_f = \frac{\mu_f}{(\rho_{feed} \cdot D_{s,w})}$$

Concentration along flow direction

$$x_{f,b,i} = S_{in} \cdot \left(\frac{m_{f,i}}{\dot{m}_{f,in}/n_{sheets}} \right)$$

$$K_{cond} = \frac{k_m \cdot (1 - \xi) + k_{air} \cdot \xi}{\delta_m}$$

Effect of concentration polarization

$$x_{f,m,i} = x_{f,b,i} \cdot \exp \left(\frac{J_i}{k_{mass} \cdot \rho_{feed}} \right)$$

..

$$P_{f,m,i} = P_{sat} (Water, T = T_{f,m,i}) \cdot \left(1 - \left(\frac{\frac{x_{f,m,i}}{MW_{solute}}}{\left(\frac{x_{f,m,i}}{MW_{solute}} \right) + \left(\frac{1000 [g/kg] - x_{f,m,i}}{MW_{water}} \right)} \right) \right)$$

$$q_{out,i} = J_i \cdot (h_{fg,f,i}) + q_{m,i} - J_i \cdot (h_{f,b,i} - h_{f,m,i})$$

Air Gap & Condensate

Diffusion Equation

$$\left(\frac{J_i}{M_{H_2O}} \right) = \frac{c_{a,i} \cdot D_{wa}}{d_{gap} - \delta_i} \cdot \ln \left(1 + \left(\frac{x_{i,i} - x_{a,m,i}}{x_{a,m,i} - 1} \right) \right)$$

$$T_{a,m,i} - T_{i,i} = \left(\frac{q_{conv,i}}{k_{mix,i}} \right) \cdot \left(\alpha_{mix,i} \cdot \frac{\rho_{mix,i}}{J_i} \right) \cdot \left(\exp \left(\frac{J_i}{\rho_{mix,i} \cdot \alpha_{mix,i}} \cdot (d_{gap} - \delta_i) \right) - 1 \right)$$

$$\nu_{f,i} = \frac{\mu(\text{Water}, P = P_p, T = T_{av,film,i})}{\rho_f}$$

Condensation film thickness

$$J_i \cdot dA = g \cdot \frac{\rho_f - \rho_g}{3 \cdot \nu_{f,i}} \cdot w \cdot (\delta_{i+1}^3 - \delta_i^3)$$

heat absorbed by condensate

$$q_{c,i} = J_i \cdot h_{fg,c,i} + q_{m,i}$$

film conduction resistance

$$q_{c,i} = \frac{k_{film,i}}{\delta_i} \cdot (T_{i,i} - T_{wall,i})$$



Cooling Channel Modeling

$$d_{h,c} = 4 \cdot \frac{w \cdot d_{cond}}{2 \cdot (w + d_{cond})}$$

BL resistance

$$T_{wall,i} = T_{c,b,i} + \left(\frac{q_{c,i} + J_i \cdot (h_{c,i,i} - h_{c,wall,i})}{h_{t,c}} \right)$$

conserve energy in bulk stream

$$h_{c,b,i+1} = h_{c,b,i} - (q_{c,i} + J_i \cdot (h_{c,i,i} - h_{c,wall,i})) \cdot \frac{dA}{\dot{m}_{f,1} + (\dot{m}_{c,ex}/1)}$$



Efficiency Definitions

Parameter

Typical Value

Definitions

J Flux

2-10 L/m²hr

$$J = \frac{\dot{m}_p}{A}$$

pure water flux (J , measured in L/m²-hr).

Where \dot{m}_p is the mass flow rate of feed,

A is the area.

GOR Energy Efficiency

1.5-15

$$\text{GOR} = \frac{\dot{m}_p h_{fg}}{\dot{Q}_f}$$

h_{fg} is the enthalpy of vaporization (2257 kJ/kg)

\dot{Q}_f is the total heat energy input.

η MD Thermal Efficiency .5-.93

$$\eta = \frac{\dot{Q}_{\text{vap}}}{\dot{Q}_{\text{vap}} + \dot{Q}_{\text{cond}}}$$

Heat transfer by conduction across the membrane (\dot{Q}_{cond})

NTU Dimensionless size

4-35

$$\text{NTU} = \frac{UA}{\dot{m}c_p}$$

NTU, or number of transfer units

U is the overall heat transfer coefficient

c_p is the specific heat.

ε Heat transfer effectiveness 0.3-0.95

$$\varepsilon = \frac{h_{c,\text{out}} - h_{c,\text{in}}}{h_{f,\text{in}} - h_{c,\text{in}}} = \frac{T_{c,\text{out}} - T_{c,\text{in}}}{T_{f,\text{in}} - T_{c,\text{in}}}$$

Model Validation

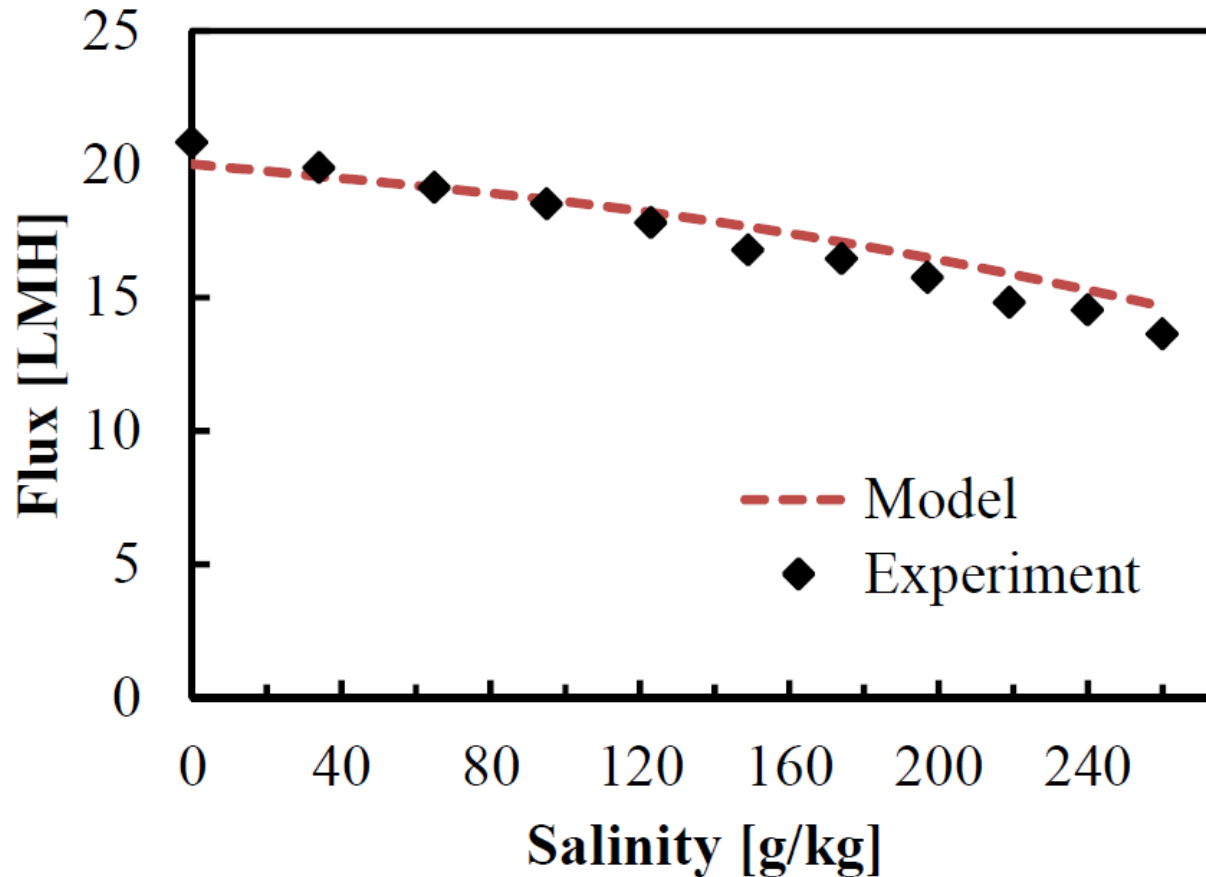
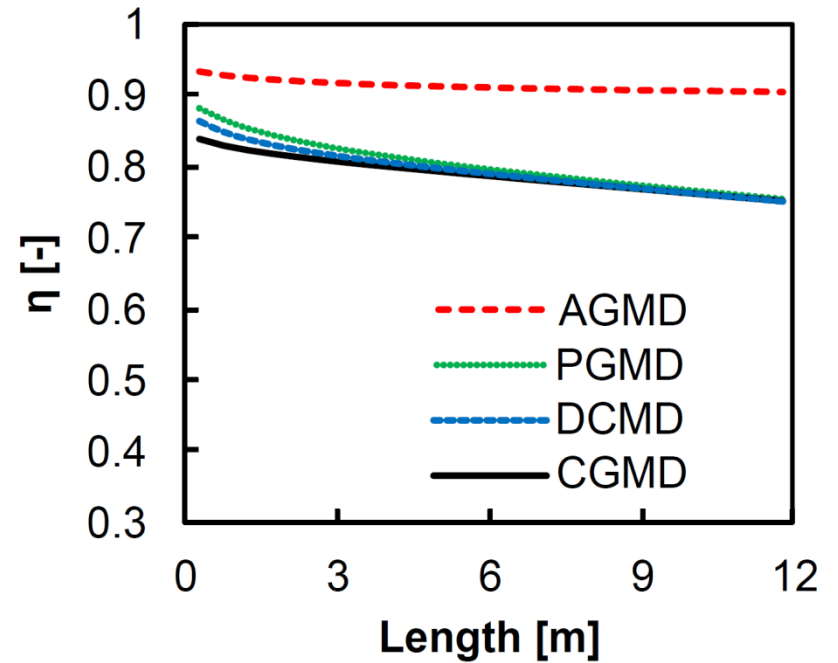
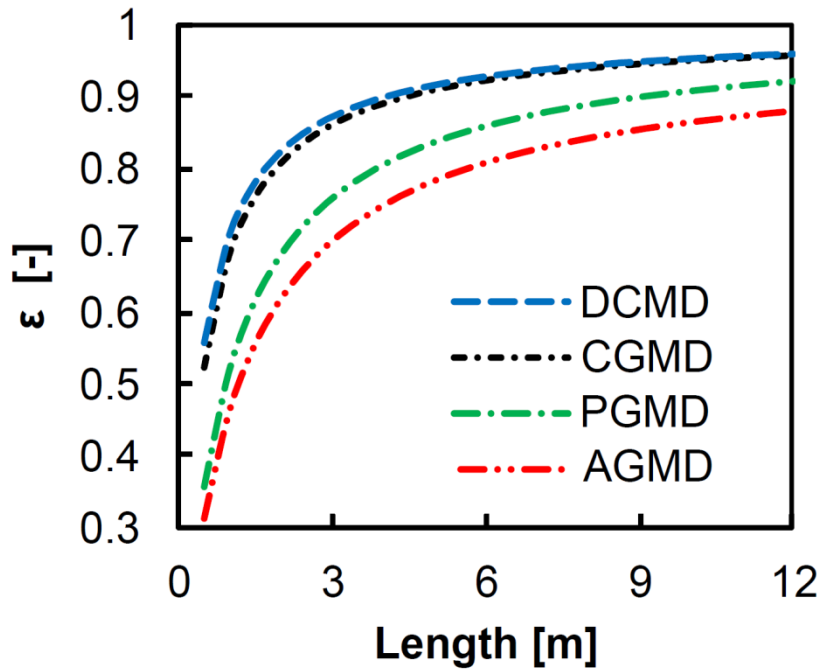


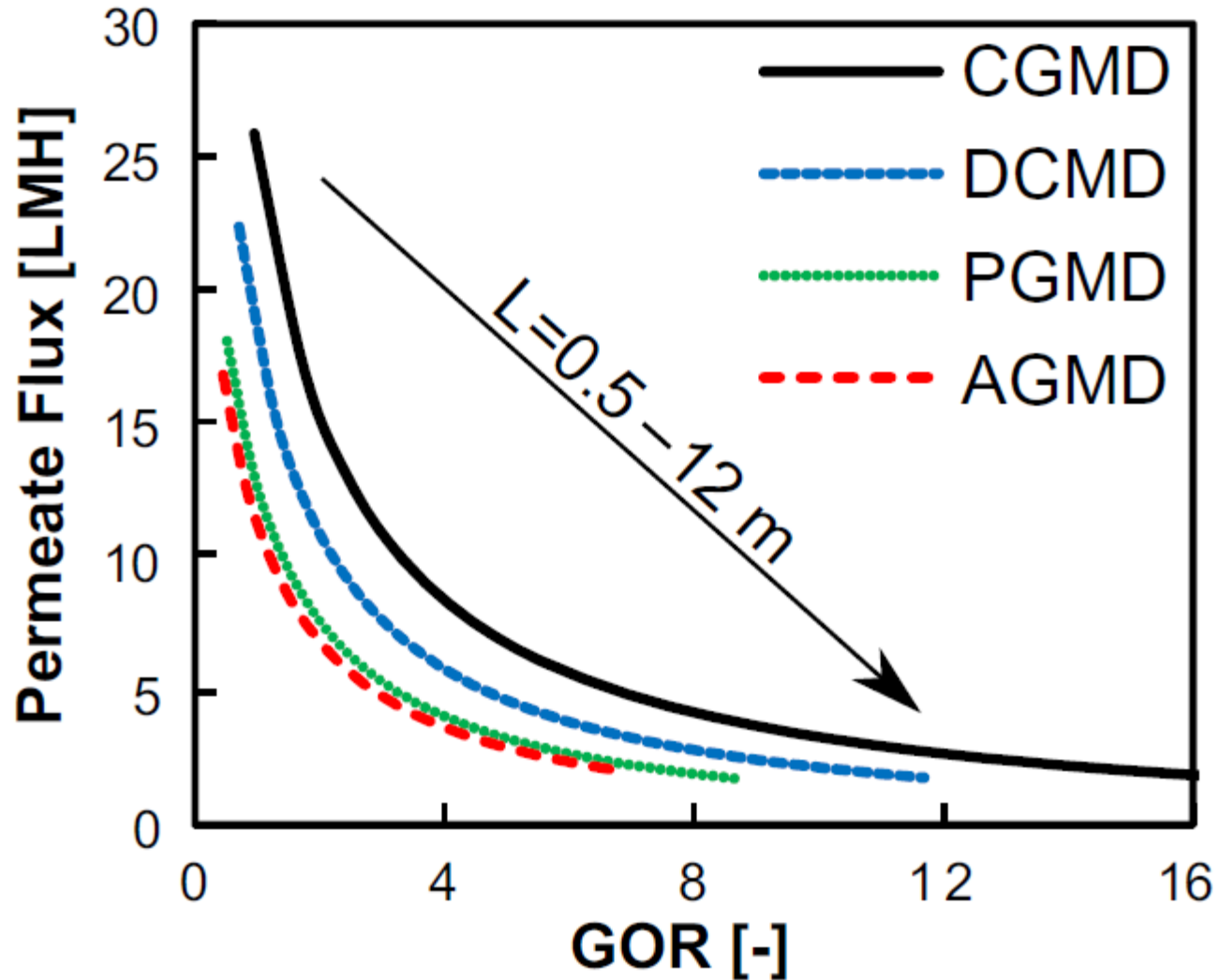
Figure 4: Validation of the 1-D Numerical Model with experimental data from [32]

η and ε



GOR vs Flux

Seawater salinity



GOR vs Flux

High salinity

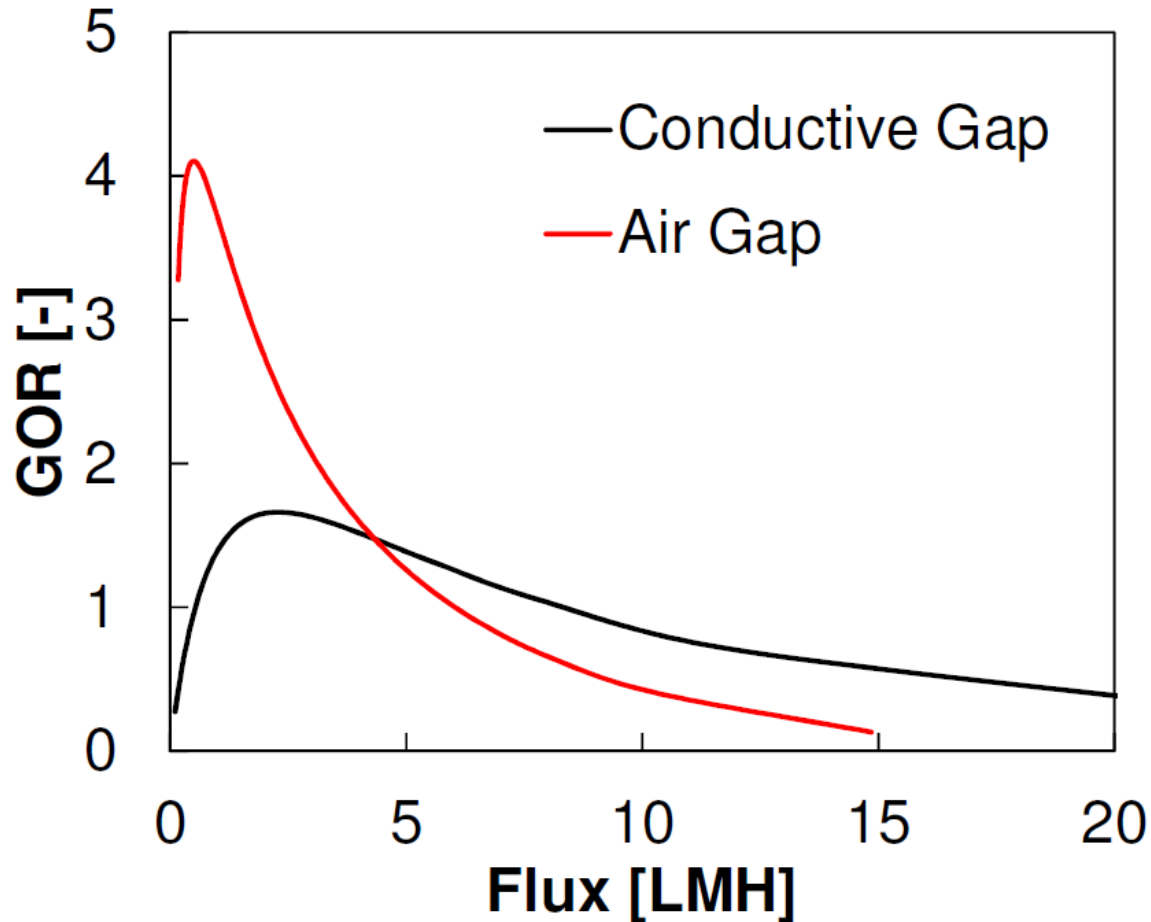
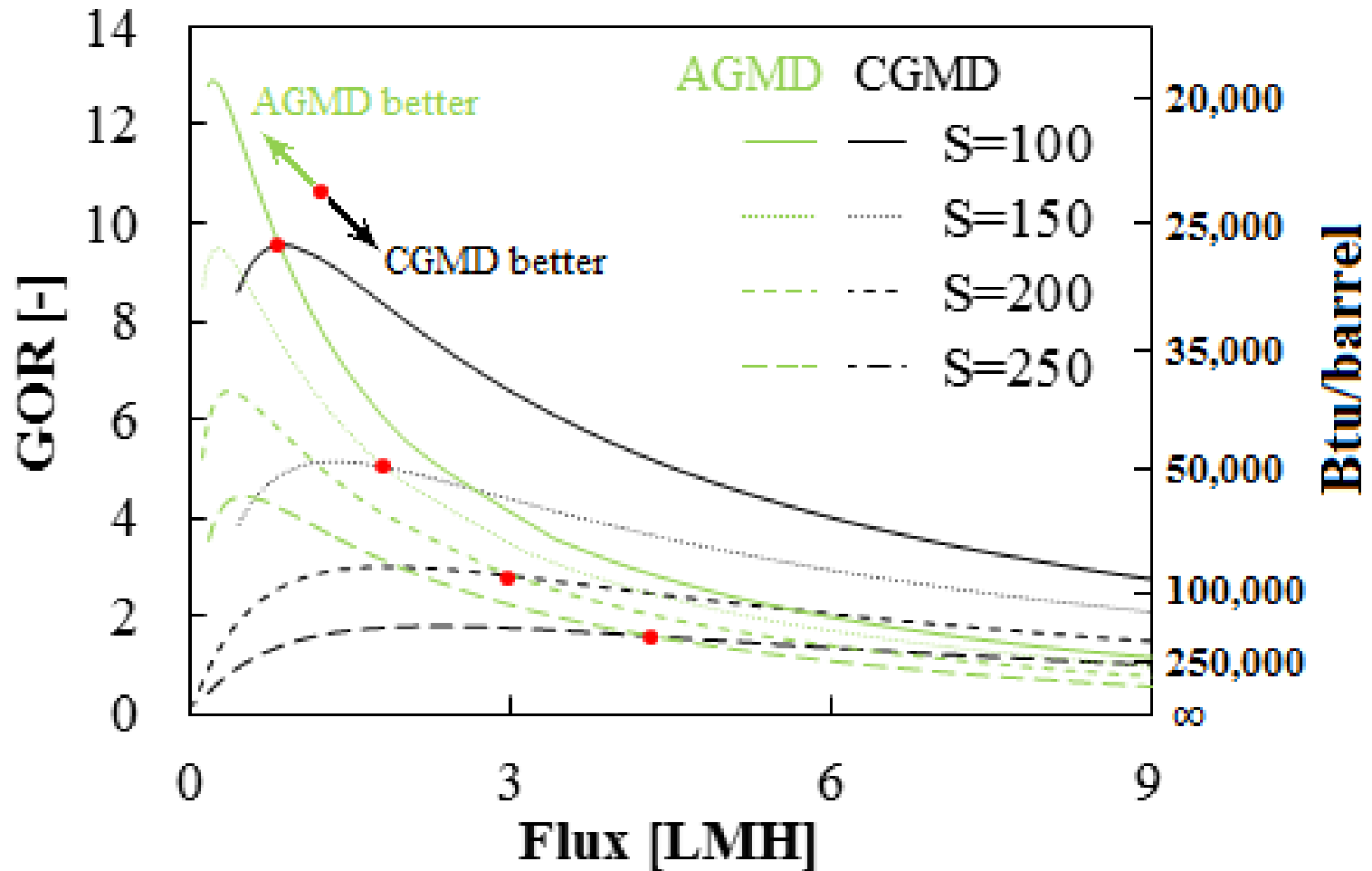


Figure 7: A comparison of GOR and Flux for AGMD and CGMD, $s_f = 250$ g/kg ⁵⁸

GOR vs Flux

High salinity



Impact of salinity AGMD

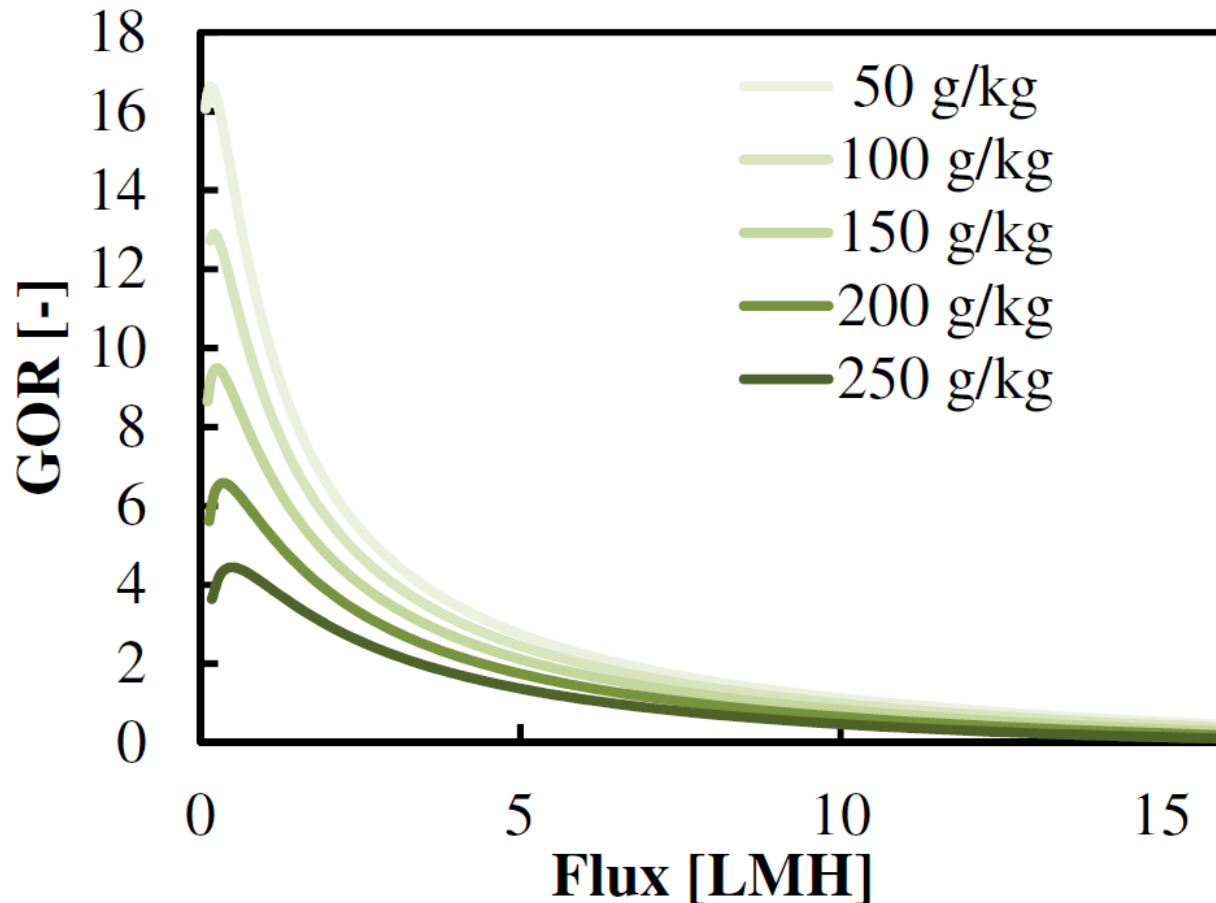


Figure 8: AGMD. The GOR-flux curves at high salinity exhibit decreasing GOR and flux at large system size ($L > L^*$) or correspondingly $J < J^*$. The J^* value increases as s_f increases, but is not as easy to see.

Dimensionless framework

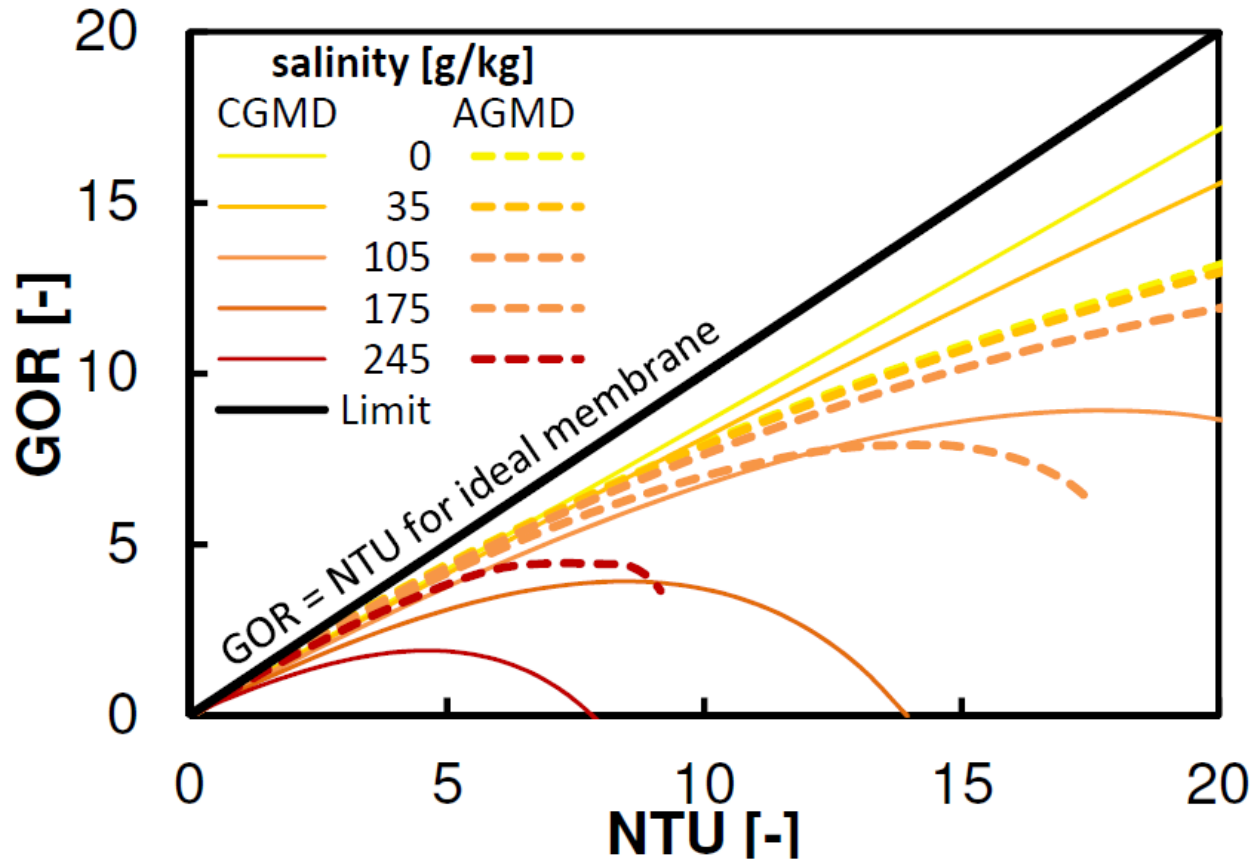


Figure 12: GOR as a function of NTU from the discretized and simplified HX model of MD. Dotted lines are results from the HX model, and show that the HX model is also capable of capturing the NTU^* beyond which flux begins to decline. Just like J^* increases at high salinity, the critical system size (or NTU^*) decreases with feed salinity. Shorter module lengths have to be used when treating high salinity water with MD. The * indicates optimal system size to maximize GOR

Maximum Performance

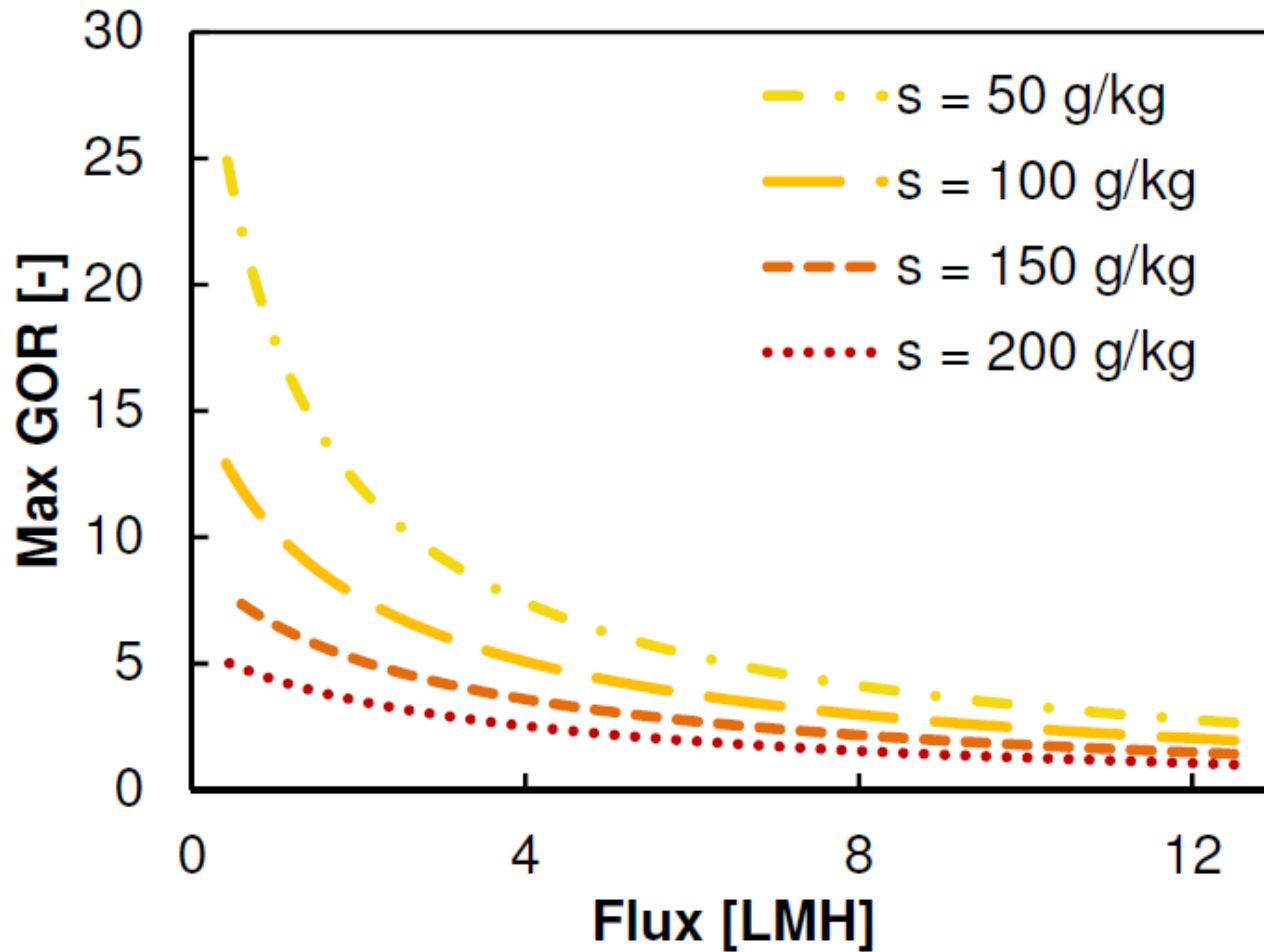


Figure 16: Max GOR possible by using the ideal membrane thickness at each salinity and flux for CGMD