

# Lecture 14

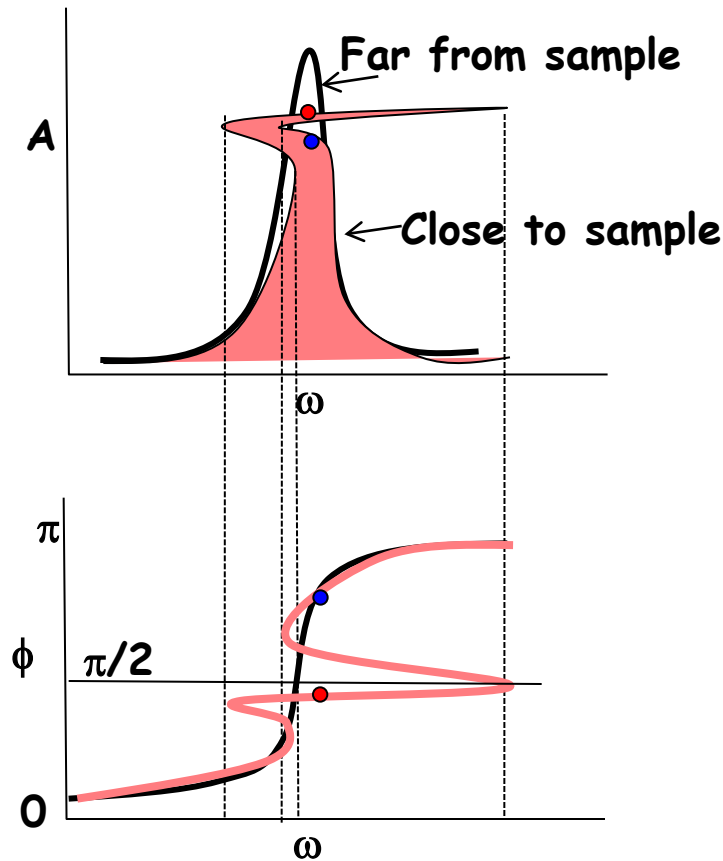
## Cantilever eigenmodes, equivalent point mass oscillator

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# Attractive vs. repulsive mode imaging



- Depending on operating conditions, it is possible to approach in attractive regime and transition to repulsive at some  $Z$

# Implications

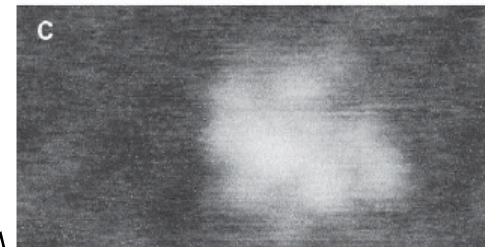
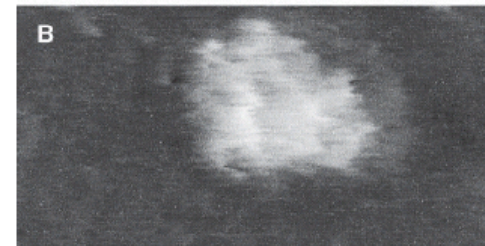
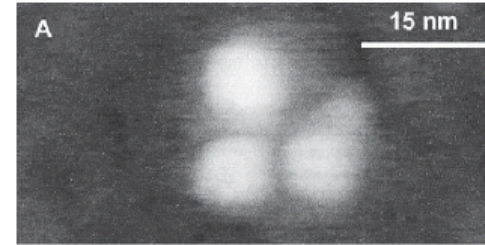
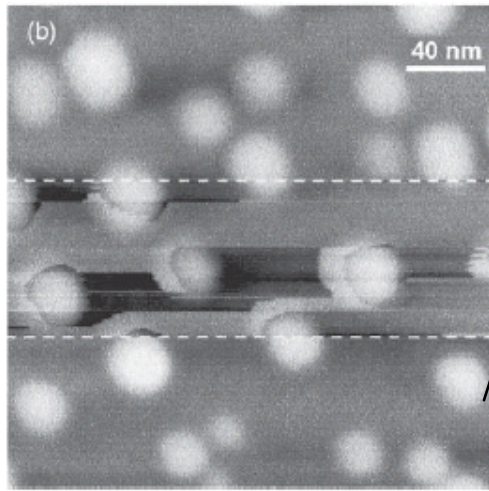
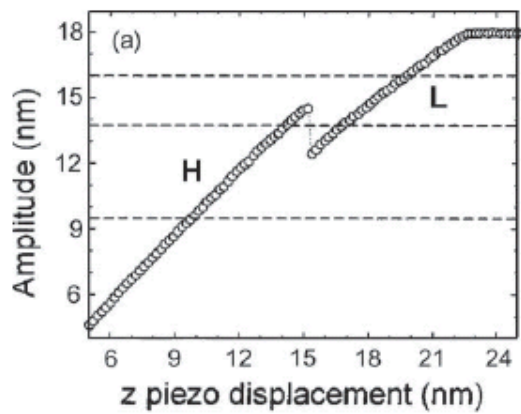
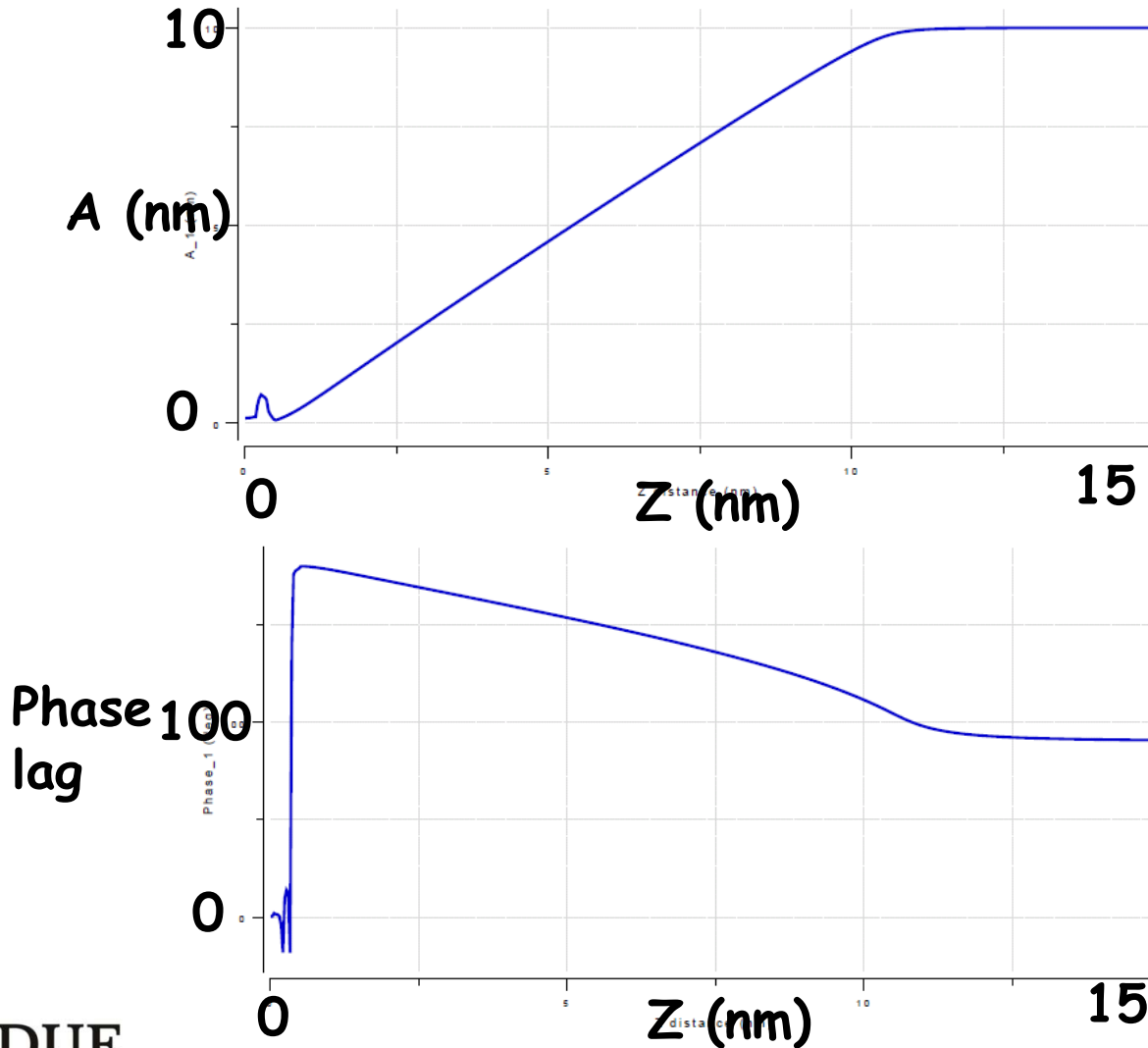


Fig. 11. Experimental determination of the low and high amplitude branches. (a) Amplitude curve, the L and H branches are plotted by open circles. Dashed lines indicate the  $A_{sp}$  values used to image a  $200 \times 200$  nm<sup>2</sup> InAs quantum dot sample. (b) The system evolves from stable imaging in the L state  $A_{sp} = 16$  nm (top) to unstable imaging due to switching between H and L states  $A_{sp} = 13.8$  nm (middle) and finally to stable imaging in the H state  $A_{sp} = 9.5$  nm (bottom). Adapted from [56].

Fig. 12. (A) High-resolution image of a single a-HSA (obtained by operating in an L state). The three fragments and the hinge regions are clearly resolved. (B) Image of the same molecule obtained by operating the instrument in an H state. (C) Image of the molecule in the initial L state after repeated imaging in an H state. The characteristic shape of the molecule has been lost by imaging in an H state. Adapted from [7].

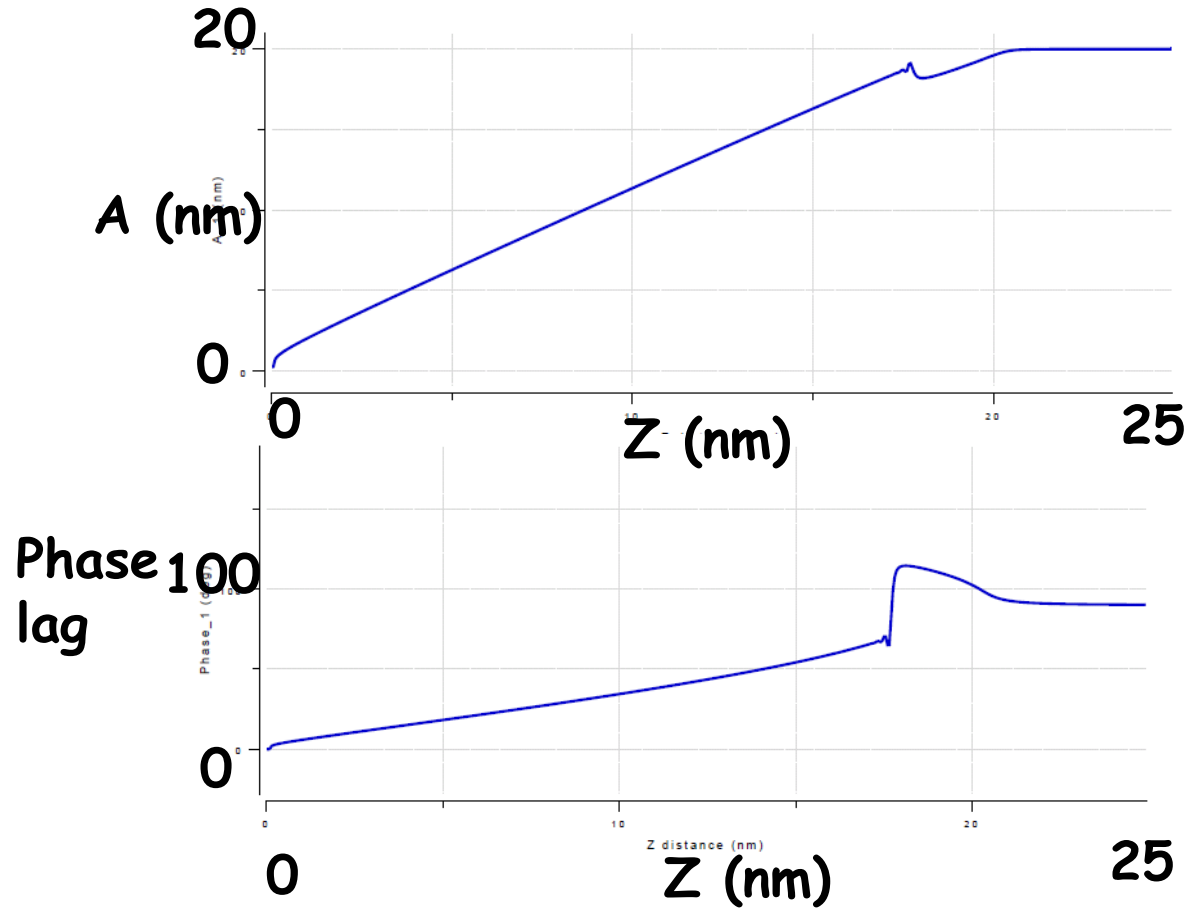
# Factors controlling this phenomenon

- $R_{\text{tip}}=10\text{nm}$ ,  $k=40\text{ N/m}$ ,  $A_0=10\text{nm}$ ,  $Q=500$ ,  $f=f_0=300\text{ kHz}$ ,  $H=2 \times 10^{-19}$ ,  $F_{\text{ad}}=1.4\text{nN}$ ,  $E^*=1\text{ GPa}$



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- Increase amplitude to tap (repulsive regime)

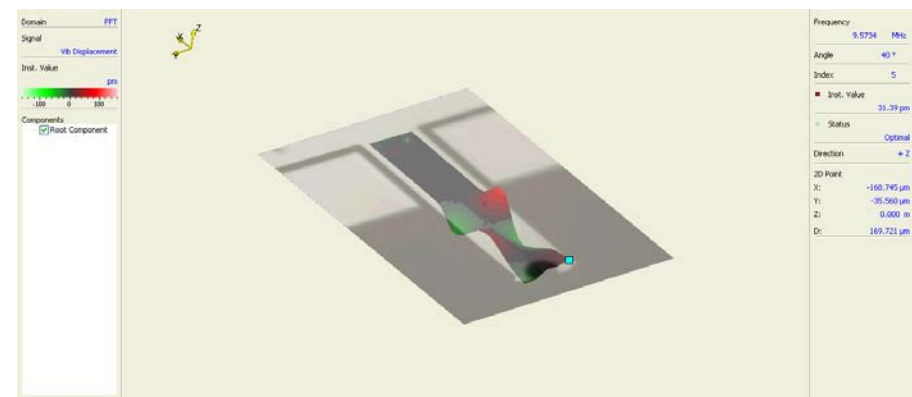
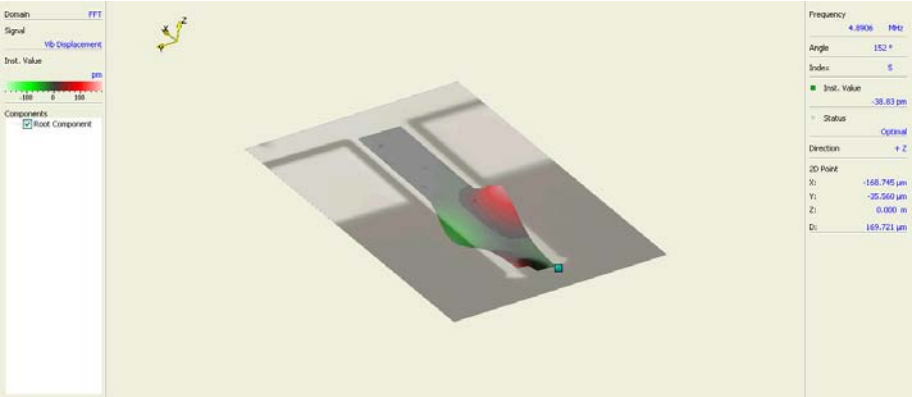
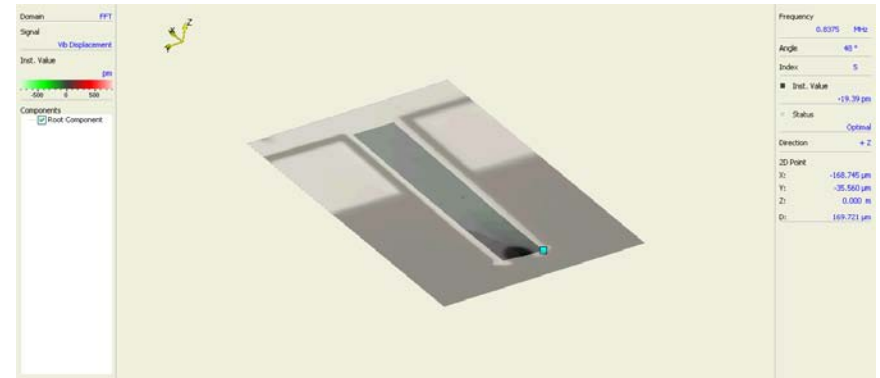
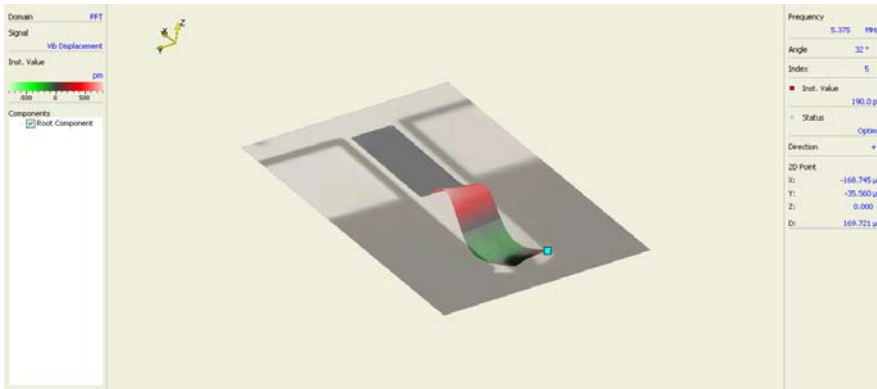
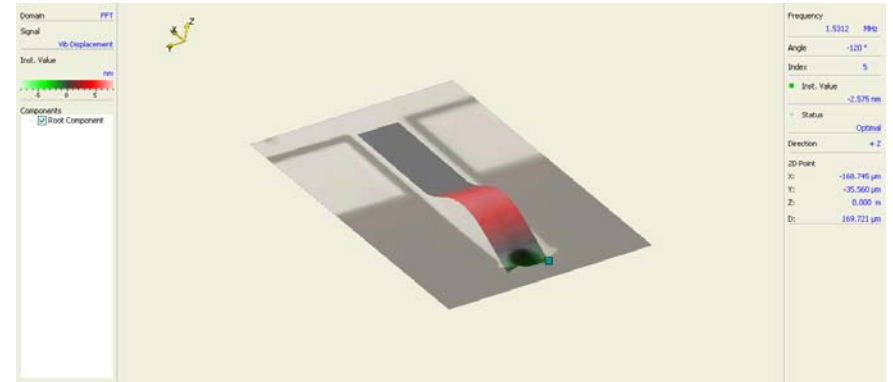
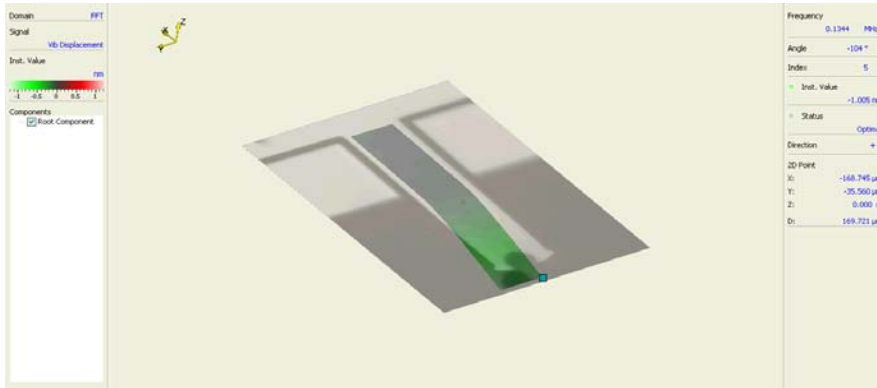
# Factors controlling this phenomenon

- $R_{\text{tip}}=10\text{nm}$ ,  $k=40\text{ N/m}$ ,  $A_0=20\text{nm}$ ,  $Q=700$ ,  $f=299\text{kHz}$   
 $z$ ,  $H=$



- Increase  $Q$  to stay in attractive regime

# Cantilever eigenmodes



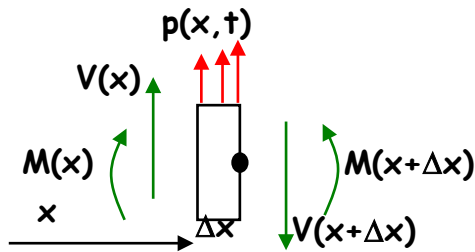
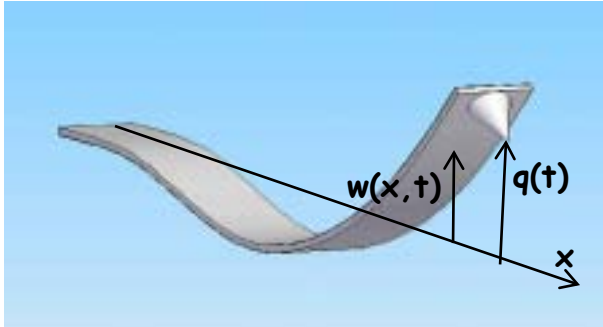


# Point mass vs. continuous oscillator?

- The point mass model was derived with the assumption that cantilever mass was  $\ll$  tip mass
- The shape of the oscillating beam in the point mass model is assumed to be that of a statically bent beam under a tip force
- The point mass model does not predict any oscillation modes beyond the fundamental
- How to include spatially continuous nature of the AFM cantilever and yet enjoy the simplicity of a point mass model?



# Transverse vibrations of classical beam



$p(x, t)$ : external force per unit length

$A$ : Area of cross section

$\rho$ : mass density of cantilever

## ■ Bernoulli-Euler beam theory

$$V(x) + p(x, t)\Delta x - V(x + \Delta x) = (\rho A \Delta x)\ddot{w},$$

as  $\Delta x \rightarrow 0$  we get  $\rho A \ddot{w} = -\frac{\partial V}{\partial x} + p(x, t)$

or

$$\rho A \ddot{w} = -\frac{\partial^2 M}{\partial x^2} + p(x, t) = -EI \frac{\partial^4 w}{\partial x^4} + p(x, t)$$

Or

$$\rho A \ddot{w} + EI \frac{\partial^4 w}{\partial x^4} = p(x, t)$$

To be solved with boundary conditions

$$w(0) = 0$$

$$\frac{\partial w}{\partial x}(0) = 0$$

$$V(L) = EI \frac{\partial^3 w}{\partial x^3}(L) = ??$$

$$M(L) = EI \frac{\partial^2 w}{\partial x^2}(L) = ??$$

# Transverse vibrations of classical beam

- To calculate eigenmodes and natural frequencies, one can set  $p(x,t)=0$  and any damping=0

$$\rho A \ddot{w} + EI \frac{\partial^4 w}{\partial x^4} = 0 \quad (1)$$

$$\text{Let } w(x,t) = \phi(x)T(t) \quad (2)$$

$$\left( \frac{EI}{\rho A} \right) \frac{d^4 \phi(x)}{dx^4} = - \frac{1}{T(t)} \frac{d^2 T}{dt^2} = \text{const} = \omega^2 \quad (3)$$

$$T(t) = A \sin(\omega t) + B \cos(\omega t) \quad \phi(x) = C e^{\lambda x} \quad (4)$$

(4) in (3a)  $\rightarrow$

$$\lambda^4 = \beta^4 = \frac{\rho A \omega^2}{EI} \Rightarrow \lambda_{1,2} = \pm \beta, \lambda_{3,4} = \pm i \beta \quad (5)$$

$$\begin{aligned} \phi(x) &= C_1 e^{\beta x} + C_2 e^{-\beta x} + C_3 e^{i\beta x} + C_4 e^{-i\beta x} \\ &\cong C_1 \sin(\beta x) + C_2 \cos(\beta x) + C_3 \sinh(\beta x) + C_4 \cosh(\beta x) \end{aligned}$$

$$\text{and } \omega^2 = \beta^2 \sqrt{\frac{EI}{\rho A}}$$

# Transverse vibrations of classical beam

- Assuming negligible tip mass

$$\phi(x) = C_1 \cos(\beta x) + C_2 \sin(\beta x) + C_3 \cosh(\beta x) + C_4 \sinh(\beta x) \text{ where } \beta^4 = \rho A \omega^2 / EI \quad (1)$$

$$w(0) = 0, \quad \frac{\partial w}{\partial x}(0) = 0, \quad EI \frac{\partial^3 w}{\partial x^3}(L) = 0, \quad EI \frac{\partial^2 w}{\partial x^2}(L) = 0$$

$$C_1 = C_3 = 0 \text{ and}$$

$$C_2(\cos(\beta L) + \cosh(\beta L)) + C_4(\sin(\beta L) + \sinh(\beta L)) = 0 \quad (2)$$

$$C_2(-\sin(\beta L) + \sinh(\beta L)) + C_4(\cos(\beta L) + \cosh(\beta L)) = 0$$

$$\text{or} \begin{bmatrix} \cos(\beta L) + \cosh(\beta L) & \sin(\beta L) + \sinh(\beta L) \\ -\sin(\beta L) + \sinh(\beta L) & \cos(\beta L) + \cosh(\beta L) \end{bmatrix} \begin{bmatrix} C_2 \\ C_4 \end{bmatrix} \quad (3)$$

for solutions where  $C_2, C_4 \neq 0$  we must have

$$\cos(\beta L) \cosh(\beta L) + 1 = 0 \quad (4)$$

$$\text{and } C_4 = -\frac{\cos(\beta L) + \cosh(\beta L)}{\sin(\beta L) + \sinh(\beta L)} C_2 \quad (5)$$

Solving (4) yields  $(\beta L)_1 = 1.875, (\beta L)_2 = 4.694, (\beta L)_3 = 7.855 \dots$

So that the eigenmodes are

$$\phi_n(x) = (\cos(\beta_n x) - \cosh(\beta_n x)) - \frac{\cos(\beta_n L) + \cosh(\beta_n L)}{\sin(\beta_n L) + \sinh(\beta_n L)} (\sin(\beta_n x) - \sinh(\beta_n x)) \quad (6)$$

Normalize so that  $\phi_n(L) = 1$

# Eigenmodes



1<sup>st</sup> eigenmode

$$(\beta L)_1 = 1.875, (\beta L)_2 = 4.694, (\beta L)_3 = 7.855 \dots$$

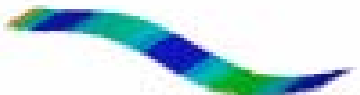
Thus



$$\omega_1 : \omega_2 : \omega_3 : \dots = 1 : 6.26 : 17.55 : \dots$$

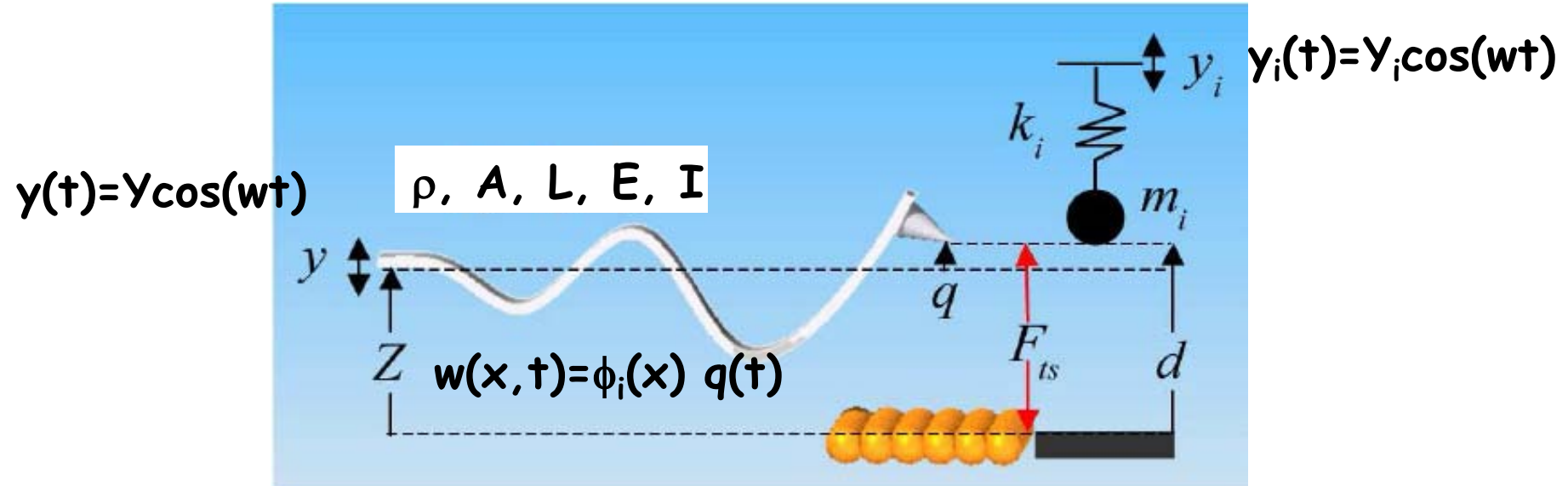
2<sup>nd</sup> eigenmode

*for a uniform rectangular lever with negligible tip mass*



3<sup>rd</sup> eigenmode

# Equivalent point mass oscillator



## Energy based equivalence principle

$$\frac{1}{2} k_i q^2 = \frac{1}{2} \int_{x=0}^{x=L} EI \left( \frac{d^2 \phi_i}{dx^2} \right)^2 dx \quad \frac{1}{2} m_i q^2 = \frac{1}{2} \int_{x=0}^{x=L} \rho A (\phi_i)^2 dx \quad Y_i = Y \left( \frac{\omega}{\omega_i} \right)^2 \frac{\int_0^L \phi_i(x) dx}{\int_0^L \left( \frac{d^2 \phi_i}{dx^2} \right) dx}$$

For negligible tip mass

$$k_1 = 1.03k, k_2 = 40.5k, k_3 = 317k$$

$$m_1 = m_2 = m_3 = \dots = 0.249 \rho AL$$

$$Y_1 \sim 1.5Y$$