Lecture 10 Force distance curves II

Arvind Raman

Mechanical Engineering

Birck Nanotechnology Center



F-Z and F-d review

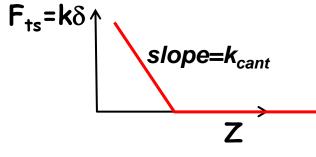
- In theory if one knows F-d then to go to F-Z:
 - For every Z solve for $k_{cant}\delta$ = Fts(d) or equivalently solve $k_{cant}(d-Z)$ = Fts(d) which can be done graphically
- In experiment, given F-Z, one goes to F-d by
 - For every F, plot along the x-axis, the quantity d= δ +Z, where Z is the Z value at that F and δ =F/k_{cant}
- Note that F-d maps one on one to F-Z curves but given a F-Z curve, more than one F-d's can exist that yield the same F-Z



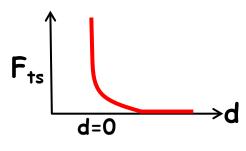
Some examples of F-Z curves

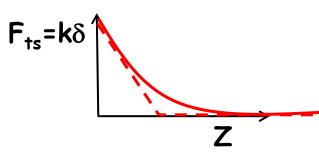
Infinitely stiff sample, rosurface forces

d=0

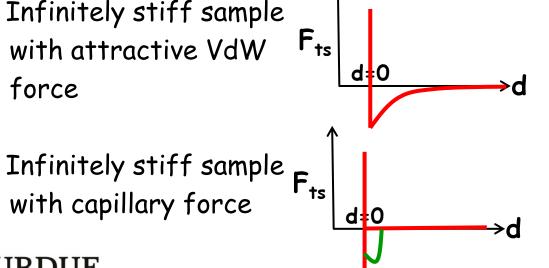


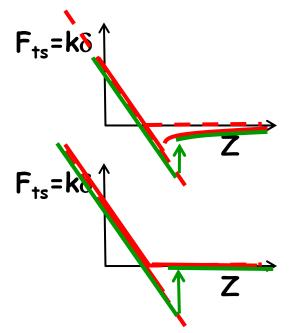
Infinitely stiff sample with surface repulsive Fts force





Infinitely stiff sample with attractive VdW force

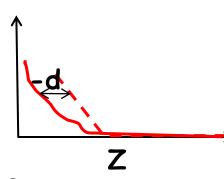




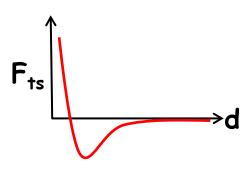
Some examples of F-Z curves

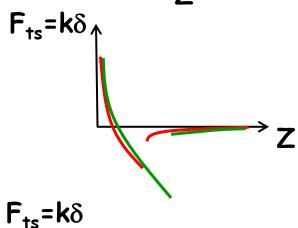
 $F_{ts}=k\delta$

Soft materials no surface forces F_{ts} d=0

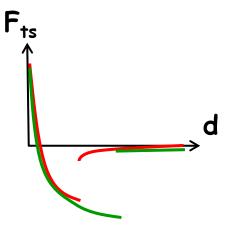


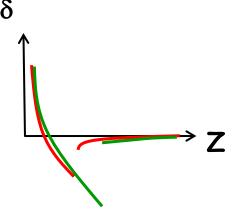
Soft material with attractive VdW force





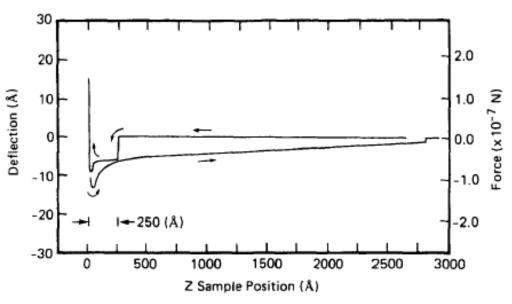
 Soft material with hysteretic F-d curve



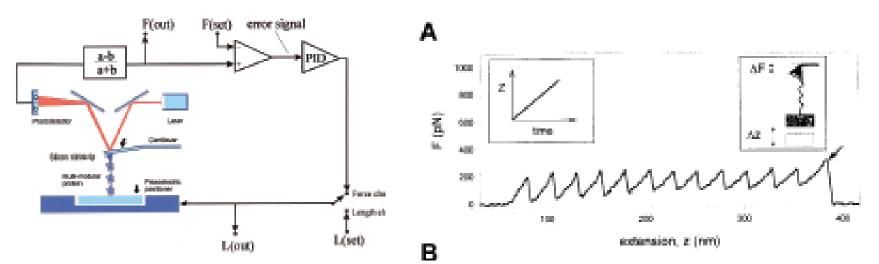




Other interesting F-Z curves

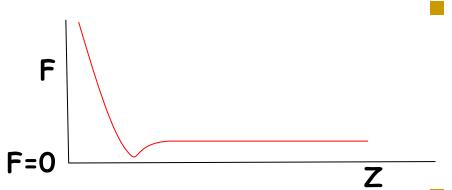


 25 nm perfluoropolyether polymeric liquid on silicon (from Mate et al (1989))



 Force-extension curves on titin (Fernandez et. al PNAS (2001))

Effects of positioning reflected laser spot in photodiode on F-Z curves



- Laser spot not centered in photodiode recenter so that photodiode output i s ~0 far from sample
- Reflected spot size affects sensitivity

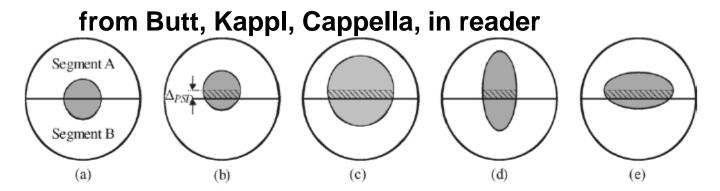
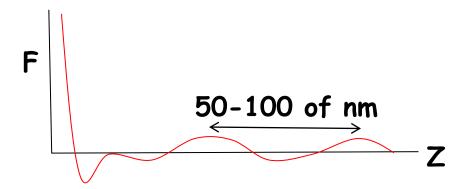


Fig. 10. The effect of laser spot shape on optical lever sensitivity. (a) A centered spot leads to zero deflection signal (A - B)/(A + B). (b) A well-shaped rotational symmetric and small spot produces a large relative area change between the A and B photodiode segments for a given deflection. This corresponds to a high sensitivity. For large deflections, however, the linear regime is small. If the spot is large (c) or distorted (d) the same deflection can produce a smaller change in relative area, hence a lower sensitivity. Also an increased sensitivity for distorted spots is possible (e).

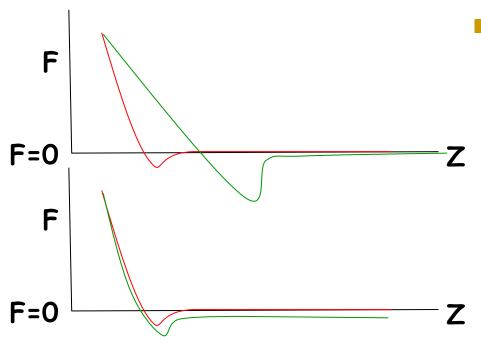
Apparent periodic signal in non-contact range



- Laser spot spilling over cantilever edge, reflecting off substrate interfering with signal back from cantilever
- Focus spot better, or use non-coherent laser.
 IR lasers are less coherent than others.

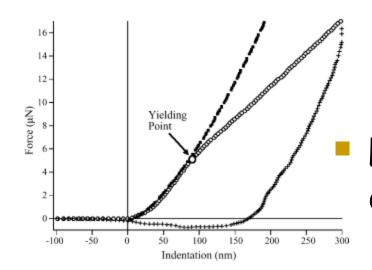


Artefacts in F-Z curves



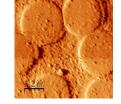
Z piezo hysteresis – warm up piezo first, use closed loop piezos

> Hydrodynamic dragreduce speed

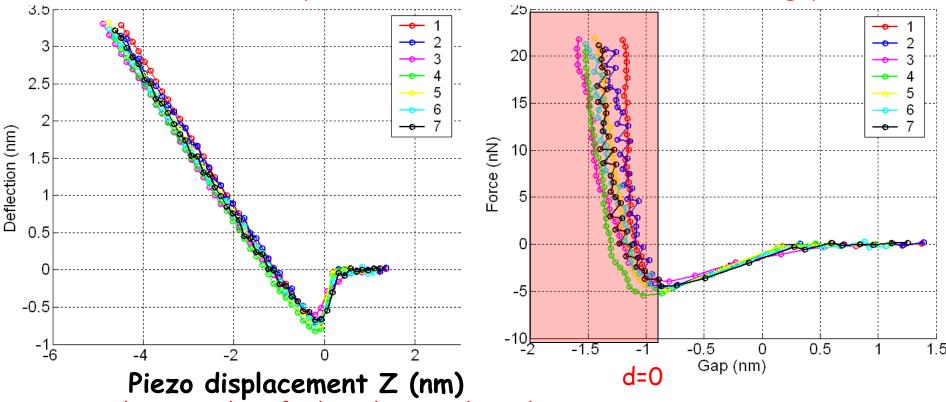


Large indentation with plastic deformation - reduce force!

Estimating sample elasticity and adhesion from F-Z curves

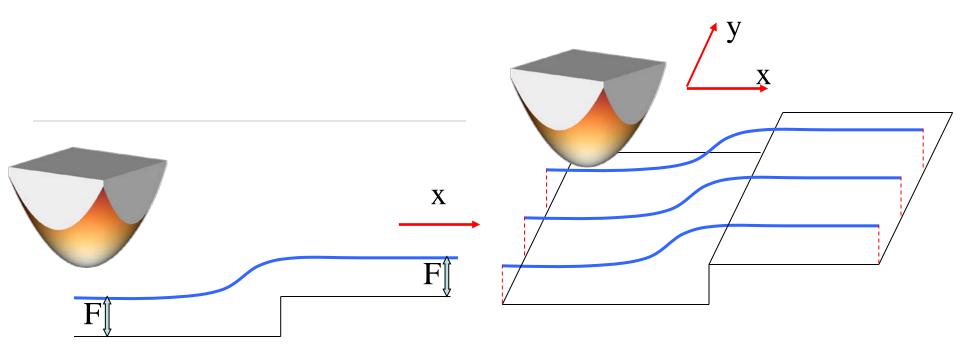


Convert deflection vs. displacement curves to force vs. distance (gap) curves



- For each curve identify d=0 where F-d reaches a minimum
- From F-d choose which model you want to use DMT, Hertz, Sneddon,Oliver-Pharr etc
- Fit curve in shaded region to DMT model F=-Fad+(3/2)E*srt(R) (-d)^3/2
- Make histogram of measured E* and Fad

Contact Mode Imaging

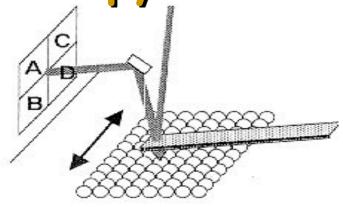


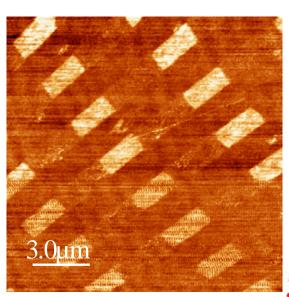


First tip contacts surface with some setpoint normal force which is kept constant during the scan

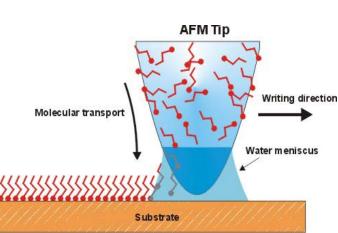
Friction Force Microscopy

- Torsional deflections due to atomic and molecular friction
- Lateral forces are specific
- Applications to nanotribology, probe based lithography

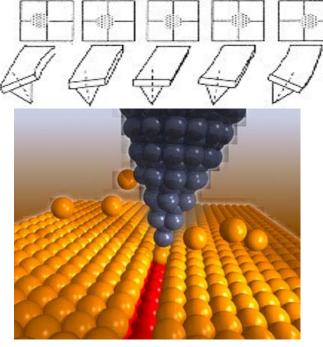




Friction force image of a self assembled monolayer (Riefenberger Group)



www.chem.nwu.edu/~mkngrp/ Dip-pen lithography



Contact mode oxidation lithography

Brief intro to dynamic AFM

- Cantilever driven near resonance
- The cantilever's resonant frequency, phase and amplitude are affected by short-scale force gradients
- In Amplitude Modulated AFM (AM-AFM) or tapping mode, driving frequency is fixed while cantilever approaches the sample
- In Frequency Modulated AFM (FM-AFM) the phase and amplitude are held constant while approaching the sample



The point mass model

$$w(x +) = A \sin(x +)$$

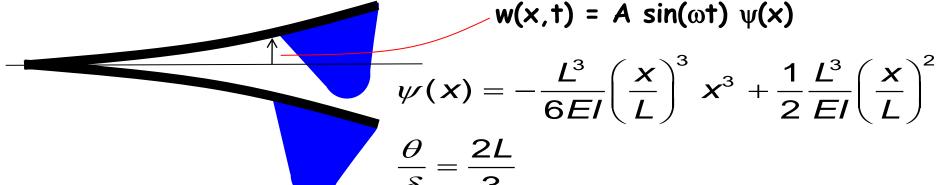
$$w(x,t) = A \sin(\omega t) \psi(x)$$

$$\cosh(\beta \frac{x}{z}) - \frac{co}{z}$$

$$\theta/\delta=$$
?

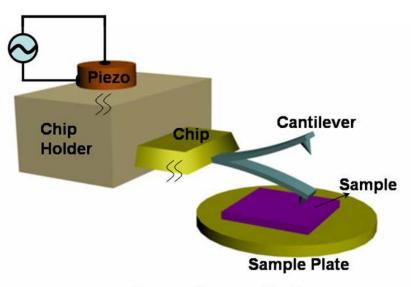
Point mass model

$$\psi(x) = \cos(\beta \frac{x}{L}) - \cosh(\beta \frac{x}{L}) - \frac{\cos(\beta) + \cosh(\beta)}{\sin(\beta) + \sinh(\beta)} \left[\sin(\beta \frac{x}{L}) - \sinh(\beta \frac{x}{L}) \right]$$
Point mass model
$$w(x,t) = A \sin(\omega t) \psi(x)$$

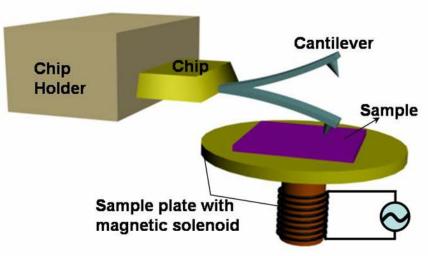


- Tip is massive, cantilever inertia negligible
- Replace cantilever by a spring of spring constant= static bending stiffness of lever
- ... Cantilever oscillates such that $\theta/\delta=2L/3$

Forced vibrations



a. Acoustic excitation



b. Magnetic excitation

- Mechanical (acoustic or piezo excitation)
- Magnetic excitation
- Magnetostrictive excitation
- Photothermal excitation
- Lorentz force excitation
- Ultrasound excitation
- Direct piezoelectric excitation