

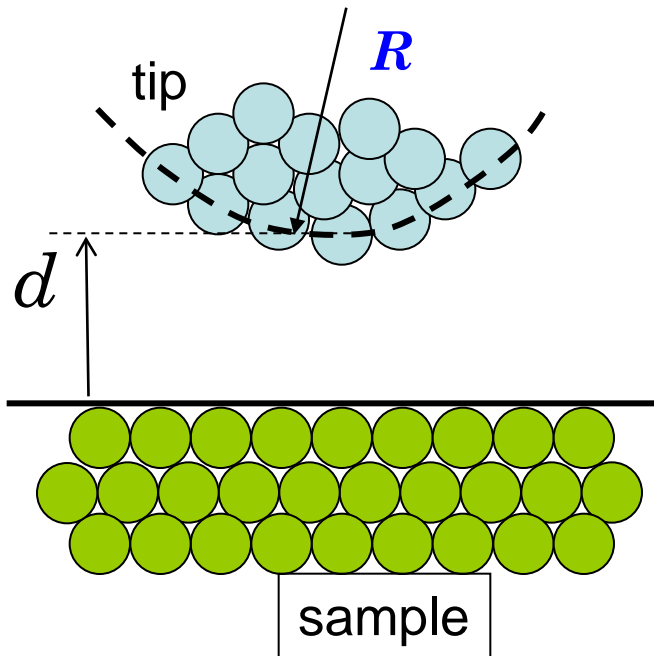
Lecture 9

Force distance curves I

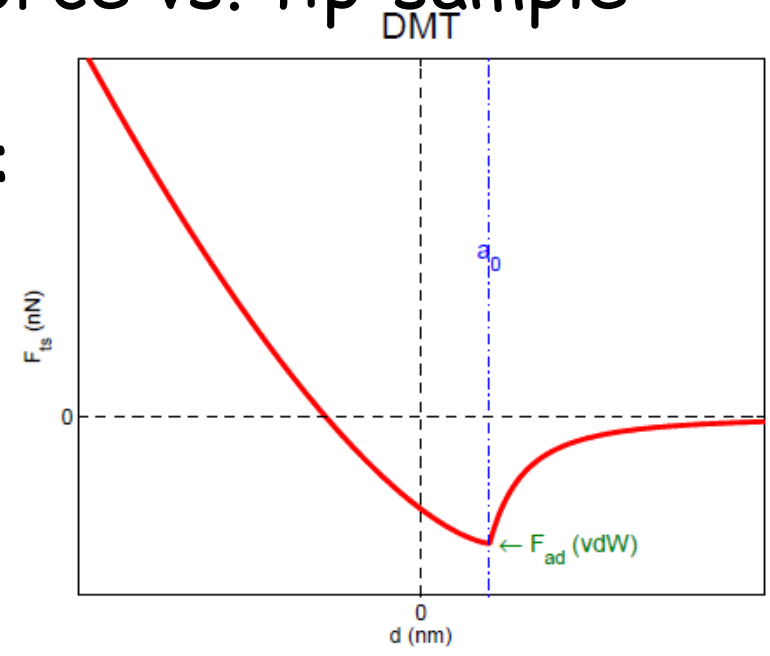
Arvind Raman
Mechanical Engineering
Birck Nanotechnology Center

F-d curve

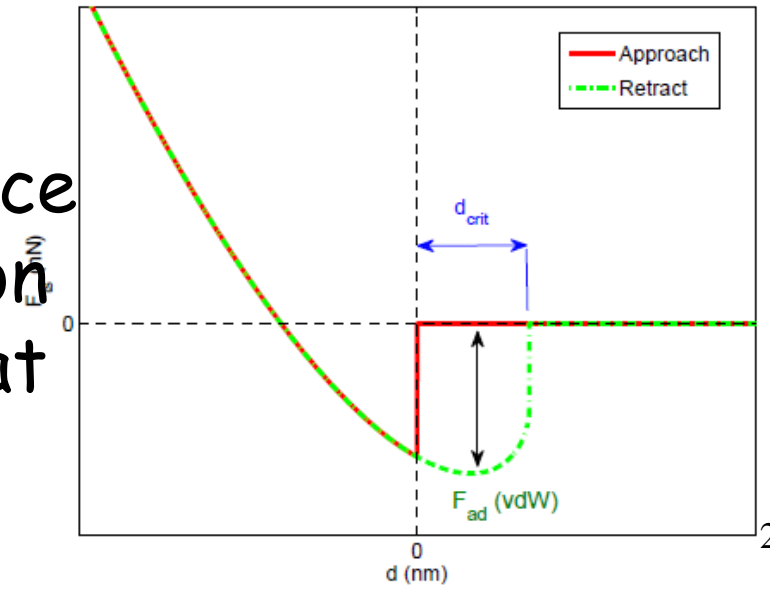
- Is the effective tip sample force vs. tip-sample separation (or indentation)



Examples:

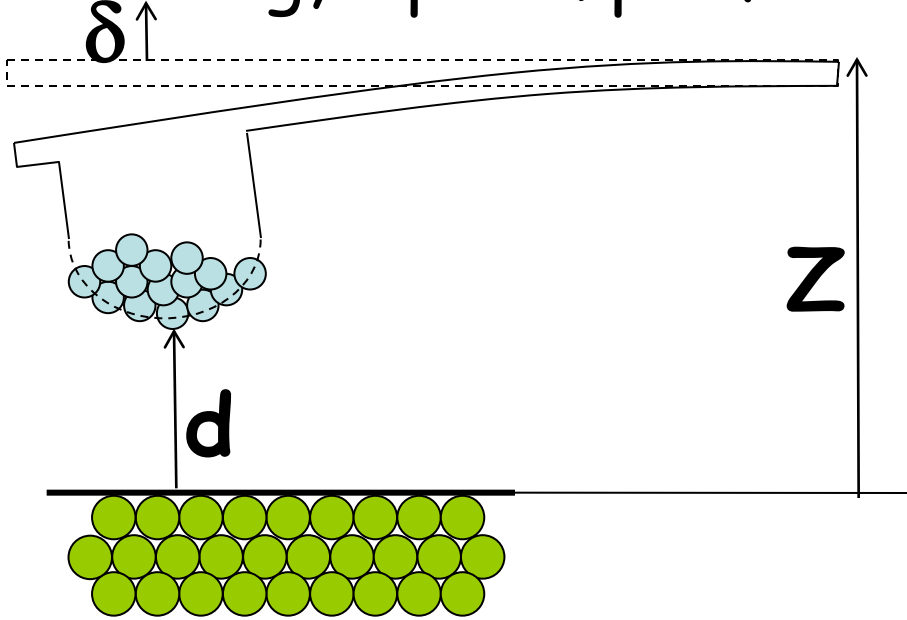


- Usually $d=0$ chosen at min force
- $d < 0$ indentation, $d > 0$ separation
- Unfortunately, this is not what we measure directly in AFM



F-Z curve - what we measure in AFM

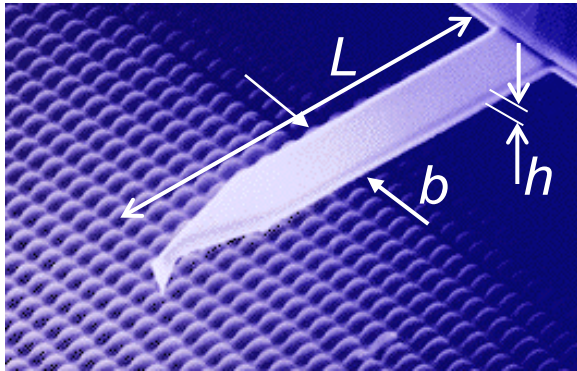
- Z is the Z-piezo displacement, δ is the cantilever bending, tip-sample force is $F_{ts} = k_{cant}\delta$



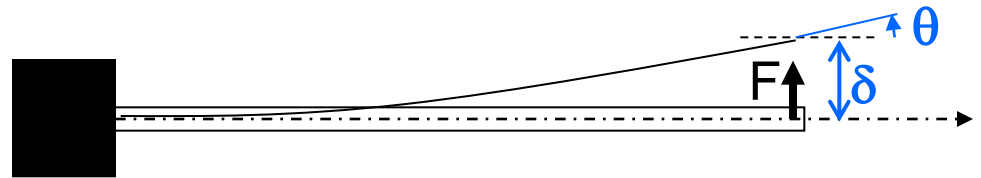
AFM's measure F_{ts} vs. Z !!

- How to convert force-displacement (F vs Z) to force distance (F vs d) and vice versa?
- Collect F - Z data and for every F value, evaluate $d = Z + \delta$, to within an arbitrary constant

The microcantilever – the force sensor



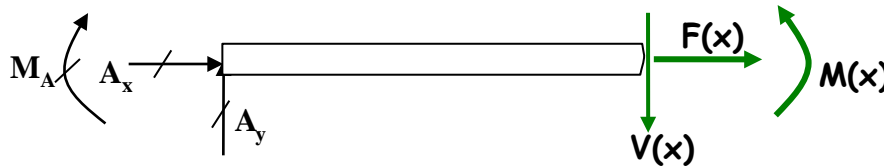
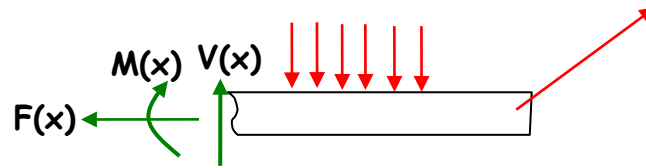
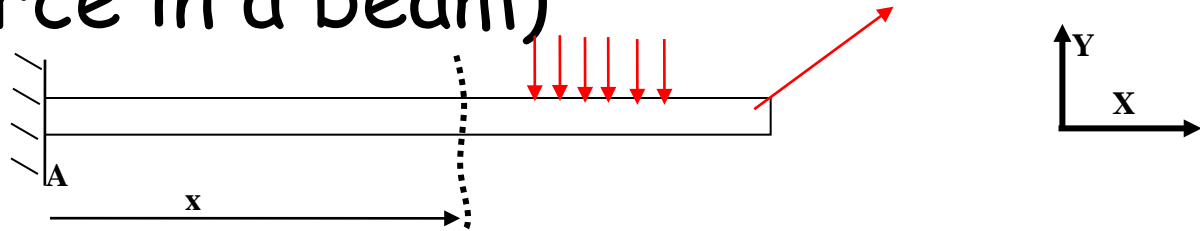
www.olympus.co.jp



- From elementary beam theory, if E =Young's modulus, $I=bh^3/12$ then
- $\delta=w(L)=F L^3/(3EI)$, and $\theta=dw(L)/dx=FL^2/(2EI)$
- Deflection and slope linearly proportional to force sensed at the tip
- $k=3EI/L^3$ is called the bending stiffness of the cantilever

Classical beam theory

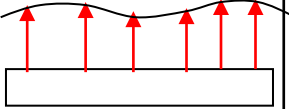
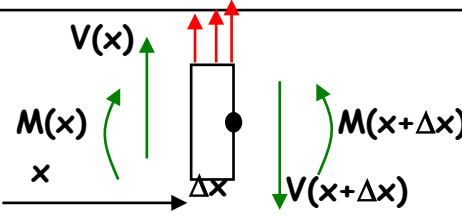
- Understanding internal resultants (shear force, bending moment and axial force in a beam)



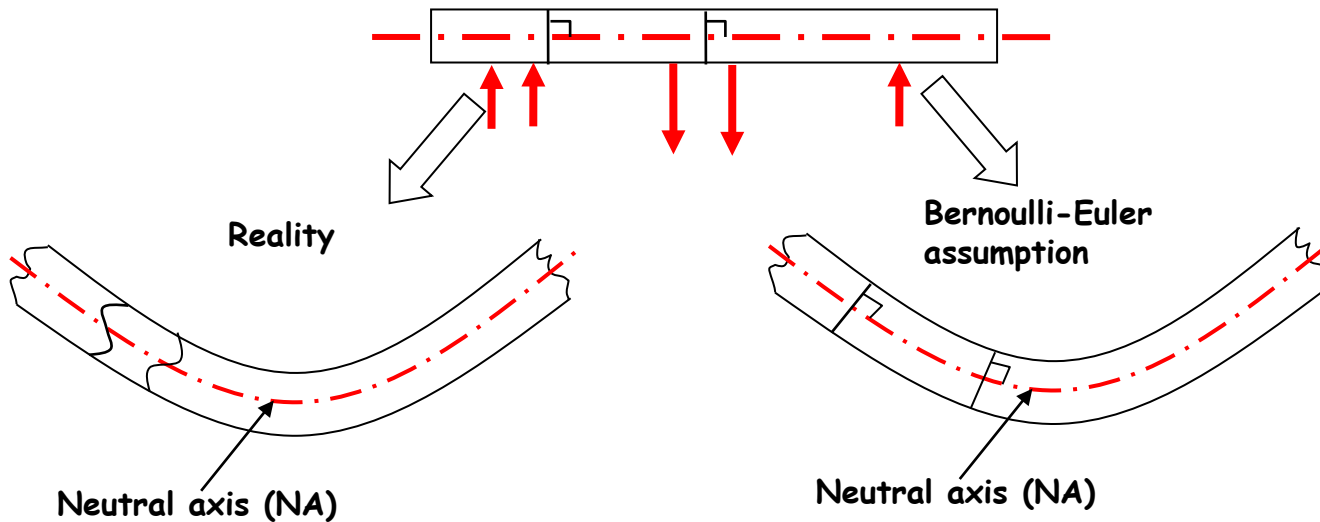
$V(x)$: Internal shear force (N)
 $F(x)$: Internal axial force (N)
 $M(x)$: Internal bending moment (N.m)

Classical beam theory

■ Relationship between $V(x)$ and $M(x)$

Key Equation	Applied Load	Derivation
$\frac{dV}{dx} = p(x)$	 <p>$p(x)$ N/m</p>	 <p> $V(x) + p(x)\Delta x - V(x + \Delta x) = 0,$ <i>as $\Delta x \rightarrow 0$ we get $\frac{dV}{dx} = p(x)$</i> </p>
$\frac{dM}{dx} = V(x)$		<p> $M(x + \Delta x) - M(x) - V(x)\Delta x - p(x)\Delta x\left(\frac{\Delta x}{2}\right) = 0,$ <i>as $\Delta x \rightarrow 0$ we get $\frac{dM}{dx} = V(x)$</i> </p>

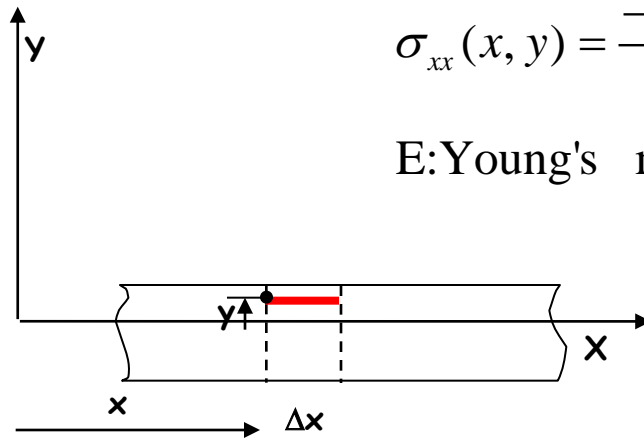
Classical beam theory- stress/strain



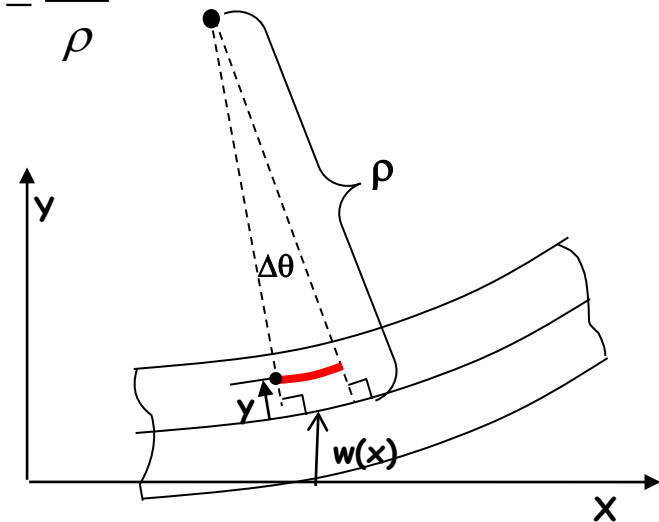
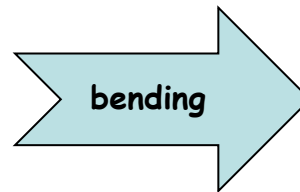
$$\epsilon_{xx}(x, y) = \lim_{\Delta x \rightarrow 0} \frac{(\rho - y)\Delta\theta - \rho\Delta\theta}{\rho\Delta\theta} = \frac{-y}{\rho}$$

$$\sigma_{xx}(x, y) = \frac{-Ey}{\rho} \sim -Ey \frac{d^2 w}{dx^2}$$

E: Young's modulus (N/m² or Pa)



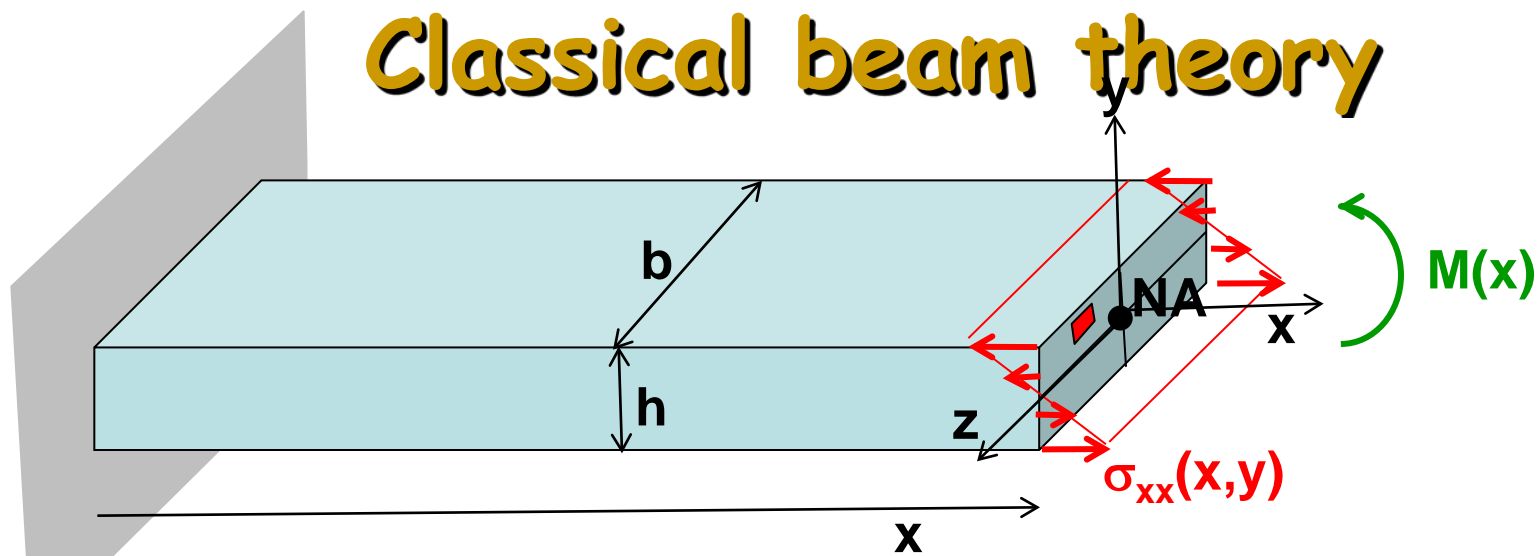
Undeformed beam segment



Deformed beam segment

Key: σ_{xx} varies linearly across section

Classical beam theory



$$M(x) = \int_{z=-b/2}^{+b/2} \int_{y=-h/2}^{h/2} (\sigma_{xx}(x) dy dz) y$$

$$\text{or } M(x) = \int_{z=-b/2}^{+b/2} \int_{y=-h/2}^{h/2} E y^2 \frac{d^2 w(x)}{dx^2} dy dz = E \frac{d^2 w(x)}{dx^2} \int_{z=-b/2}^{+b/2} \int_{y=-h/2}^{h/2} y^2 dy dz$$

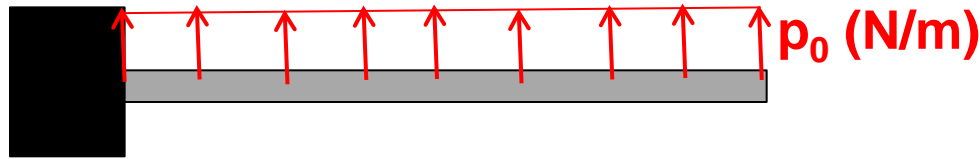
$$\text{or } M(x) = E I_{zz} \frac{d^2 w(x)}{dx^2} \quad \text{where } I_{zz} = \frac{bh^3}{12} \quad (\text{area moment } m^4)$$

$$\text{Likewise } V(x) = E I_{zz} \frac{d^3 w(x)}{dx^3}$$

$$\text{Finally } E I \frac{d^4 w(x)}{dx^4} = p(x) \text{ to be solved with boundary conditions at } x = 0, L$$

Classical beam theory

■ Example 1



$$EI \frac{d^4 w(x)}{dx^4} = p_0 \Rightarrow \frac{d^3 w(x)}{dx^3} = \frac{p_0}{EI} x + c_1$$

$$\Rightarrow \frac{d^2 w(x)}{dx^2} = \frac{1}{2} \frac{p_0}{EI} x^2 + c_1 x + c_2 \Rightarrow \frac{dw(x)}{dx} = \theta(x) = \frac{1}{6} \frac{p_0}{EI} x^3 + \frac{1}{2} c_1 x^2 + c_2 x + c_3$$

$$w(x) = \frac{1}{24} \frac{p_0}{EI} x^4 + \frac{1}{6} c_1 x^3 + \frac{1}{2} c_2 x^2 + c_3 x + c_4$$

Boundary conditions

$$w(0) = \theta(0) = 0 \quad EI \frac{d^2 w(L)}{dx^2} = EI \frac{d^3 w(L)}{dx^3} = 0$$

(no point moments or force applied at $x = L$)

$$\Rightarrow c_3 = c_4 = 0, \quad c_1 = -\frac{p_0 L}{EI}, \quad c_2 = \frac{1}{2} \frac{p_0 L^2}{EI}$$

$$w(L) = \delta = \frac{1}{8} \frac{p_0 L^4}{EI}, \quad \theta(L) = \theta = \frac{1}{6} \frac{p_0 L^3}{EI} \Rightarrow \frac{\theta}{\delta} = \frac{4}{3} L$$

Classical beam theory

■ Example 2



$$EI \frac{d^4 w(x)}{dx^4} = 0 \Rightarrow \frac{d^3 w(x)}{dx^3} = c_1 \Rightarrow \frac{d^2 w(x)}{dx^2} = c_1 x + c_2$$

$$\Rightarrow \frac{dw(x)}{dx} = \theta(x) = \frac{1}{2} c_1 x^2 + c_2 x + c_3$$

$$w(x) = \frac{1}{6} c_1 x^3 + \frac{1}{2} c_2 x^2 + c_3 x + c_4$$

Boundary conditions

$$w(0) = \theta(0) = 0 \quad EI \frac{d^2 w(L)}{dx^2} = 0 \quad EI \frac{d^3 w(L)}{dx^3} = -F$$

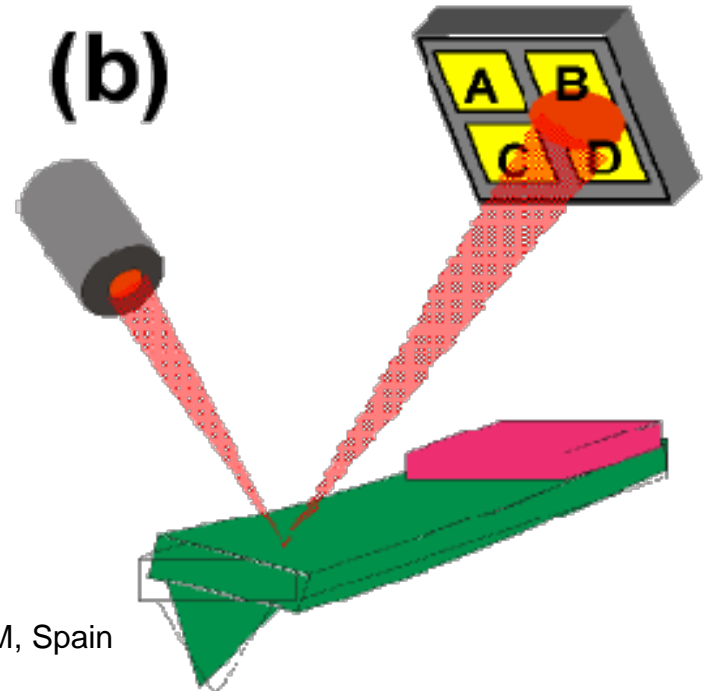
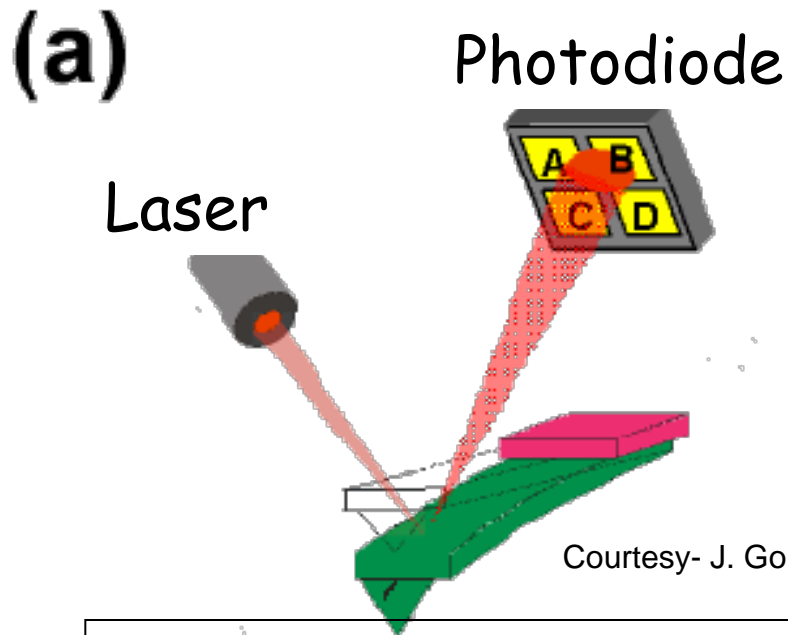
(no point moment applied at $x = L$)

$$\Rightarrow c_3 = c_4 = 0, \quad c_1 = -\frac{F}{EI}, \quad c_2 = \frac{FL}{EI}$$

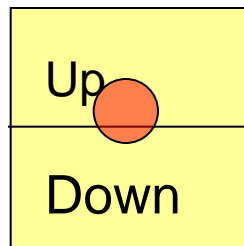
$$w(L) = \delta = \frac{1}{3} \frac{FL^3}{EI}, \quad \theta(L) = \theta = \frac{1}{2} \frac{FL^2}{EI} \Rightarrow \frac{\theta}{\delta} = \frac{2}{3} L$$

$F = k\delta$, where $k = \frac{3EI}{L^3}$ is the static bending stiffness of the cantilever

The four-quadrant photodiode



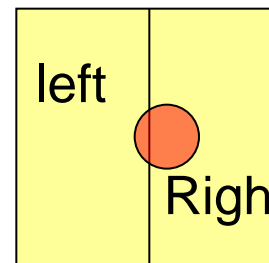
a) Vertical bending



$A+B=UP$

$C+D=DOWN$

b) Lateral/torsion motion

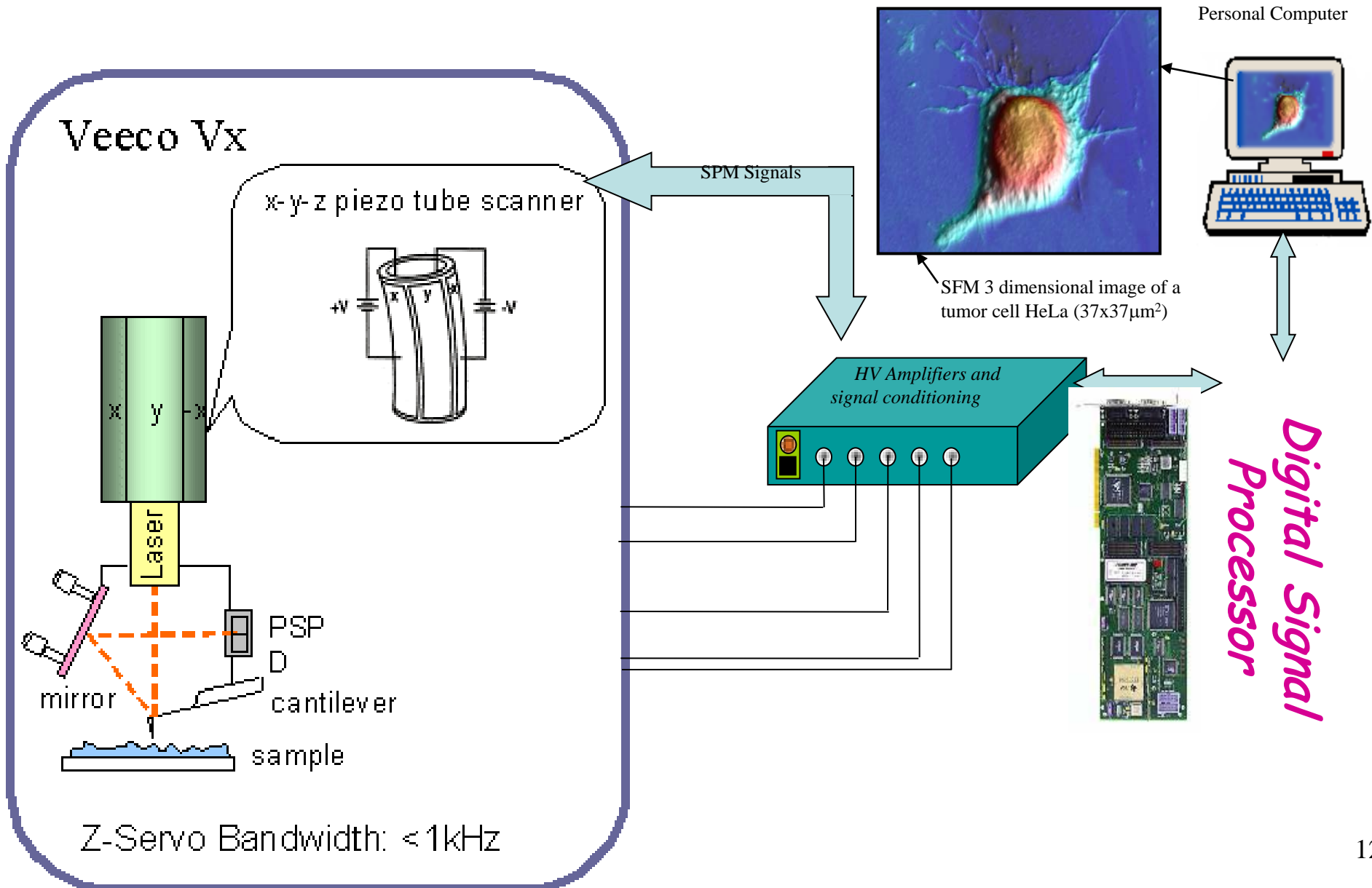


$A+C=LEFT$

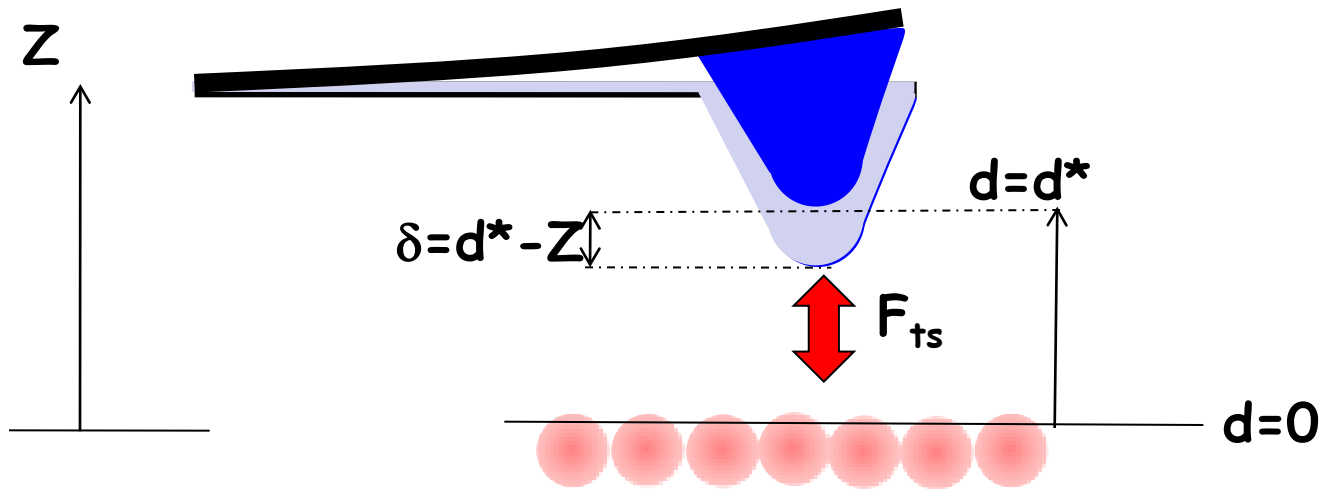
$B+D=Right$

Commercial AFMs measure the rotation angle!!! (bending or torsion)

AFM Block Diagram



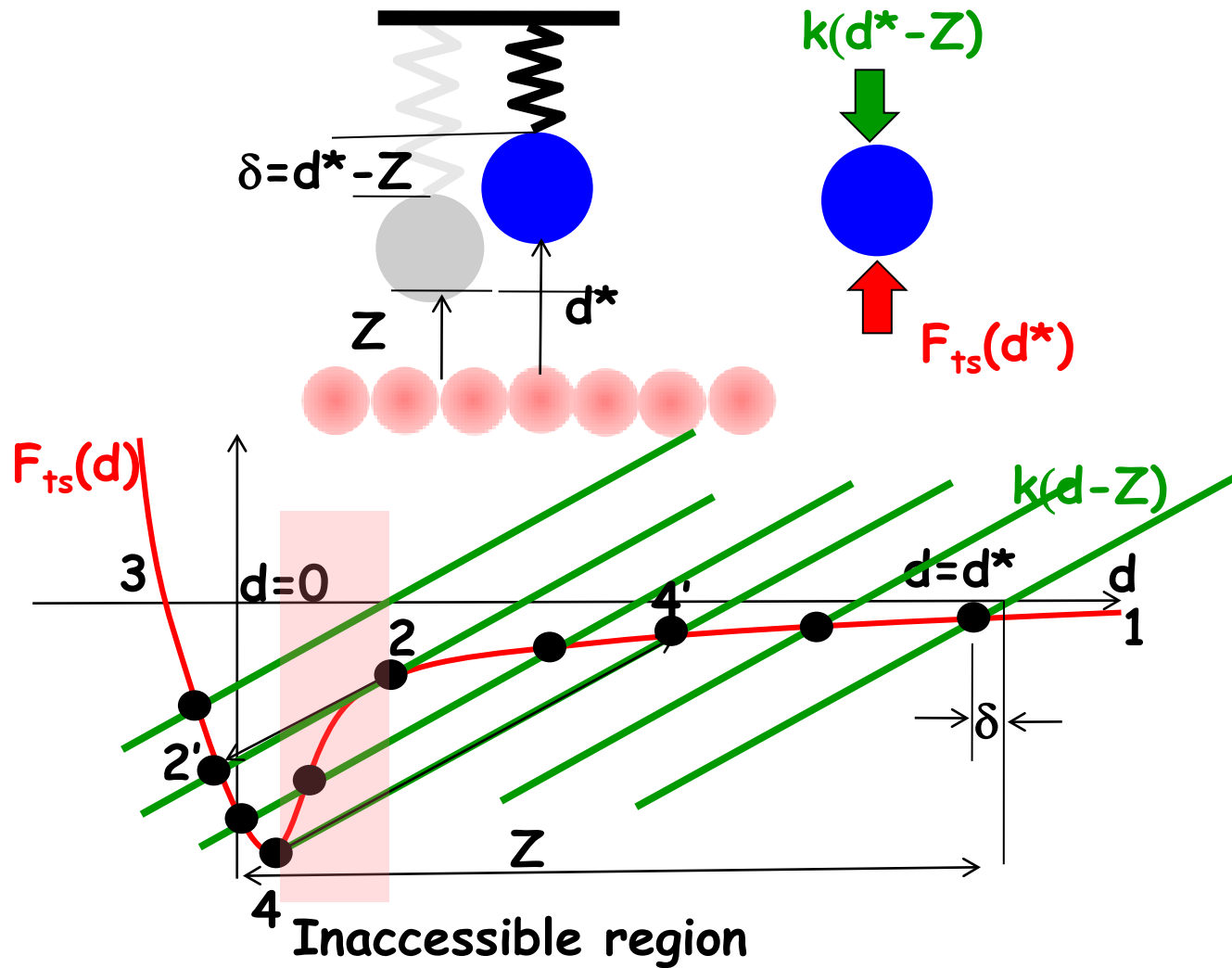
Equilibrium positions during approach and retraction



- How do d^* and δ change as Z is reduced during approach and then retracted?
- Note that technically $\delta = d^* - Z - \text{Tip height}$ but tip height is basically an arbitrary constant

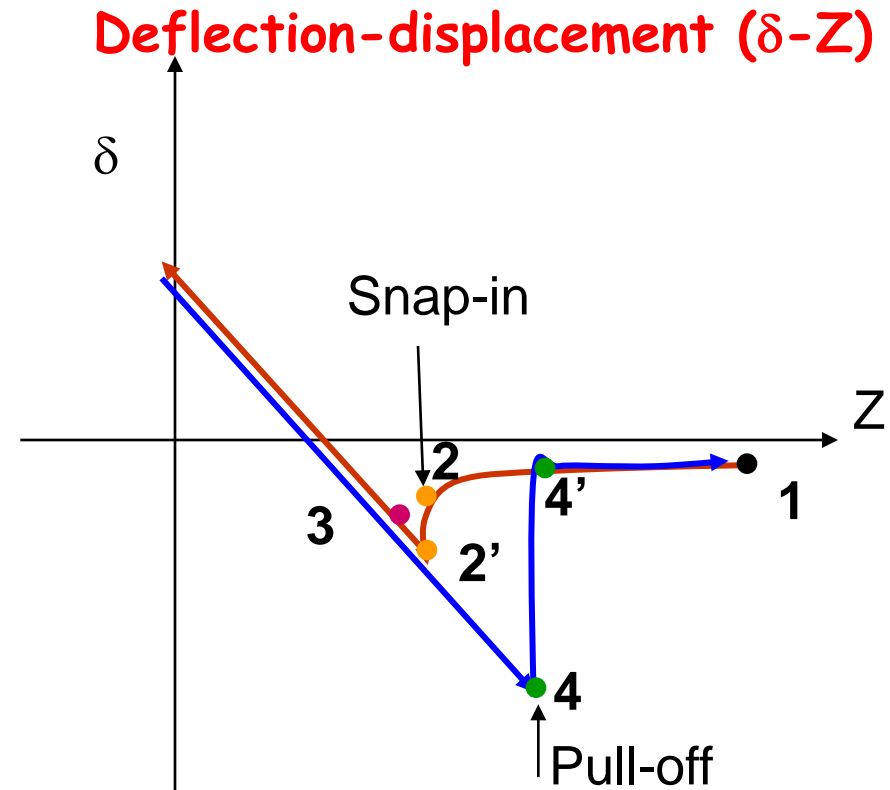
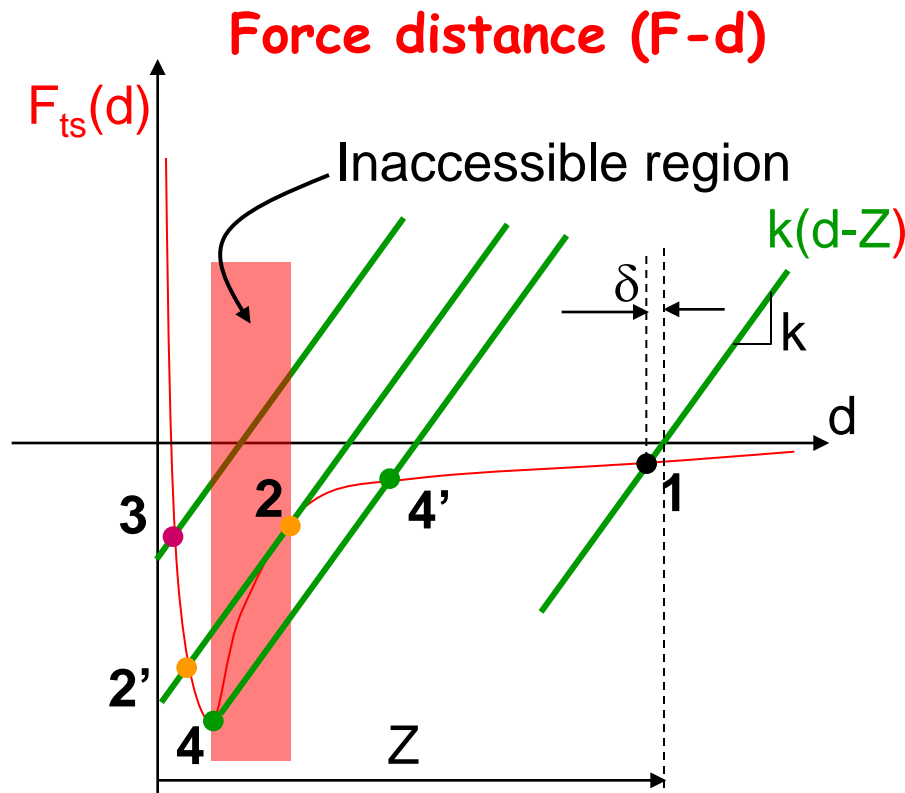
Cantilever instabilities during approach and retraction

2



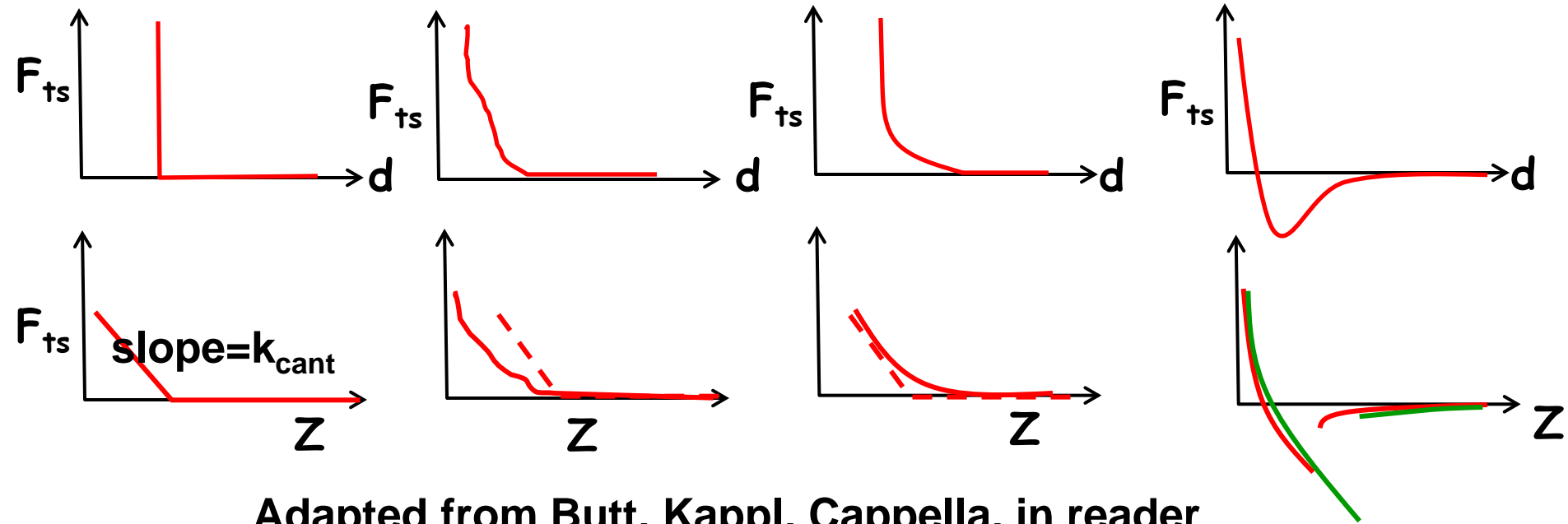
- With soft cantilevers (small k) it is not possible to measure entire 'd' range

F-d to F-Z conversion

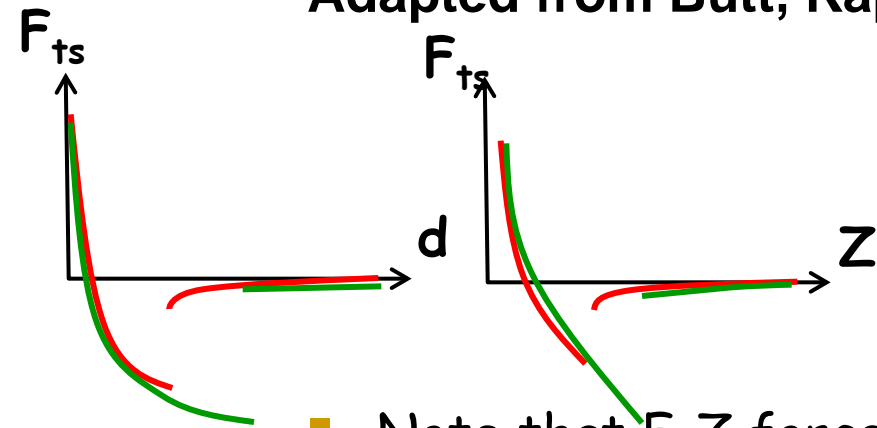


- Note that hysteresis occurs in the δ -Z curve between approach and retraction even though $F_{ts}(d)$ is conservative

Some examples of F-d to F-Z conversions



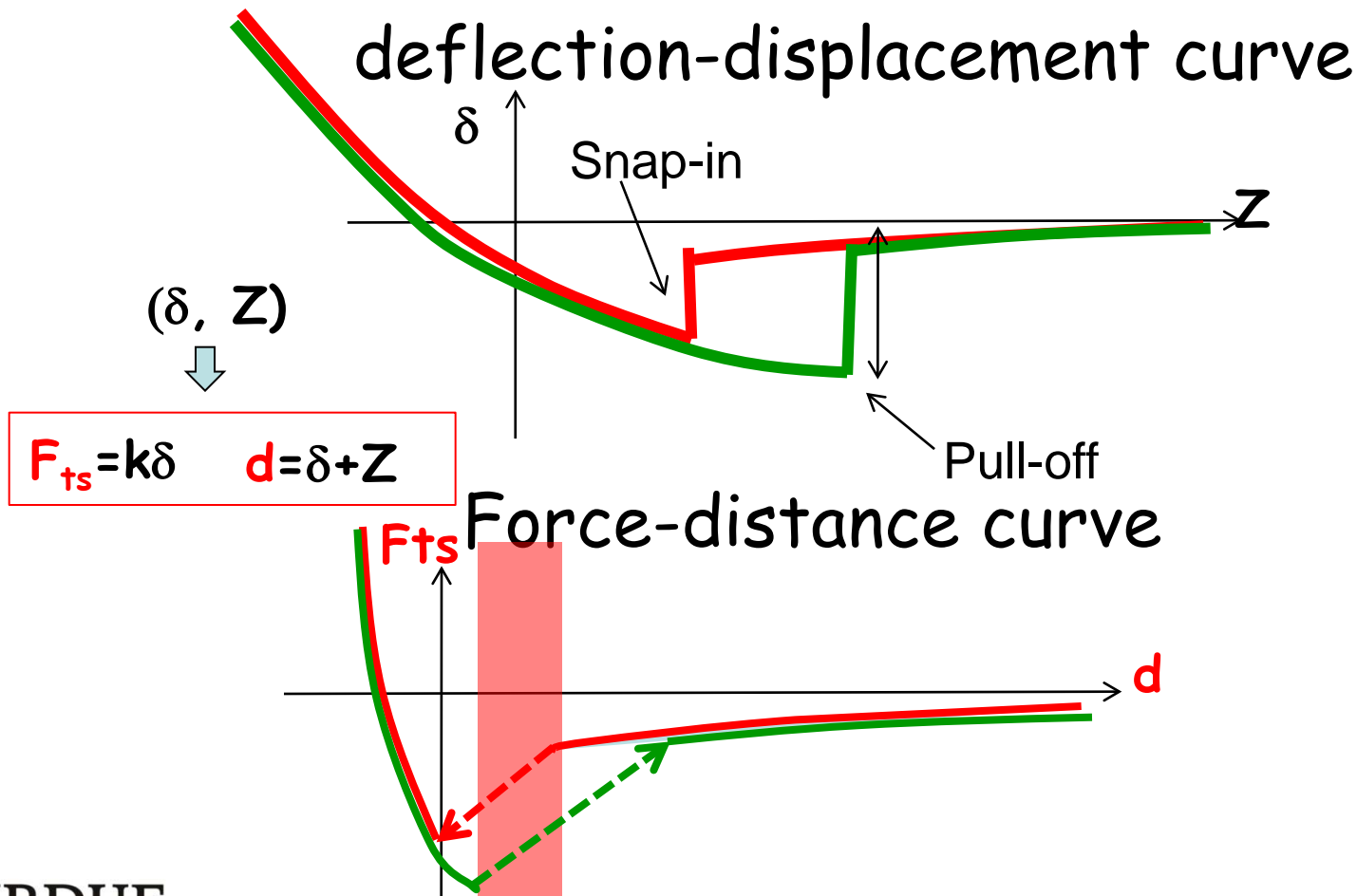
Adapted from Butt, Kappl, Cappella, in reader



- Note that F-Z force hysteresis does not mean that the F-d is hysteretic (non-conservative)
- F-Z to F-d is actually non-unique when there is hysteresis in F-Z!!

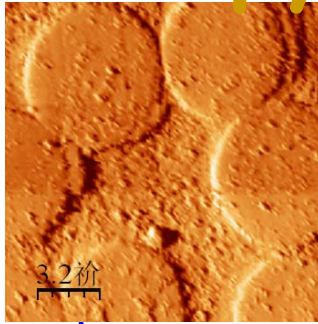
Conversely: F-Z to F-d conversion

- In a typical δ -Z experiment in AFM, the cantilever approaches/retracts from the sample while recording the cantilever deflection.
- However in force spectroscopy we are interested in converting this to a force-distance curve i.e. F_{ts} vs. d . How to convert?

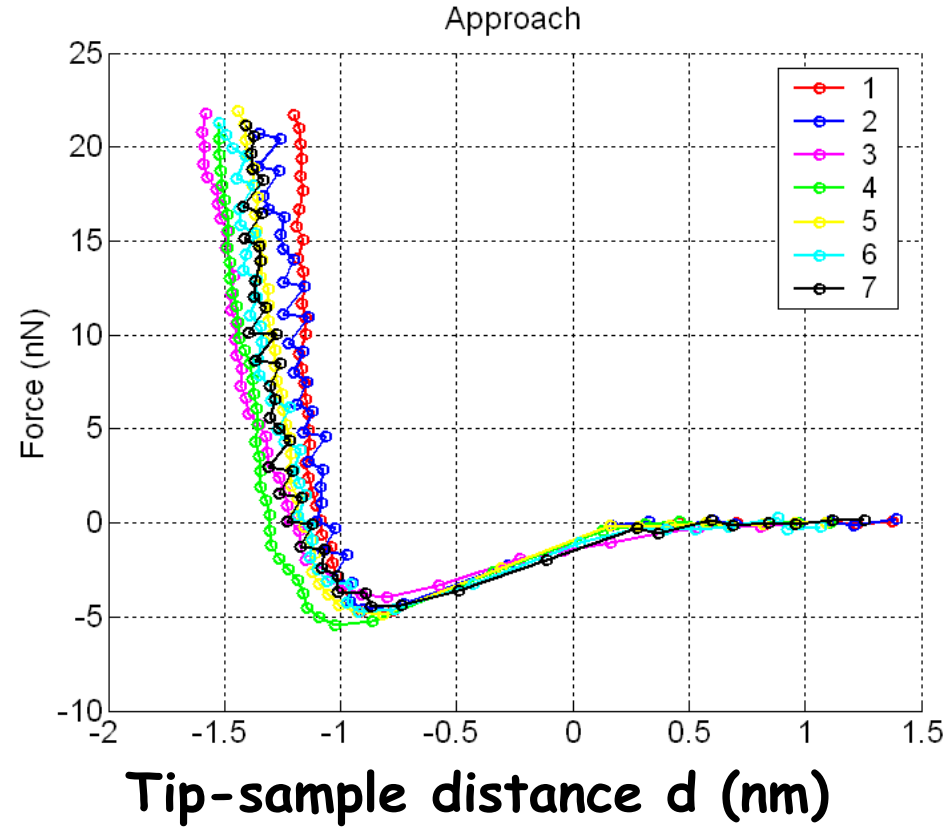
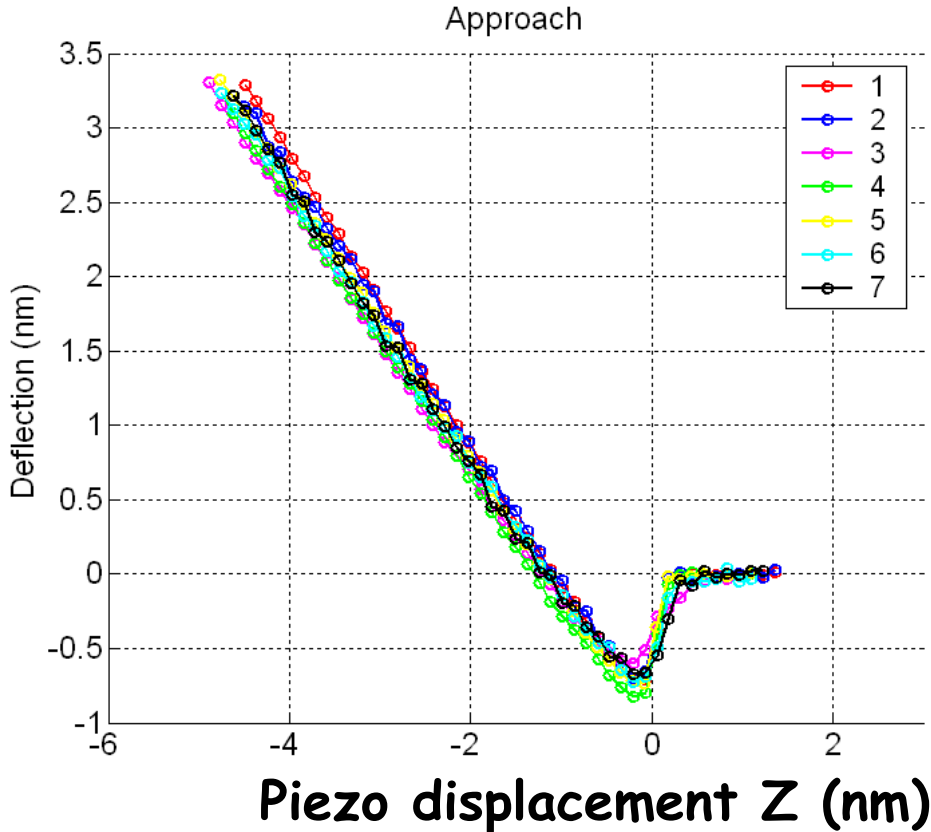


■ Important: d is only known to within an arbitrary constant!

Force spectroscopy - an example



Convert deflection vs. displacement curves to force vs. distance (gap) curves



Next class

- Practical aspects of force distance curves